

NASA Technical Memorandum 72661, VOL. IX

SPACE SHUTTLE ORBITER TRIMMED  
CENTER-OF-GRAVITY EXTENSION STUDY:  
VOLUME IX - EFFECTS OF CONFIGURATION  
MODIFICATIONS ON THE AERODYNAMIC  
CHARACTERISTICS OF THE 140A/B ORBITER  
AT MACH NUMBERS OF 1.5, 2.0, AND 2.5

(NASA-TM-72661-Vcl-9) SPACE SHUTTLE ORBITER  
TRIMMED CENTER-OF-GRAVITY EXTENSION STUDY.  
VOLUME 9: EFFECTS OF CONFIGURATION  
MODIFICATIONS ON THE AERODYNAMIC  
CHARACTERISTICS OF THE 140 A/B ORBITER AT

NE5-1E956

G3/C2 14235  
Unclass

W. PELHAM PHILLIPS AND ROGER H. FOURNIER

JANUARY 1985



**NASA**

National Aeronautics and  
Space Administration

Langley Research Center  
Hampton, Virginia 23665

SPACE SHUTTLE ORBITER TRIMMED CENTER-OF-GRAVITY EXTENSION STUDY:  
VOLUME IX--EFFECTS OF CONFIGURATION MODIFICATIONS ON THE  
AERODYNAMIC CHARACTERISTICS OF THE 140A/B ORBITER  
AT MACH NUMBERS OF 1.5, 2.0 AND 2.5

by W. Pelham Phillips and Roger H. Fournier  
Langley Research Center

SUMMARY

Wind-tunnel tests were conducted in the Langley Unitary Plan Wind Tunnel to determine the effects of modifications designed to extend the forward trimmed center-of-gravity envelope on the static longitudinal and lateral-directional characteristics of an 0.01 scale, 140 A/B Space Shuttle Orbiter model at Mach numbers of 1.5, 2.0, and 2.5. The test Reynolds number was  $2.15 \times 10^6$ , based on model fuselage reference length. The angle-of-attack range was  $-1^\circ$  to  $32^\circ$  for sideslip angles of  $0^\circ$  and  $5^\circ$ .

All the modifications, forward extended wing fillet, a flat plate canard, and a blended canard, provided significant reductions in longitudinal stability at all Mach numbers tested. The modifications also tended to increase the directional stability at the higher angles of attack and in most cases, provided some increases in positive effective dihedral.

## INTRODUCTION

The longitudinal center-of-gravity range of the Space Shuttle Orbiter for trimmed flight during entry, approach, and landing is quite limited. This puts a considerable constraint on the allowable mass distribution of Shuttle payloads. In an effort to extend the orbiter center-of-gravity envelope, a study was undertaken at the Langley Research Center to determine the feasibility of developing simple, "bolt-on" modifications.

Modifications which were studied included changes in fuselage nose shape and wing fillet planform and the addition of fixed canard surfaces. Systems design analyses were undertaken to determine the weight penalties (ref. 1), and aerodynamic heating tests and analyses provided information on the impact of the modifications on thermal protection system requirements (ref. 2). Wind-tunnel force and moment tests were conducted across the speed range to assess the effectiveness of the modifications on flight characteristics. Hypersonic aerodynamic characteristics of the modification are presented in references 3 and 4, and transonic characteristics in reference 5.

The purpose of this paper is to present the effects of planform fillet and canard modifications on the aerodynamic characteristics of the 140A/B orbiter configuration at Mach numbers from 1.5 to 2.5. The investigation was conducted in the low Mach number test section of the Langley Unitary Plan Wind Tunnel at Mach numbers 1.5, 2.0 and 2.5 for a Reynolds number of  $2.15 \times 10^6$ , based on fuselage reference length. The angle-of-attack range extended from approximately  $-1^\circ$  to  $32^\circ$  at sideslip angles of  $0^\circ$  and  $5^\circ$ .

## SYMBOLS

The longitudinal aerodynamic data are presented about the stability system of axes, and the lateral directional data are presented about the body axes. All of the aerodynamic data contained herein are non-dimensionalized using the baseline model values for wing reference area, span, and mean aerodynamic chord. The moment reference point is located at 65 percent of the fuselage reference length (i.e. 21.38 cm (8.42 in.)) aft of the model nose. Values are given in both SI and US Customary Units. When two symbols are listed for an aerodynamic coefficient, the second applies to the computerized tabulation of coefficients in the appendix.

A	aspect ratio
b	wing span, 23.79 cm (9.37 in.)
c	mean aerodynamic chord, 12.06 cm (4.75 in.)
$C_A$ , $C_A$	axial-force coefficient, $\frac{\text{Axial force}}{q_\infty S}$
$C_D$ , $C_D$	drag coefficient $\frac{\text{Drag force}}{q_\infty S}$
$C_L$ , $C_L$	lift coefficient, $\frac{\text{Lift force}}{q_\infty S}$
$C_R$ , $C_{BL}$	rolling-moment coefficient, $\frac{\text{Rolling moment}}{q_\infty S_b}$
$C_{\alpha\beta}$	$\left(\frac{\Delta C_\alpha}{\Delta \beta}\right)_{\beta=0^\circ, 5^\circ}$ , per degree

$C_m$ , CLM      pitching-moment coefficient,  $\frac{\text{Pitching moment}}{q_\infty Sc}$

$C_N$ , CN      normal-force coefficient,  $\frac{\text{Normal force}}{q_\infty S}$

$C_n$ , CYN      yawing-moment coefficient,  $\frac{\text{Yawing moment}}{q_\infty Sh}$

$c_{n_\beta}$        $\left(\frac{\Delta C_n}{\Delta \beta}\right)_{\beta=0^\circ, 5^\circ}$ , per degree

$c_{y_\beta}$        $\left(\frac{\Delta C_Y}{\Delta \beta}\right)_{\beta=0^\circ, 5^\circ}$ , per degree

L/D      lift-drag ratio

$l$       fuselage reference length, 32.77 cm (12.90 in.)

M      Mach number

$q_\infty$       free-stream dynamic pressure, Newtons per meter<sup>2</sup> (lb/ft<sup>2</sup>)

$R_l$       free-stream Reynolds number based on  $l$

S      wing reference area, 0.025 m<sup>2</sup> (0.269 ft<sup>2</sup>)

$x_0$ ,  $y_0$       model stations, cm (in.)

$\alpha$       angle of attack, deg

$\beta$  sideslip angle, deg  
 $\delta_{BF}$  body-flap deflection angle (positive for trailing edge down), deg  
 $\delta_e$  elevon deflection angle (positive for trailing edge down), deg.  
 $\delta_{SB}$  split-rudder flare angle (positive for trailing edges deflected outboard), deg.

Model Configuration Components:

B<sub>1</sub>WVS<sub>0</sub>EF baseline 140 A/B orbiter configuration  
B<sub>1</sub> baseline fuselage forebody  
C<sub>4</sub> canard with flat-plate airfoil sections  
C<sub>5</sub> blended canard with contoured airfoil sections  
E baseline elevon  
F baseline body flap  
S<sub>0</sub> baseline planform fillet  
S<sub>2</sub> fillet modification having planform geometry similar to a strake  
V baseline vertical tail  
W baseline wing (outboard panel) having a leading-edge sweep of 45°

## APPARATUS AND TESTS

### Model

Geometric details of the model used in the wind-tunnel investigation are shown in figure 1 and table 1, and photographs of the model are shown in figure 2. The baseline configuration (fig. 1(a)) was an 0.01-scale model of the Rockwell International 140 A/B Space Shuttle Orbiter configuration described in reference 3. The model had a removable forebody and removable components in the wing planform fillet region which allowed geometry modifications. The modifications shown in figures 1(b), 1(c), and 1(d) consisted of one wing planform fillet configuration,  $S_2$ , and two canard configurations,  $C_4$  and  $C_5$ . All configurations of the present investigation incorporated a split-rudder flare angle of 55°.

The leading edge of the  $S_2$  fillet modification produced a planform shape very similar to a strake (fig. 1(b)). Fillet  $S_2$  had a leading-edge sweep angle of 67.4° that extended outboard to  $y_0 = 3.584$  cm at  $x_0 = 12.929$  cm. At this point, the fillet leading-edge sweep increased to 85°, and the effective fillet intersection with the outboard wing panel was the same as for the baseline fillet ( $S_0$ ) intersection. The streamwise sections of this modified fillet were faired with the outboard wing panel and had leading-edge radii identical to those of the baseline fillet,  $S_0$ .

Canard  $C_4$  (fig. 1(c)) had a flat-plate section with a rounded leading edge and a sharp trailing edge. The leading-edge sweep angle was 54.7°. The trailing edge was formed by a circular arc segment having a radius of 6.217 cm. The blended canard,  $C_5$  (fig. 1 (d)) was about the same size as canard  $C_4$ , but it was contoured more realistically for the actual flight environment where aerodynamic heating effects must be considered.

## Tests

The investigation was conducted in the low Mach number test section of the Langley Unitary Plan Wind Tunnel (ref. 9) at Mach numbers of 1.5, 2.0, and 2.5. Free-stream Reynolds number for the investigation was approximately  $2.15 \times 10^6$ , based on fuselage reference length. Tests angles of attack were varied from about  $-1^\circ$  to  $32^\circ$  at  $0^\circ$  and  $5^\circ$  of sideslip. An internally mounted strain-gage balance was used to measure aerodynamic forces and moments acting on the model. Corrections have been applied to the angles of attack and sideslip to account for sting and balance deflections produced by aerodynamic loads on the model.

Transition strips approximately 0.16 cm wide were located behind the leading edges of all model components using carborundum grains having a nominal grain diameter of 0.027 cm. The streamwise locations of the transition strips were 3.05 cm behind fuselage nose and 1.02 cm behind the leading edges of the wing planform fillets, canards, wing, and vertical tail.

## RESULTS AND DISCUSSION

Aerodynamic data obtained in the present study are tabulated by run number in the appendix which also includes a Data Set/Run Number Collation Summary (table II) to expedite the location of data for a particular configuration and test condition.

### Longitudinal Aerodynamic Characteristics

The longitudinal aerodynamic characteristics for the baseline orbiter configuration, B<sub>1</sub>WVS<sub>0</sub>EF, are shown in figure 3 for three elevon deflections at  $\delta_{RF} = -11.7^\circ$  and  $\delta_{SB} = 55^\circ$ .

The effects of the various configuration modifications on the static longitudinal characteristics of the orbiter model are presented in figures 4 to 6. Replacing the baseline fillet,  $S_0$ , with the forward extended fillet,  $S_2$  produced significant reductions in longitudinal stability levels over the Mach number range of this investigation (fig. 4). The model was still longitudinally stable in the nominal flight angle-of-attack range ( $10 \leq \alpha \leq 13.2^\circ$ ) at Mach 1.5, but it was unstable at the two higher Mach numbers. With the c.g. moved to the maximum forward hypersonic trim position,  $x/l=0.623$ , as taken from the table in reference 6, the model was longitudinally stable in the nominal flight angle of attack range at all three Mach numbers. The dashed line in figure 4 represents the  $C_m = 0$  line rotated to reflect the maximum forward c.g. location.

Addition of the canards (figs. 5 and 6) also produced significant reductions in longitudinal stability at all Mach numbers tested, but the model is still stable at Mach 1.5. Figures 5(a) and 6(a) show that the unstable break in the baseline model pitching moment curve at Mach 1.5 was eliminated by installing the canards. Reference 8 also shows this effect for the  $C_4$  canard at a Mach number of 1.2. A comparison of the model longitudinal characteristics with the  $C_4$  and blended ( $C_5$ ) canards (fig. 7) indicates that the flat-plate canard produced larger positive pitching-moment increments than the blended canard. Reference 5 also shows the same trend at Mach 6.0. Post-test measurements indicated that, although the areas of the canards were nearly the same, the estimated effective moment arm of the blended canard was somewhat shorter than that of the flat-plate canard, and this may explain some of the differences. The blended canard produced about the same negative stability contribution as the  $S_2$  fillet for the Mach number range of these tests.

With the c.g. moved to the maximum forward position for hypersonic trim (dashed zero- $C_m$  lines, figs. 5 and 6) as taken from the table in reference 6 (0.6182 for  $C_4$ , and 0.623 for the blended canard, assuming its contribution to be equivalent to that of  $S_2$ ), the model would be longitudinally stable at all Mach numbers except for the blended canard at Mach 2.5 (fig. 6(c)) where it is neutrally stable in the nominal flight angle-of-attack range.

#### Lateral-Directional Aerodynamic Characteristics

The static lateral-directional characteristics of the baseline model and with the configuration modifications are presented in figures 8 to 12. Figure 9 shows that, in general, all of the modifications tended to increase the directional stability of the baseline model over the higher angle-of-attack range at all Mach numbers investigated. The modifications also increased the positive effective dihedral parameter,  $-C_{\delta_B}$ , at Mach numbers of 1.5 and 2.0, but a slight reduction in this parameter occurred at Mach 2.5.

#### Concluding Remarks

The results of an investigation of the static aerodynamic characteristics of an 0.01 scale Space Shuttle Orbiter model at Mach numbers of 1.5, 2.0, and 2.5, as affected by configuration modifications, showed that the extended fillet, flat-plate canard, and blended canard decreased the longitudinal stability at all Mach numbers tested. With the center of gravity moved to the maximum forward hypersonic trim position, the model with the modifications was longitudinally stable at all Mach numbers tested, with the exception that the model with the blended canard was neutrally stable at Mach 2.5. The modifications increased the directional stability at high angles of attack at all Mach numbers tested and increased the effective dihedral parameter at Mach numbers of 1.5 and 2.0.

## REFERENCES

1. MacConochie, Ian O.; LeMessurier, Robert W.; and Walsh, Robert F.: Space Shuttle Orbiter Trimmed Center-of Gravity, Extension Study. Vol. VI - System Design Studies. NASA TM X-72661, 1978.
2. Dunavant, James C.: Space Shuttle Orbiter Trimmed Center-of-Gravity Extension Study. Vol. III - Impact of Retrofits for Center-of-Gravity Extension on Orbiter Thermal Protection System. NASA TM X-72661, 1979.
3. Bernot, Peter T.: Space Shuttle Orbiter Trimmed Center-of-Gravity Extension Study. Vol. I - Effects of Configuration Modifications on the Aerodynamic Characteristics of the 140 A/B Orbiter at Mach 10.3. NASA TM X-72661, 1975.
4. Scallion, William I.; and Stone, David R.: Space Shuttle Orbiter Trimmed Center-of-Gravity Extension Study. Vol. IV - Effects of Configuration Modifications on the Aerodynamic Characteristics of the 139B Orbiter at Mach 20.3. NASA TM X-72661, 1978.
5. Phillips, W. Pelham: Space Shuttle Orbiter Trimmed Center-of-Gravity Extension Study. Vol.VIII - Effects of Configuration Modifications on the Aerodynamic Characteristics of the 140 A/B Orbiter at a Mach Number of 5.97. NASA TM X-72661, 1984.
6. Phillips, W. Pelham; and Fournier, Roger H.: Space Shuttle Orbiter Trimmed Center-of-Gravity Extension Study. Vol. V - Effects of Configuration Modifications on the Aerodynamic Characteristics of the 140 A/B Orbiter at Mach Numbers of 2.5, 3.95 and 4.6. NASA TM X-72661, 1979.
7. Phillips, W. Pelham: Space Shuttle Orbiter Trimmed Center-of-Gravity Extension Study. Volume VII - Effects of Configuration Modifications on the Subsonic Aerodynamic Characteristics of the 140 A/B Orbiter at High Reynolds Numbers. NASA TM X-72661, 1981.

8. Phillips, W. Pelham: Space Shuttle Orbiter Trimmed Center-of-Gravity Extension Study, Vol. II - Effects of Configuration Modifications on the Aerodynamic Characteristics of the 140 A/B Orbiter at Transonic Speeds.  
NASA TM X-72661, 1976.

9. Schaefer, William T., Jr.: Characteristics of Major Active Wind Tunnels at the Langley Research Center. NASA TM X-1130, 1965.

TABLE I. - MODEL GEOMETRY

## Theoretical wing:

Area, planform, $m^2$ ( $ft^2$ ) . . . . .	0.02499 (0.2690)
Area, cleven, $m^2$ ( $ft^2$ ) . . . . .	0.001951 (.0210)
Span, cm (in.) . . . . .	23.792 (9.367)
Chord, centerline root, cm (in.) . . . . .	17.507 (6.892)
Chord, tip, cm (in.) . . . . .	3.501 (1.378)
Taper ratio . . . . .	0.20
Aspect ratio . . . . .	2.265
Leading-edge sweep angle, deg . . . . .	45.0
Trailing-edge sweep angle, deg . . . . .	-10.0
Dihedral angle, deg . . . . .	3.5
Incidence angle, deg ( $y_0 = 5.056$ cm) . . . . .	0.5
Twist angle, deg . . . . .	3.0
Airfoil section, tip . . . . .	0012-64 modified
$x_0$ , wing leading edge, plane of symmetry . . . . .	21.234 (8.360)

Wing planform fillet  $S_0$ , baseline:

Leading-edge sweep angle, deg . . . . .	80.9
$x_0$ , wing leading-edge (theoretical) intersection cm (in.) . . . . .	25.984 (10.230)

Wing planform fillet  $S_2$ :

Leading-edge sweep angle (forward portion), deg . . . . .	67.4
Leading-edge sweep angle (aft portion), deg . . . . .	85.0
$x_0$ , intersection of forward and aft fillet leading edges, cm (in.) . . . . .	12.929 (5.090)
$x_0$ , intersection of aft fillet and theoretical wing, cm (in.) . . . . .	25.984 (10.230)

TABLE I. - CONCLUDED

Canard C<sub>4</sub>:

Leading-edge sweep angle( $ft^2$ ) . . . . .	54.7
Exposed area, $m^2$ ( $ft^2$ ). . . . .	0.002544(0.027388)

Blended Canard C<sub>5</sub>

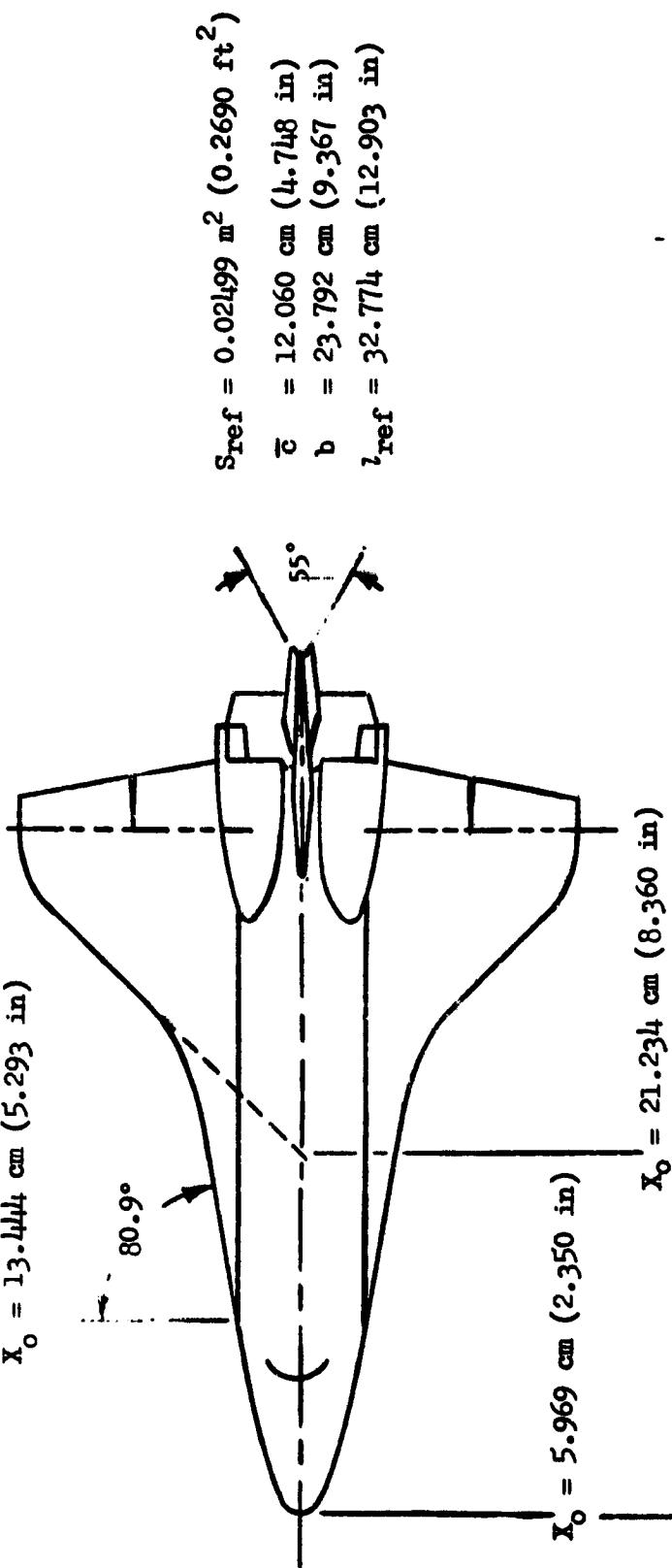
Exposed area, $m^2$ ( $ft^2$ ). . . . .	0.001839 (0.019798)
Leading-edge sweep angle, deg . . . . .	58.15

## Vertical tail:

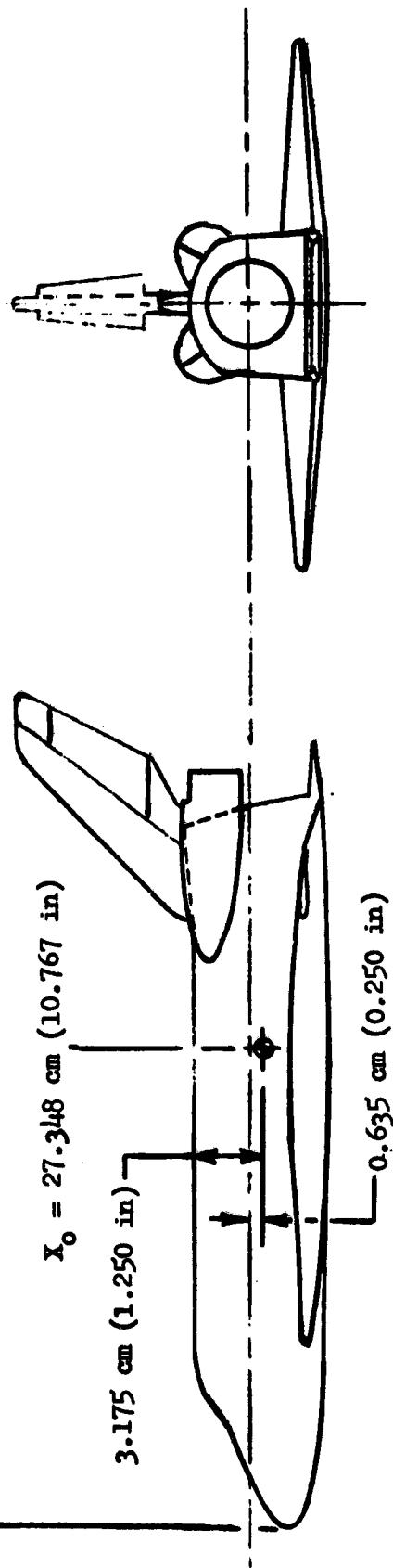
Area (theoretical), $m^2$ ( $ft^2$ ) . . . . .	0.003839 (0.041325)
Leading-edge sweep angle, deg . . . . .	45.0
Root chord (theoretical), cm (in.) . . . . .	6.820 (2.685)
Tip chord (theoretical), cm (in.) . . . . .	2.755 (1.085)
Span, cm (in.) . . . . .	8.019 (3.157)

## Fuselage:

Maximum cross-sectional area, $m^2$ ( $ft^2$ ) . . . . .	0.003595 (.0387)
Length, cm (in.) . . . . .	32.774 (12.903)
Maximum width, cm (in.) . . . . .	6.797 (2.676)

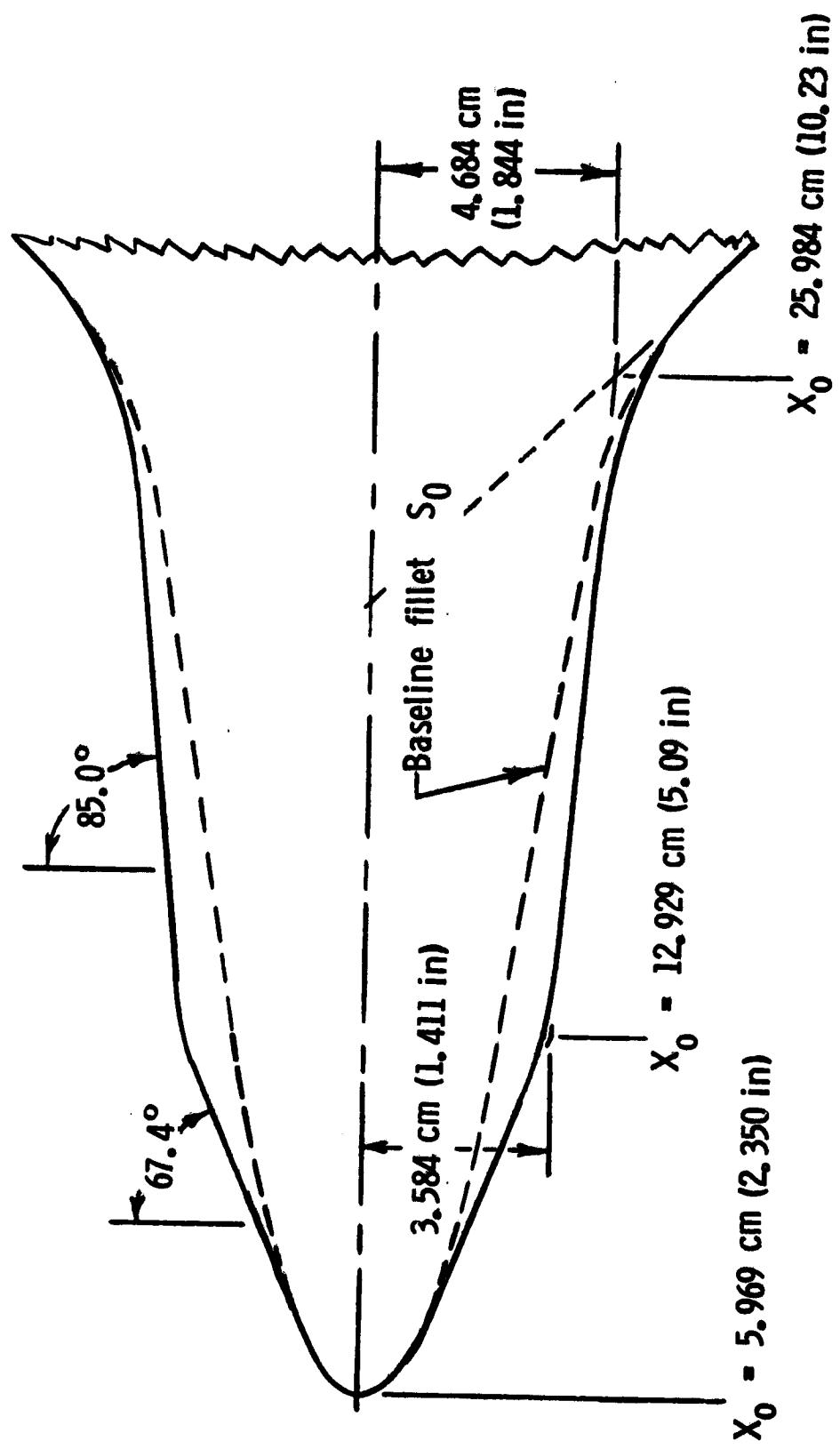


14



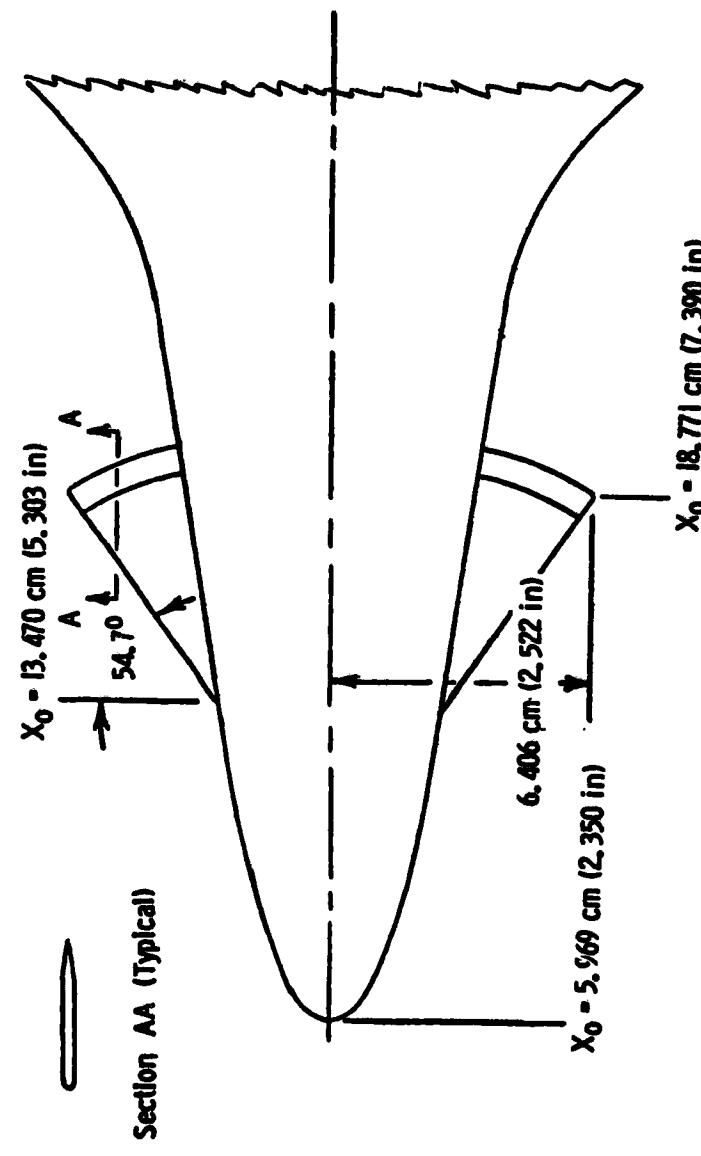
(a) Three-view of baseline orbiter model (Configuration B1W5QEF)

Figure 1. - Model drawings.



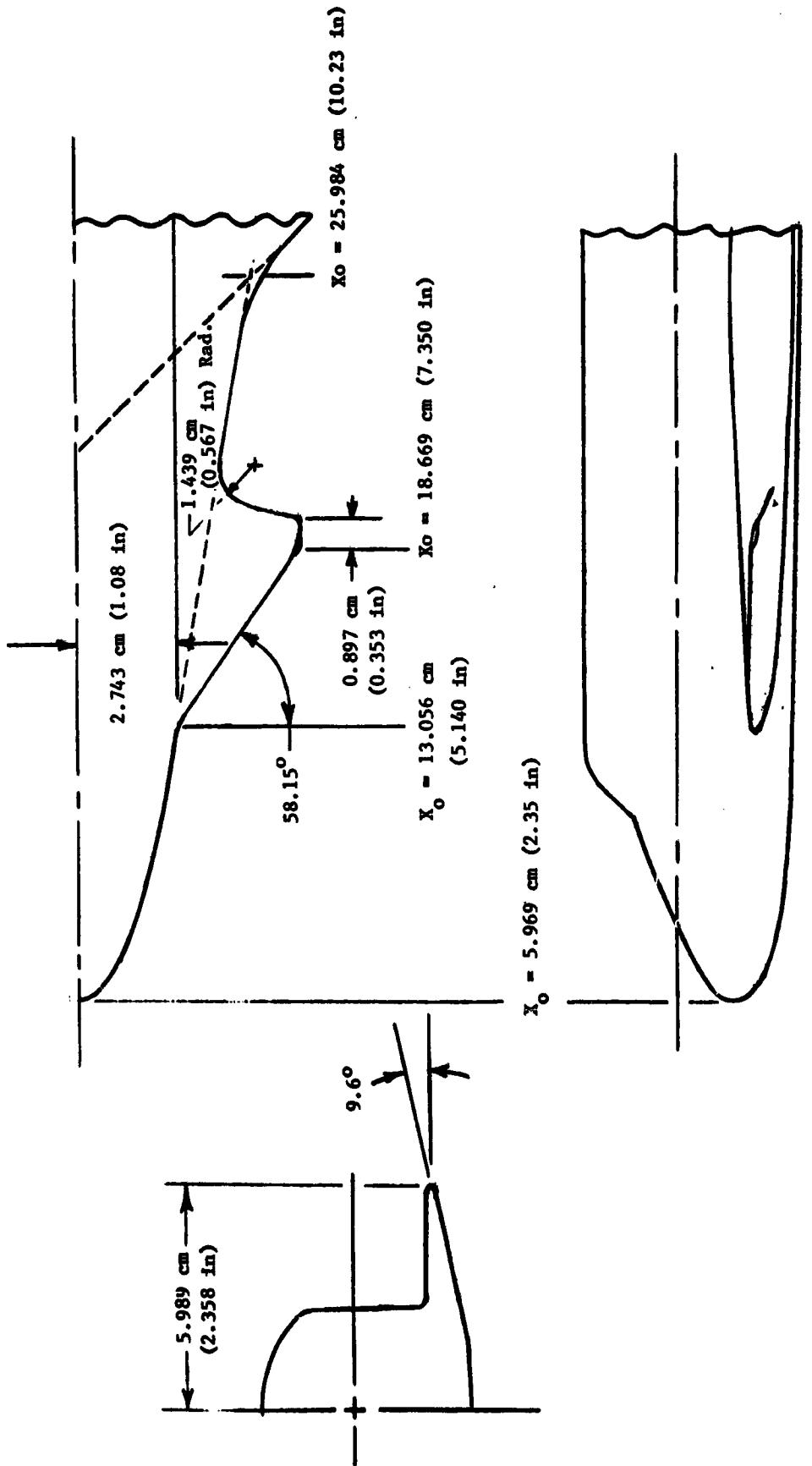
(b) Fillet  $S_2$  (Configuration  $B_1WVS_2^{\text{EF}}$ )

Figure 1.- Continued.



(c) Canard  $C_4$  modification

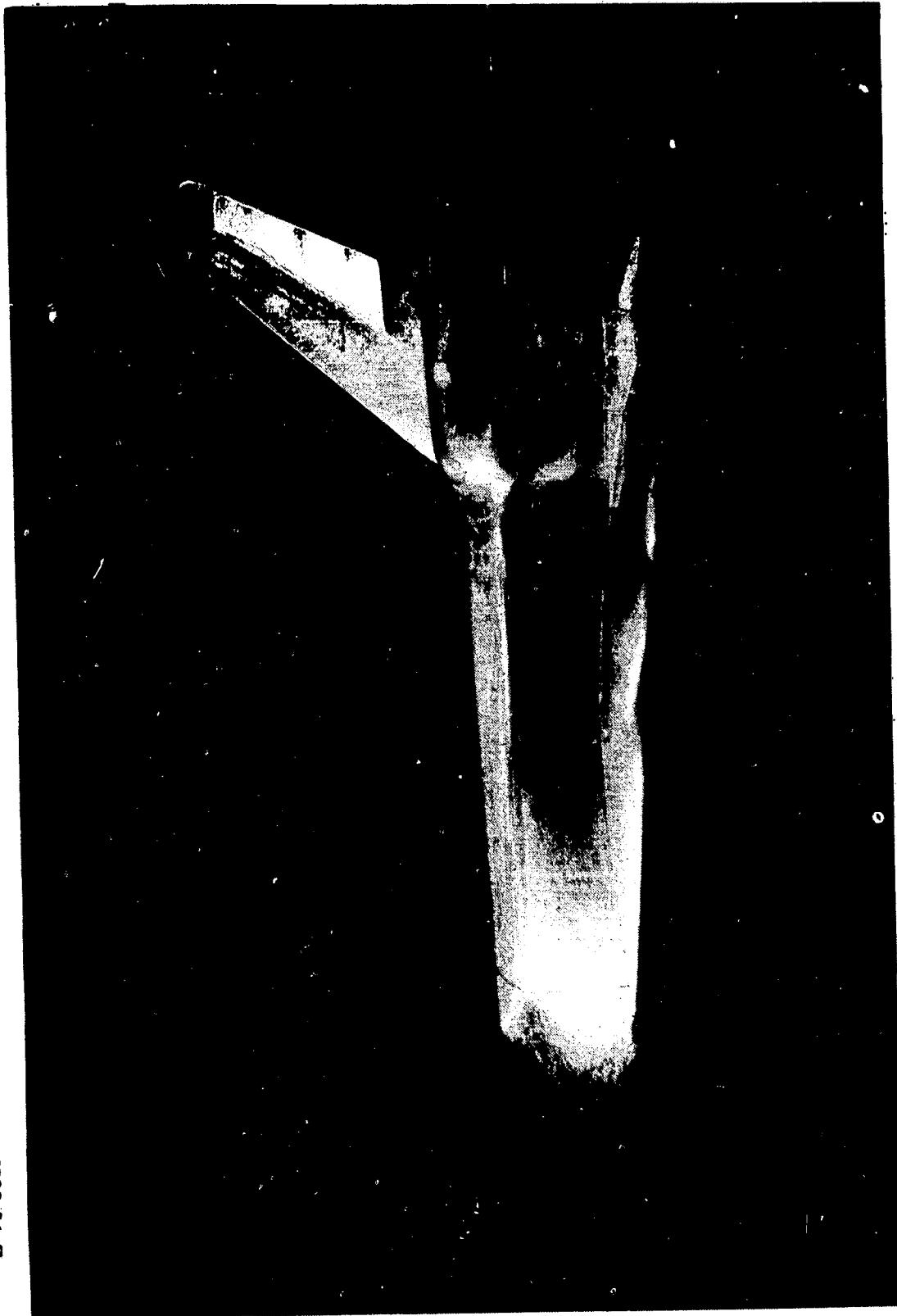
Figure 1. - Continued



(d) Canard  $C_5$

Figure 1. - Concluded.

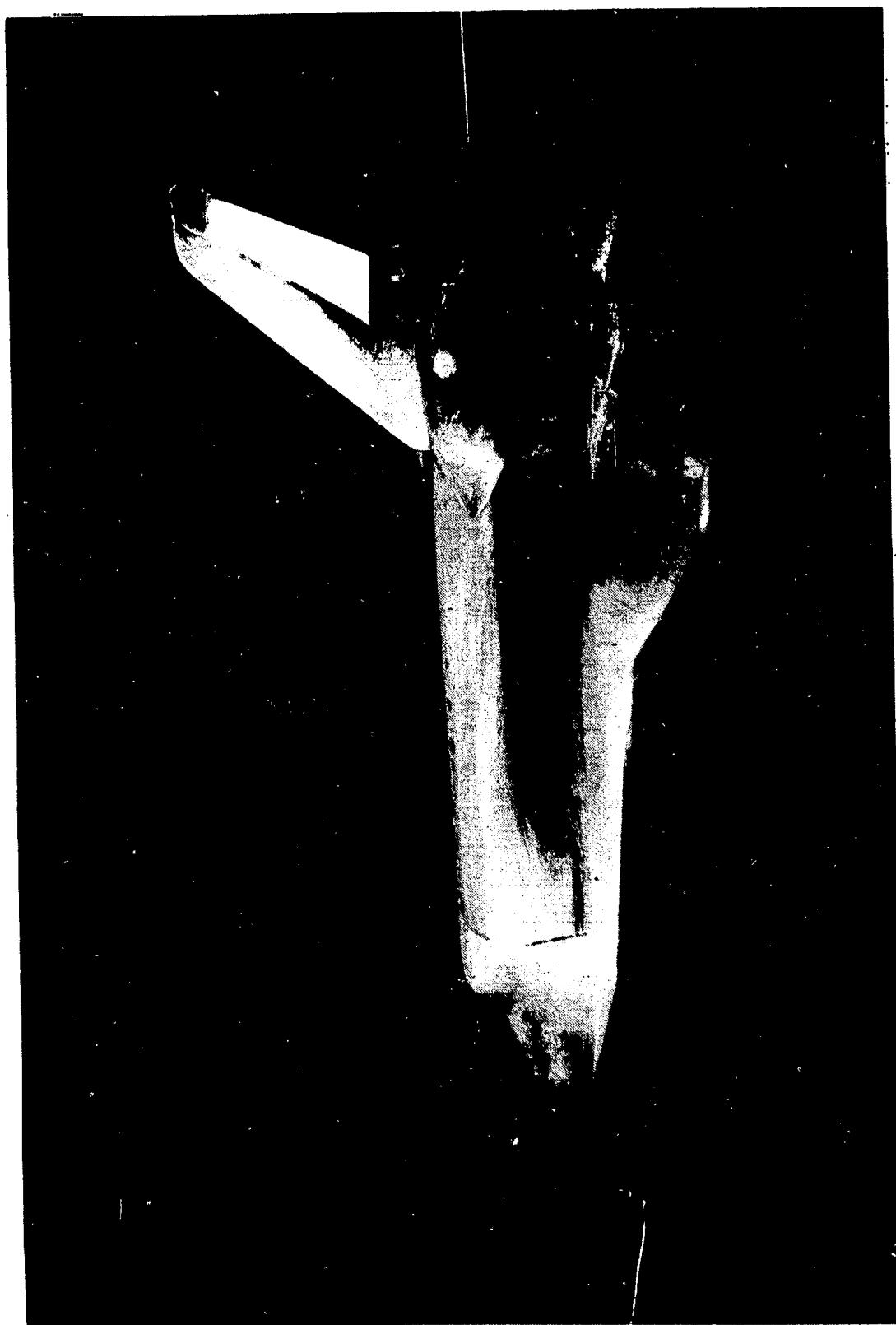
NASA  
L-74-5615



(a) Baseline orbiter model configuration.

Figure 2. - Photographs of the 0.01-scale 140 A/B orbiter model.

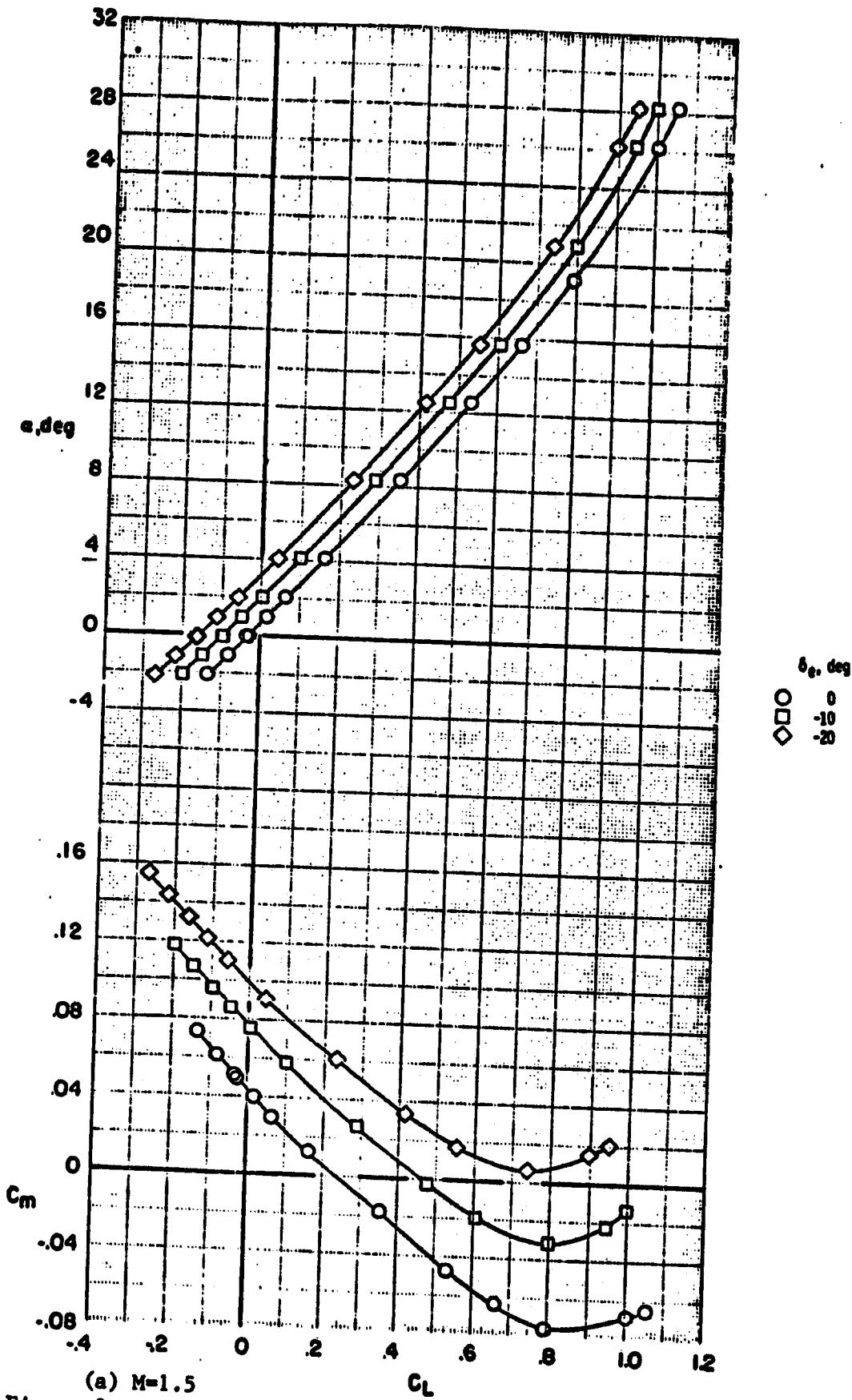
ORIGINAL PAGE IS  
OF POOR QUALITY.



(b) Model with the  $S_2$  fillet modifications.

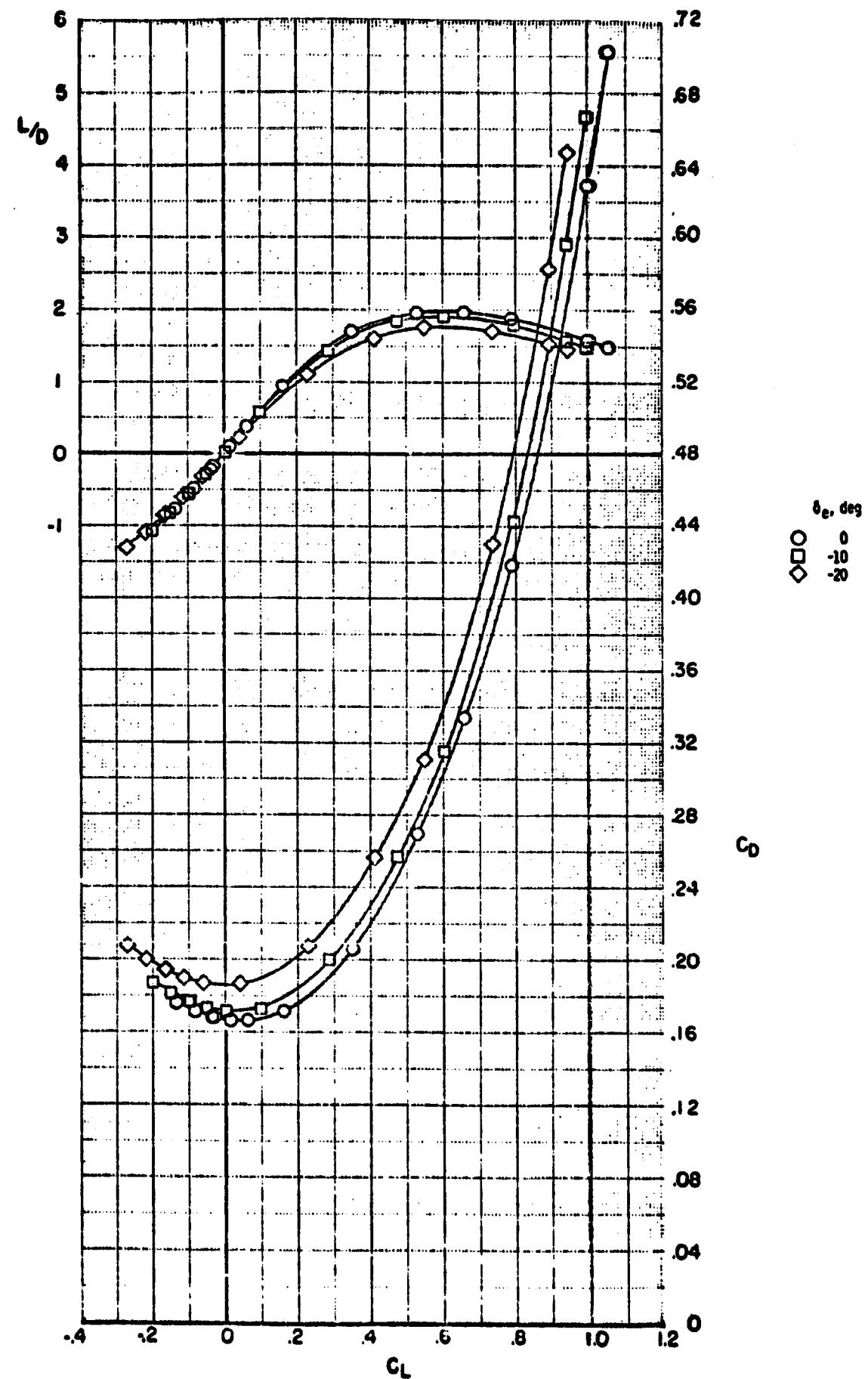
Figure 2. - Concluded.

NASA  
174-5609

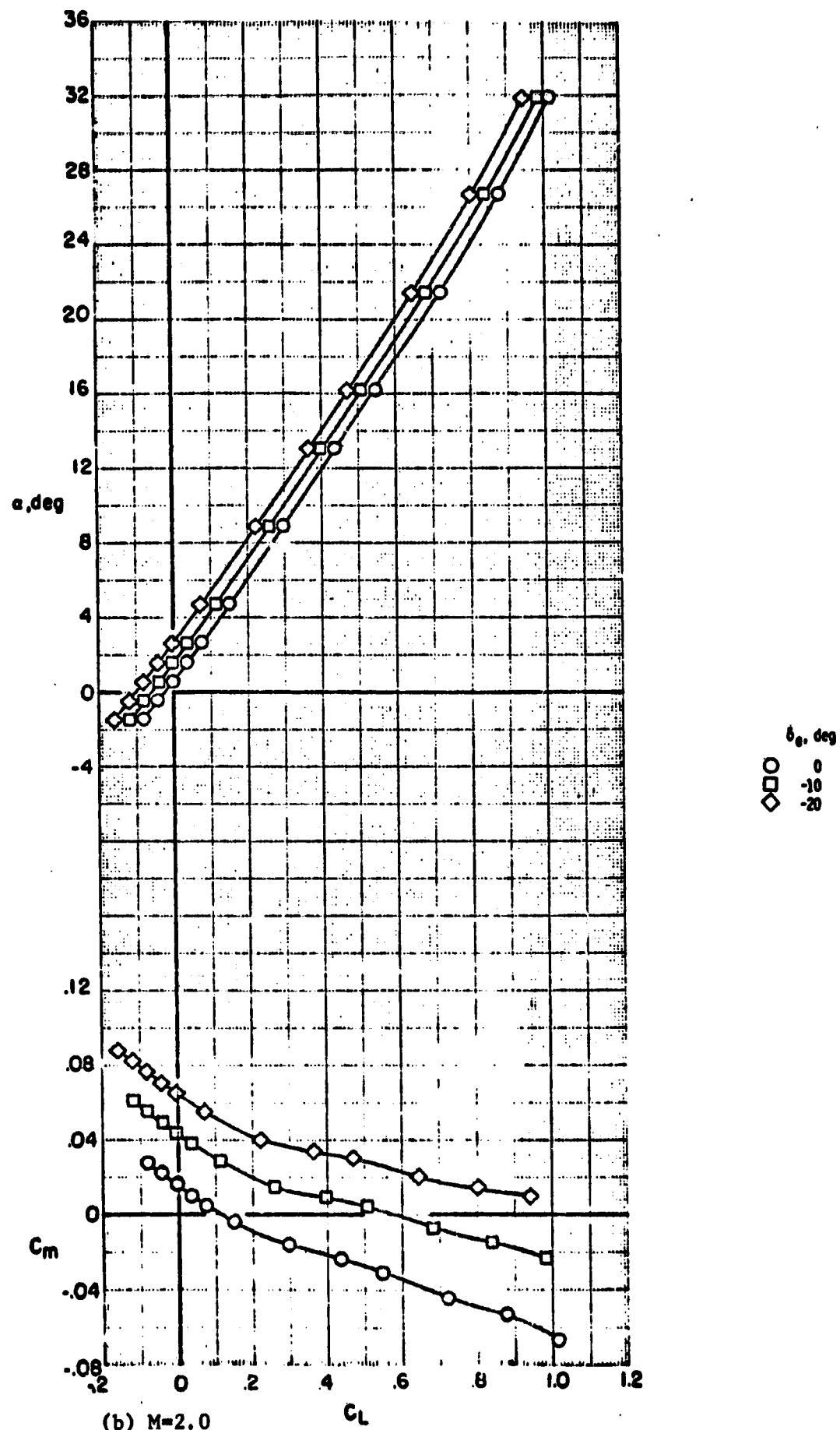


(a)  $M=1.5$

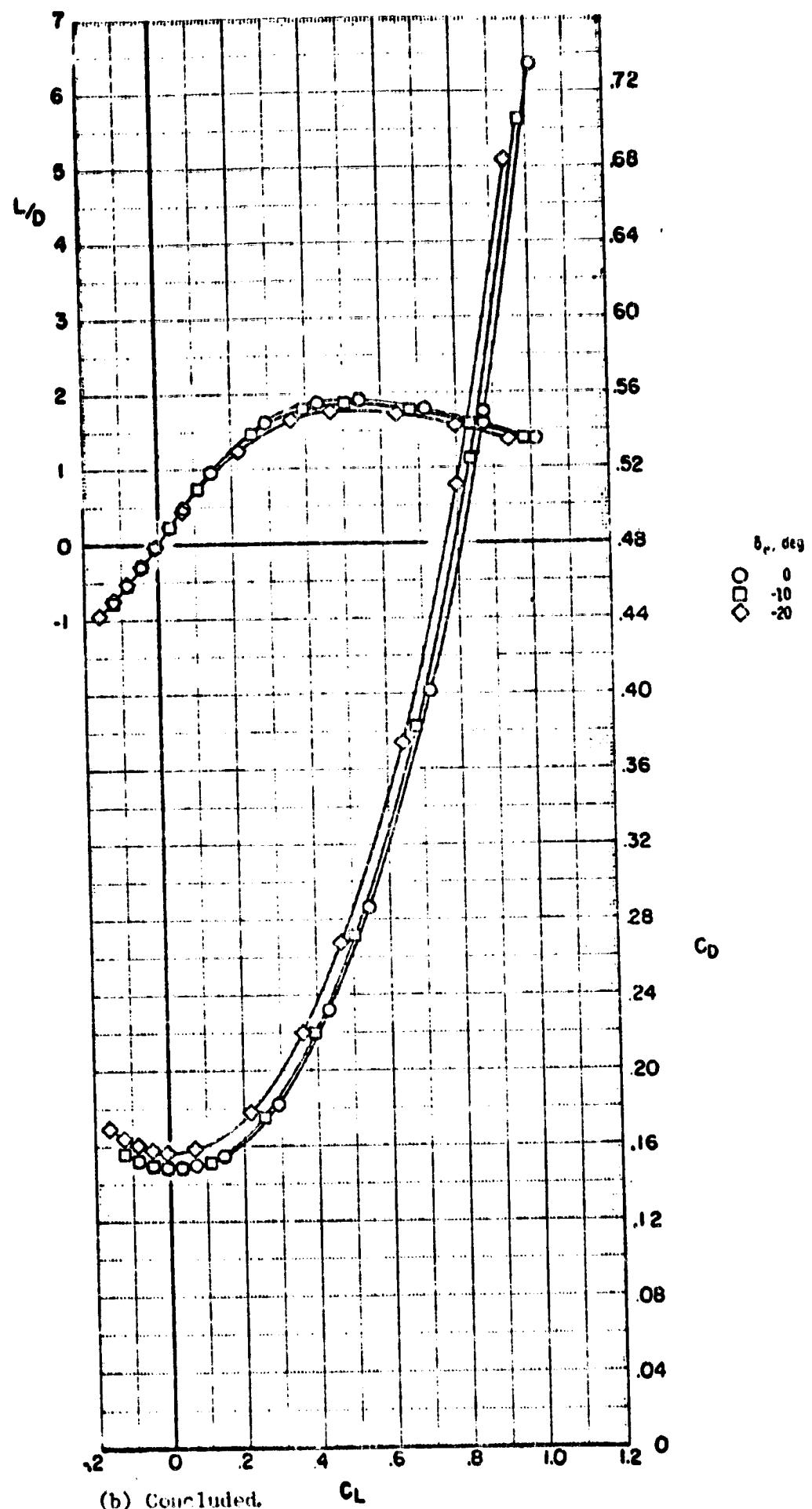
Figure 3. - Longitudinal aerodynamic characteristics  
for baseline 140 A/B configuration ( $B_1 WVS_0 EF$ )  $\delta_{BF} = -11.7^\circ$ ;  
 $\delta_{SB} = 55^\circ$



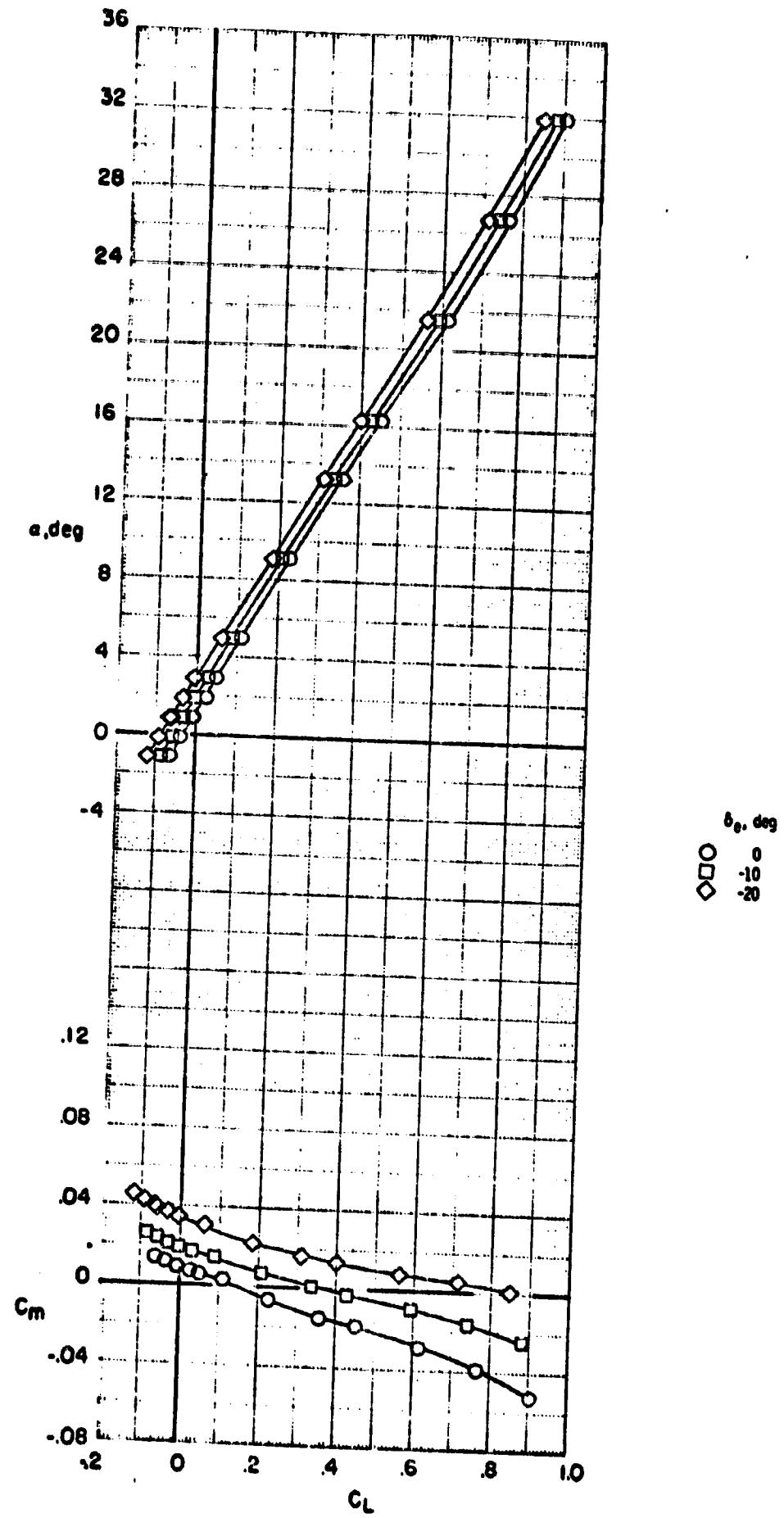
(a) Concluded.  
Figure 3. - Continued.



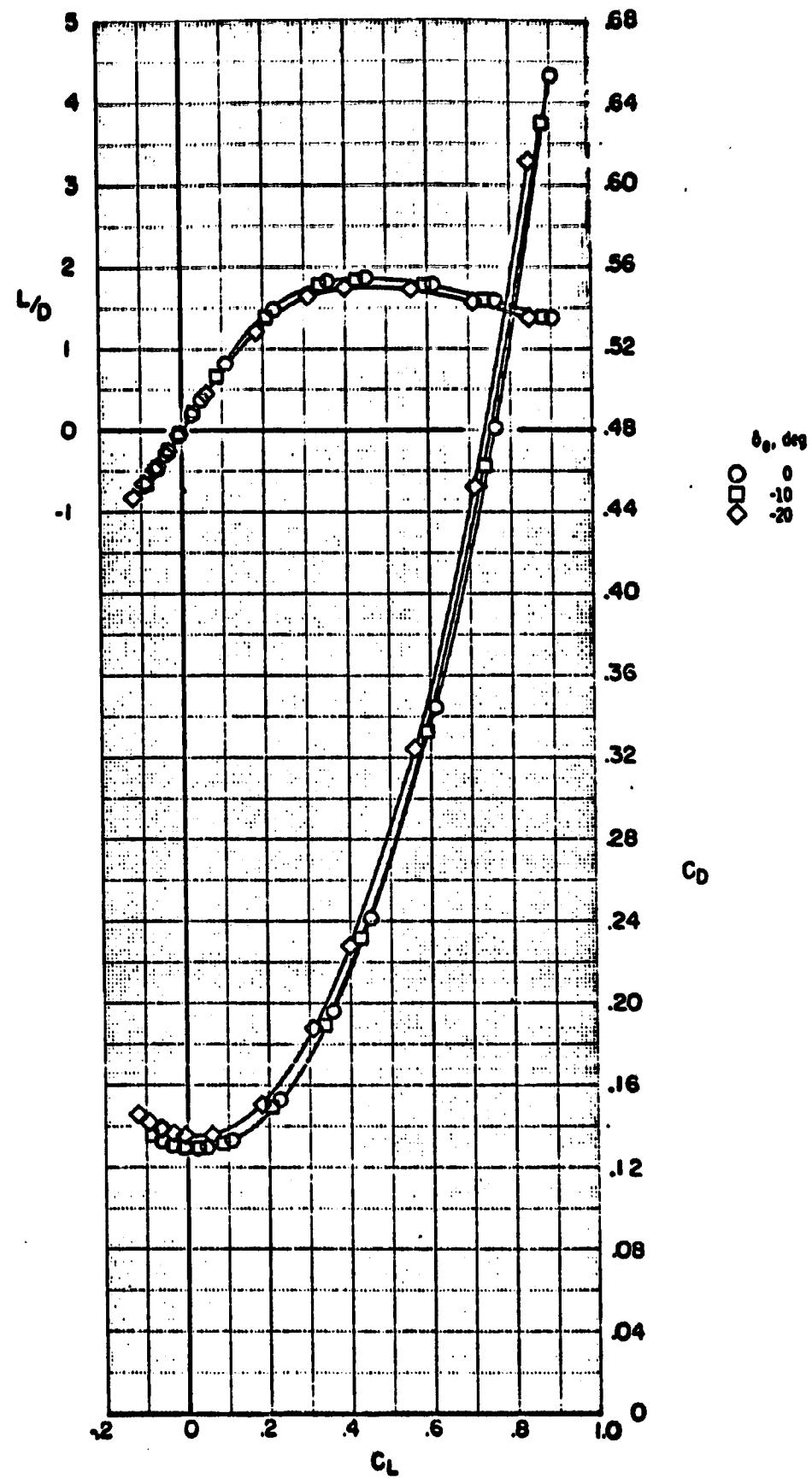
(b)  $M=2.0$   
Figure 3. - Continued.



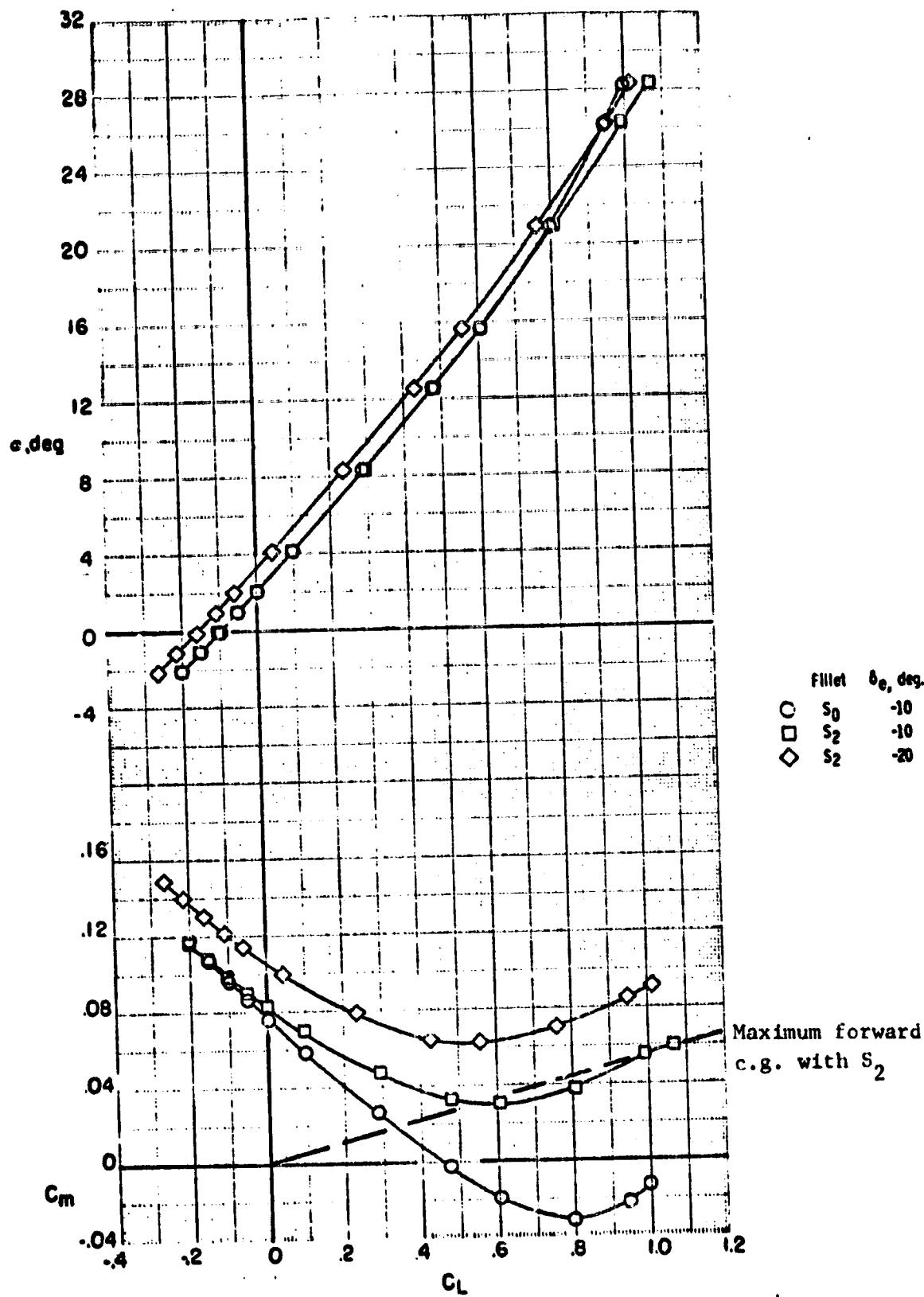
(b) Concluded.  
Figure 3. - Continued.



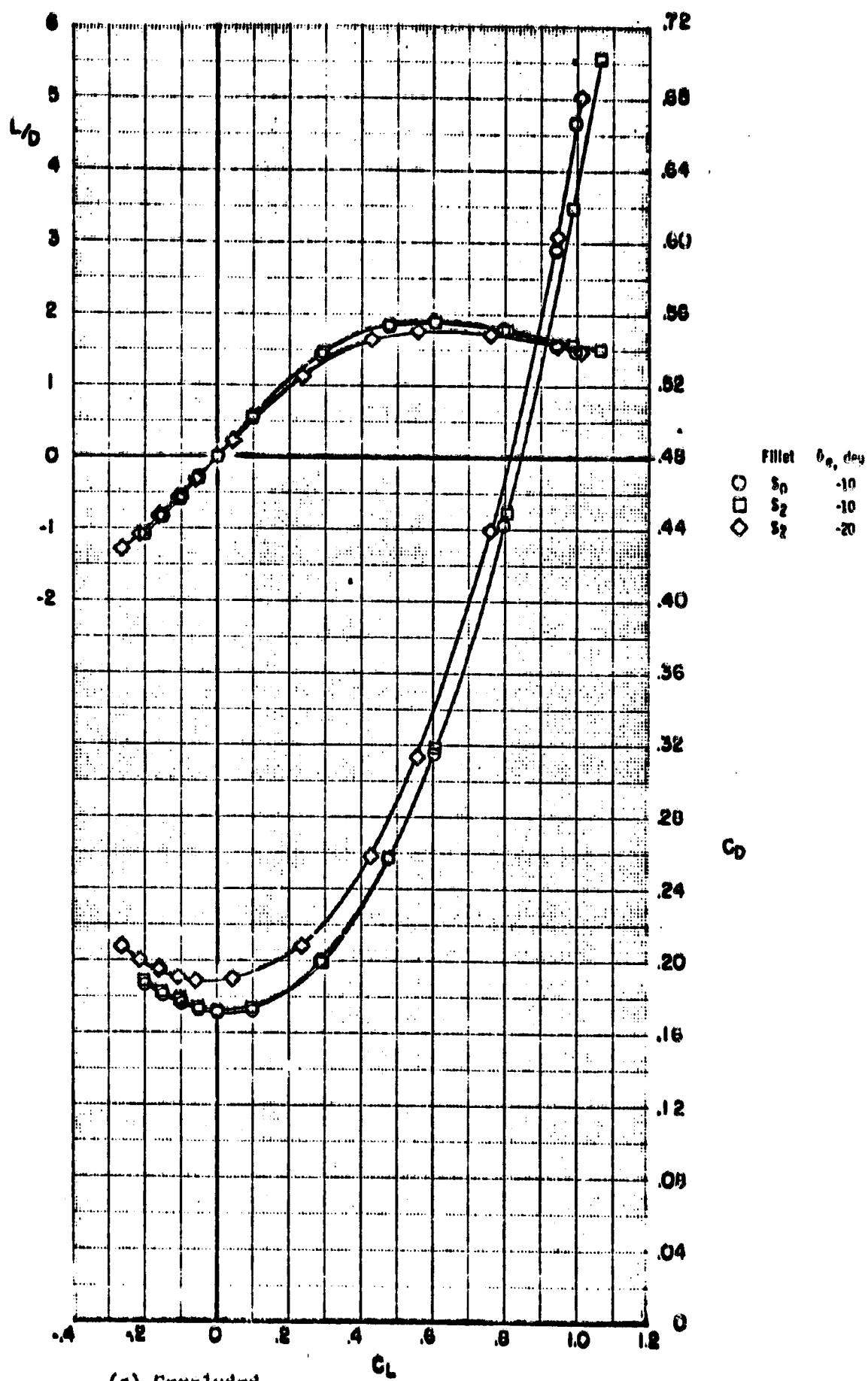
(c)  $M=2.5$   
Figure 3. - Continued.



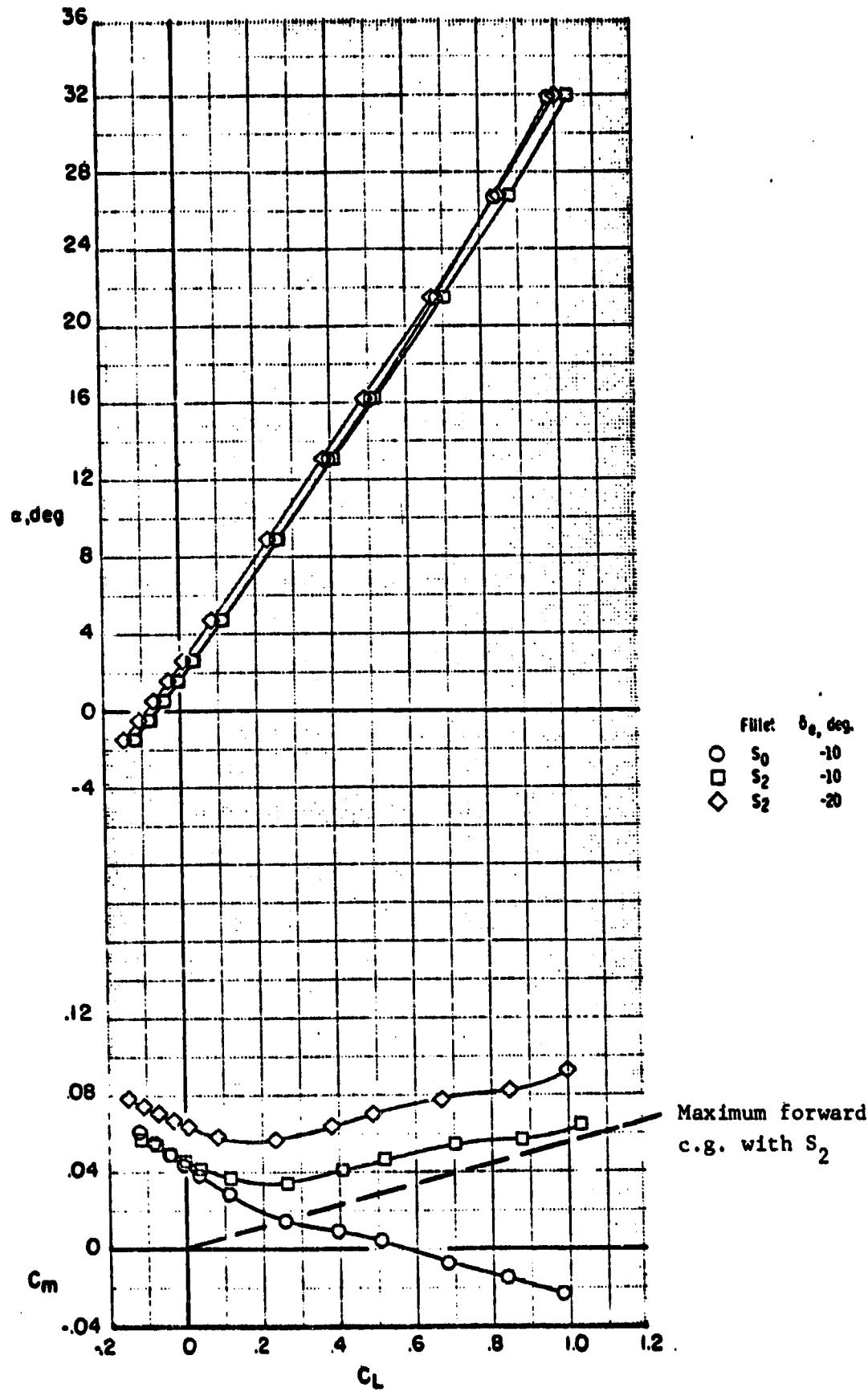
(c) Concluded.  
Figure 3. - Concluded.



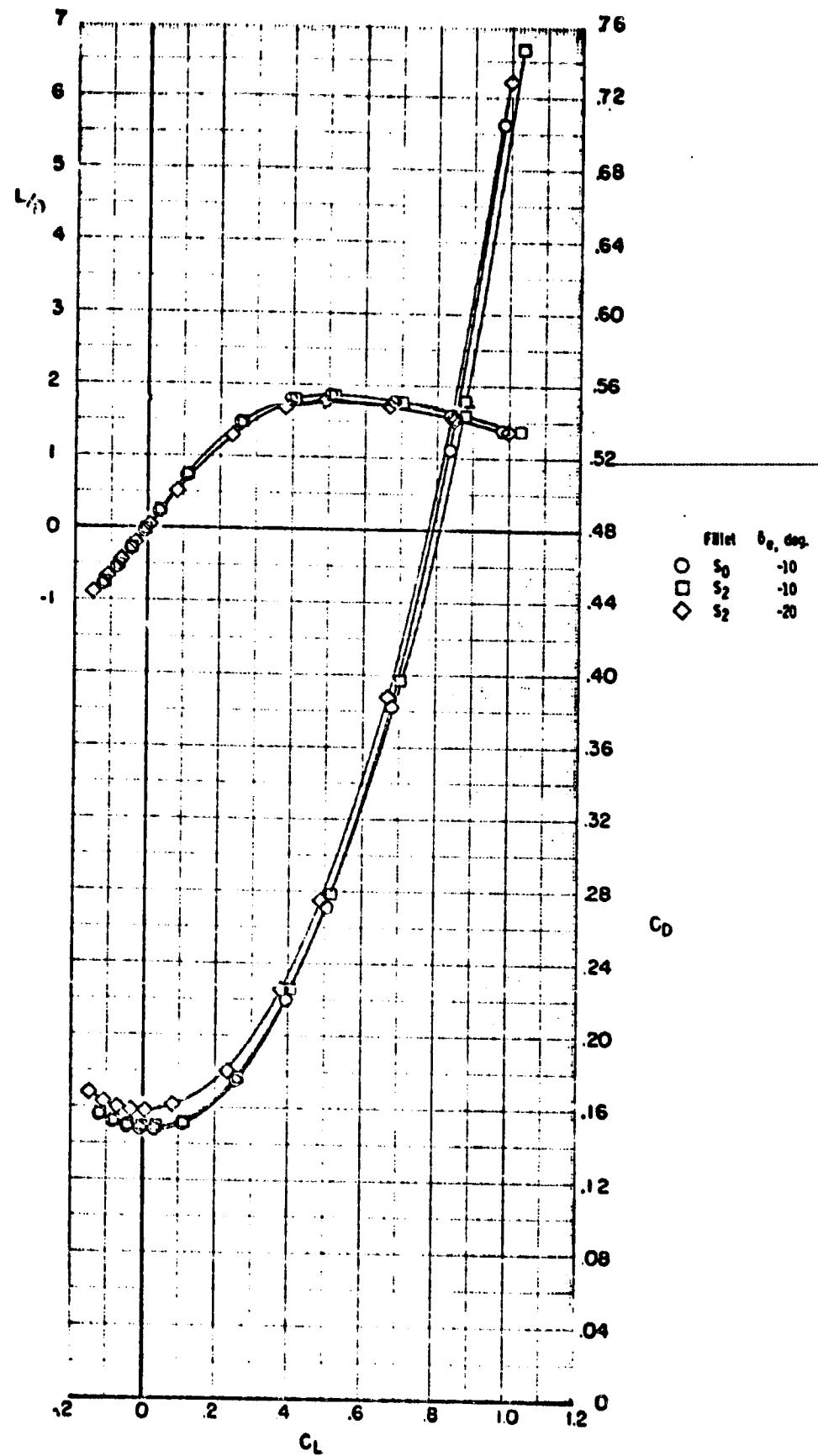
(a)  $M=1.5$   
 Figure 4. - Effect of fillet  $S_2$  on longitudinal  
 aerodynamic characteristics of configuration  $B_1^WVS_0EF$ .  
 $\delta_{BF} = -11.7^\circ$ ;  $\delta_{SB} = 55^\circ$ .



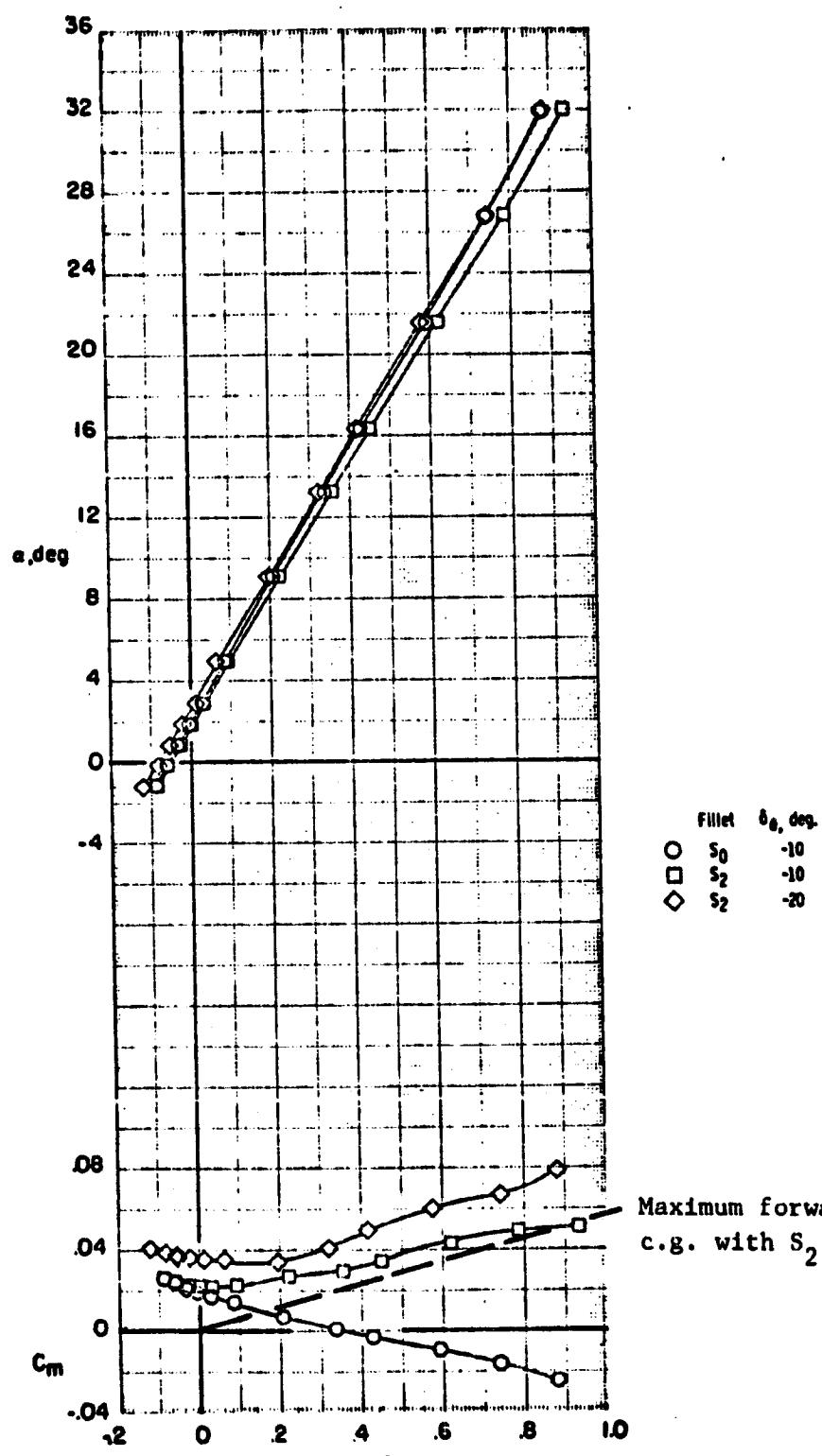
(a) Concluded.  
Figure 4. - Continued.



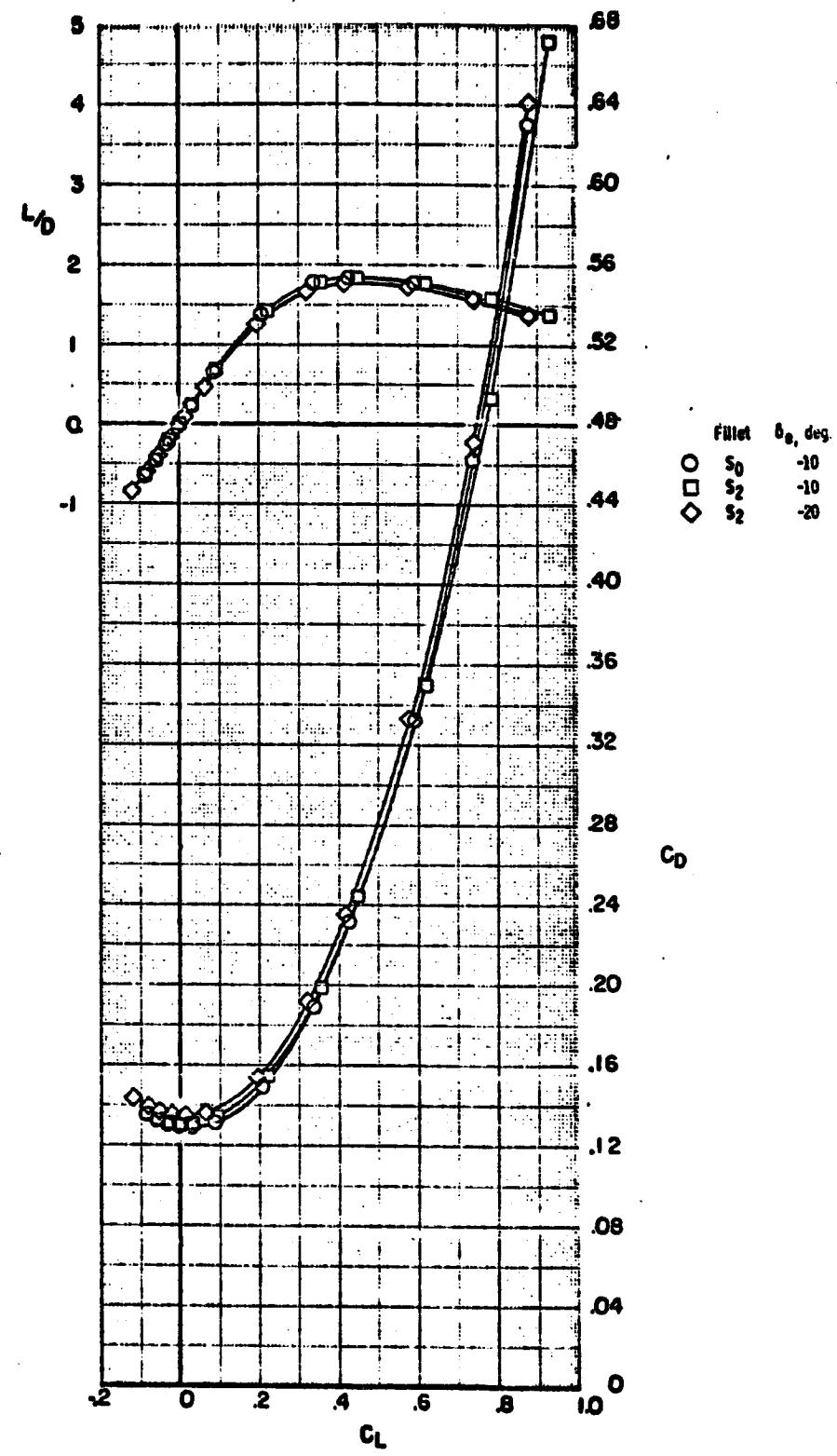
(b)  $M=2.0$   
Figure 4. - Continued.



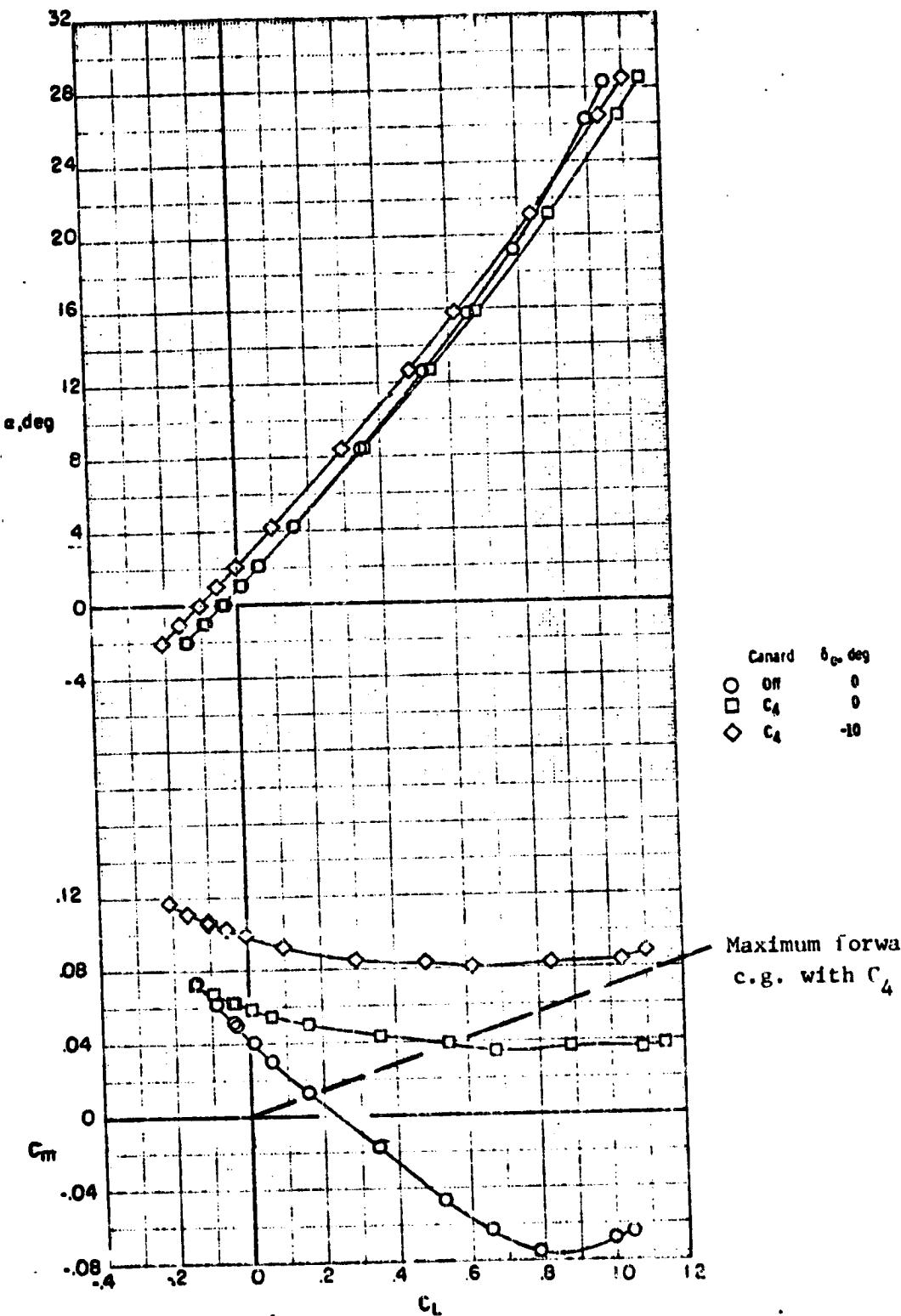
(b) Concluded.  
Figure 4. - Continued. 29



(c)  $M=2.5$   
Figure 4. - Continued.

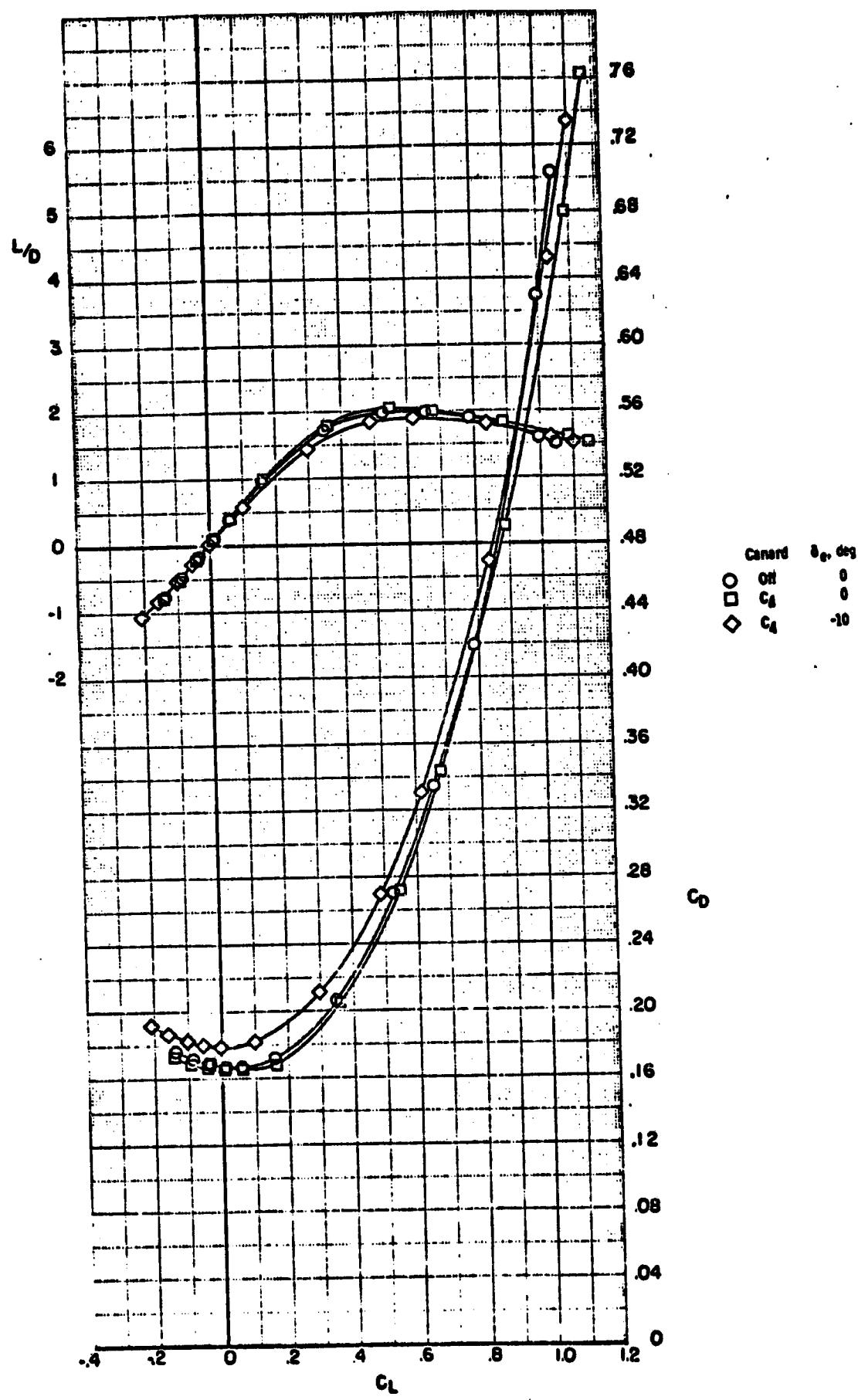


(c) Concluded.  
Figure 4. - Concluded.



(a)  $M=1.5$

Figure 5. - Effect of canard  $C_4$  on the longitudinal aerodynamic characteristics of configuration B<sub>1</sub>WVS<sub>0</sub>EF  
 $\alpha_f = -11.7^\circ$ ;  $\delta_{SB} = 55^\circ$



(a) Concluded.  
Figure 5. - Continued.

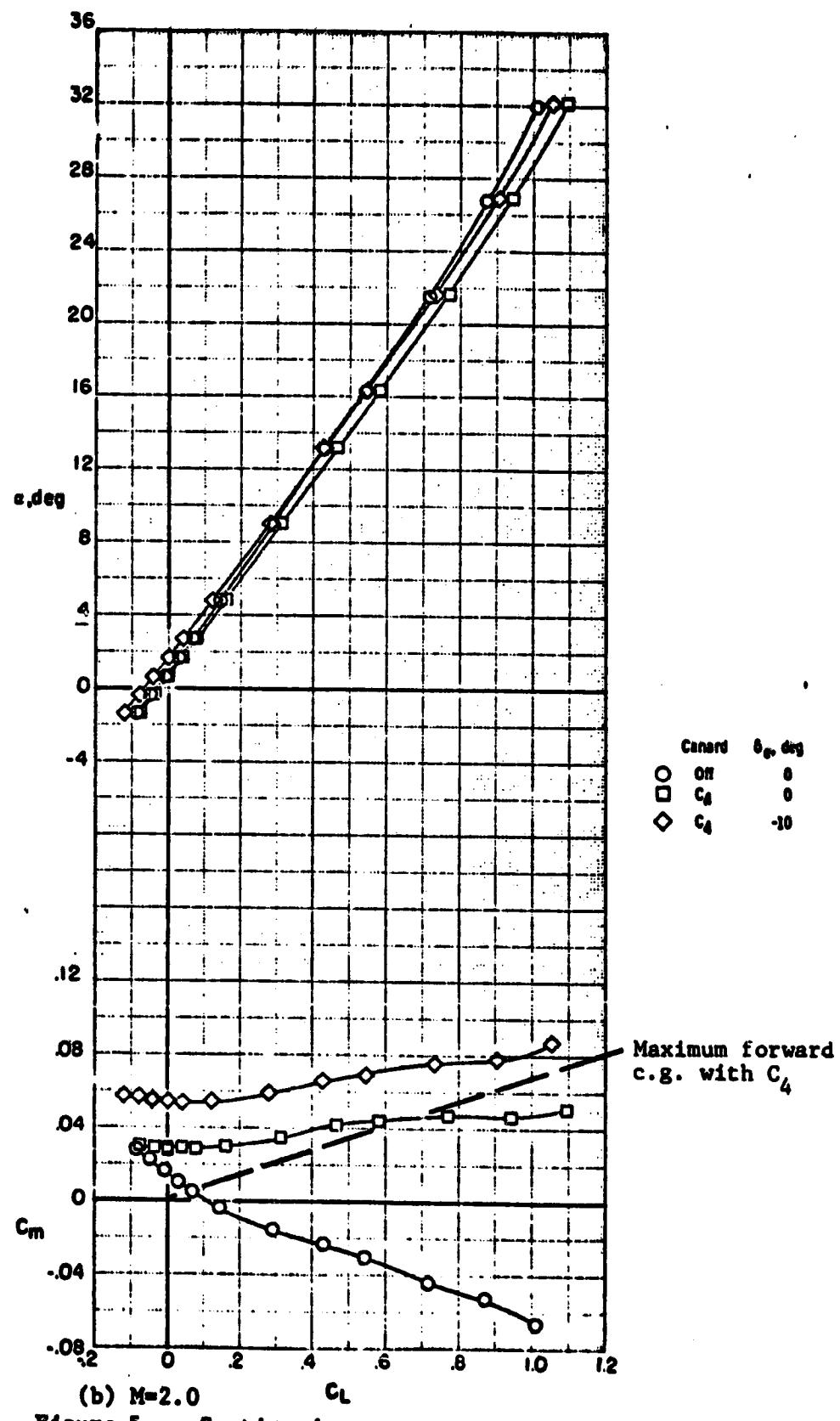
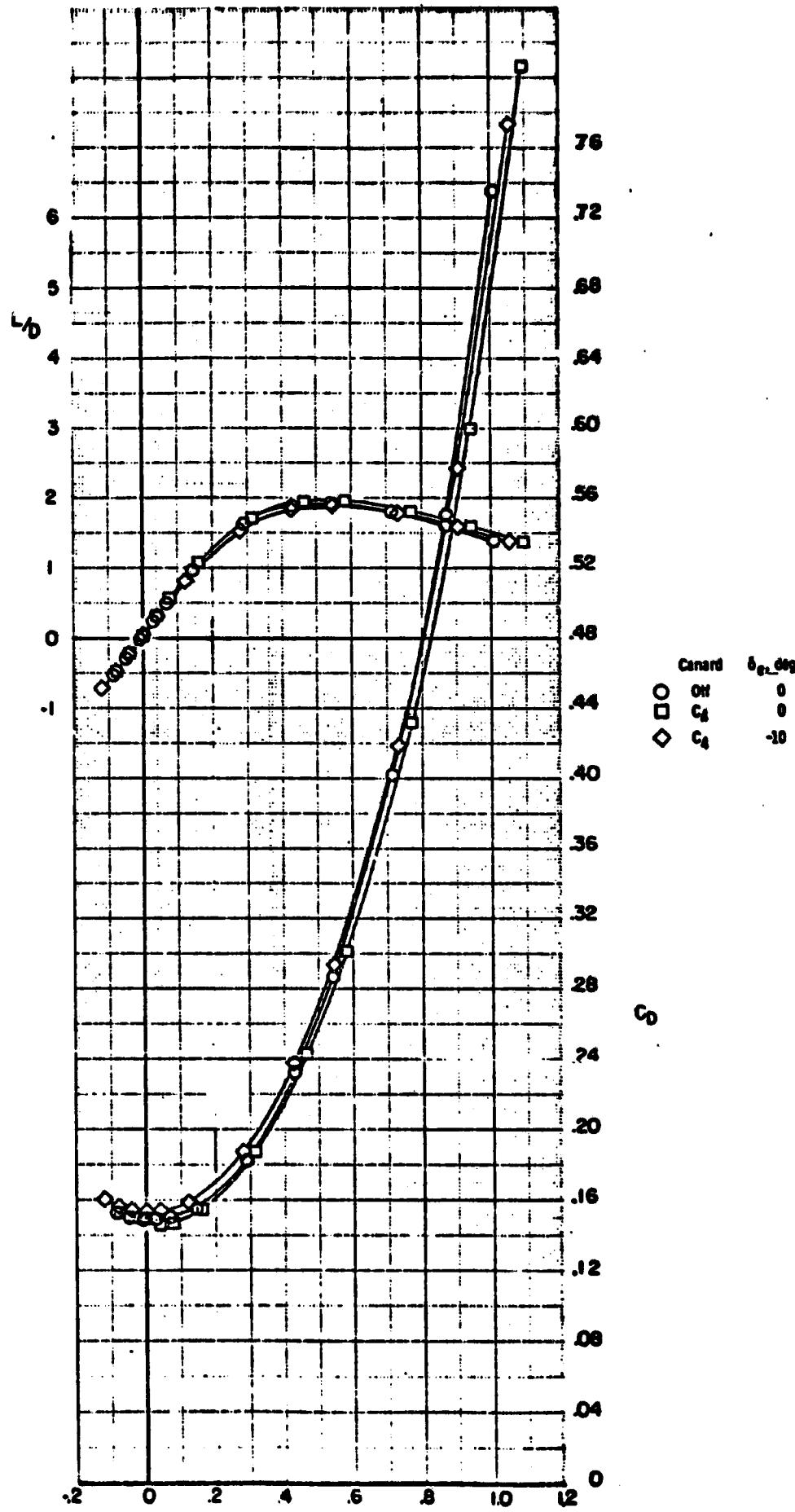
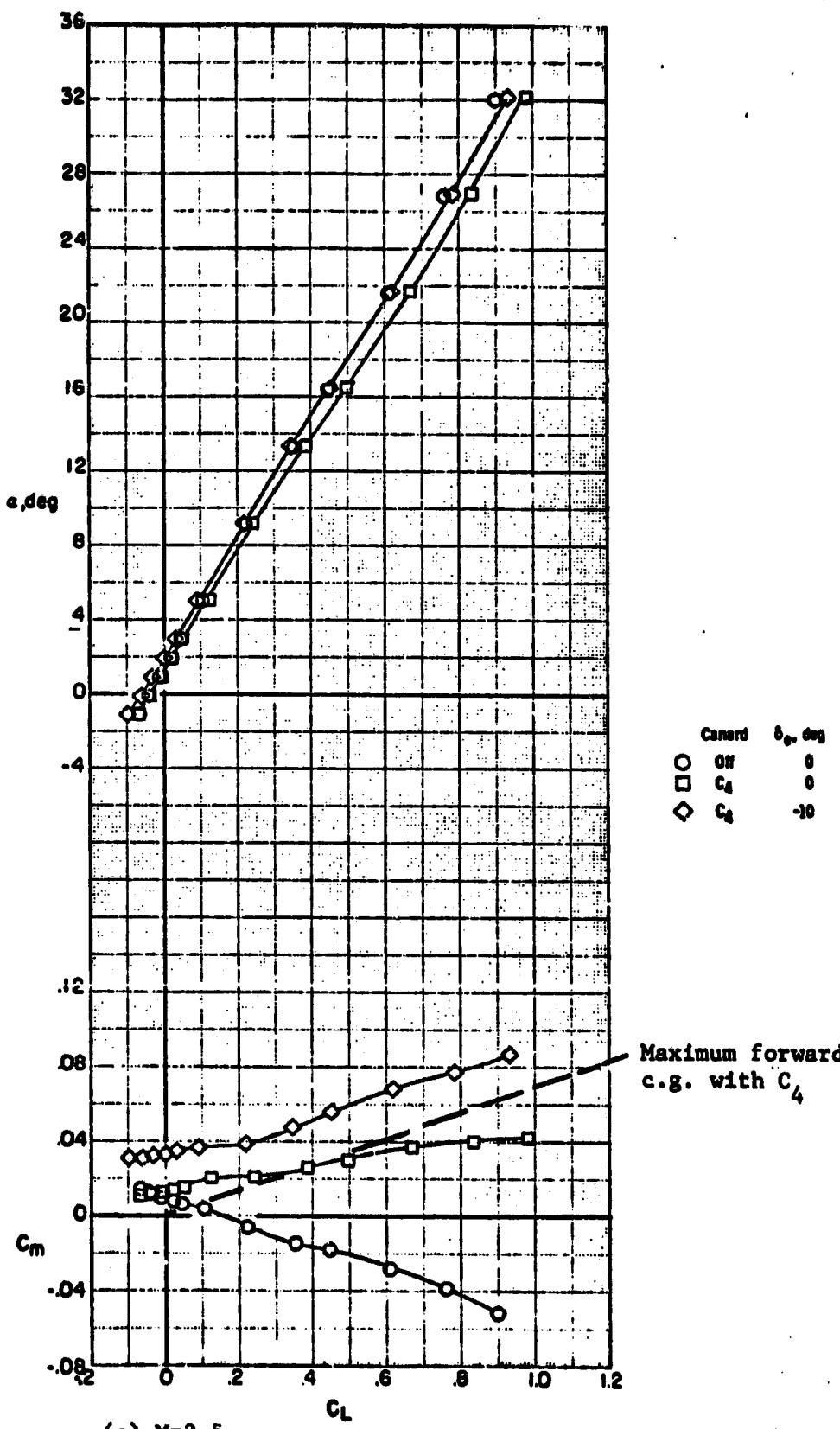


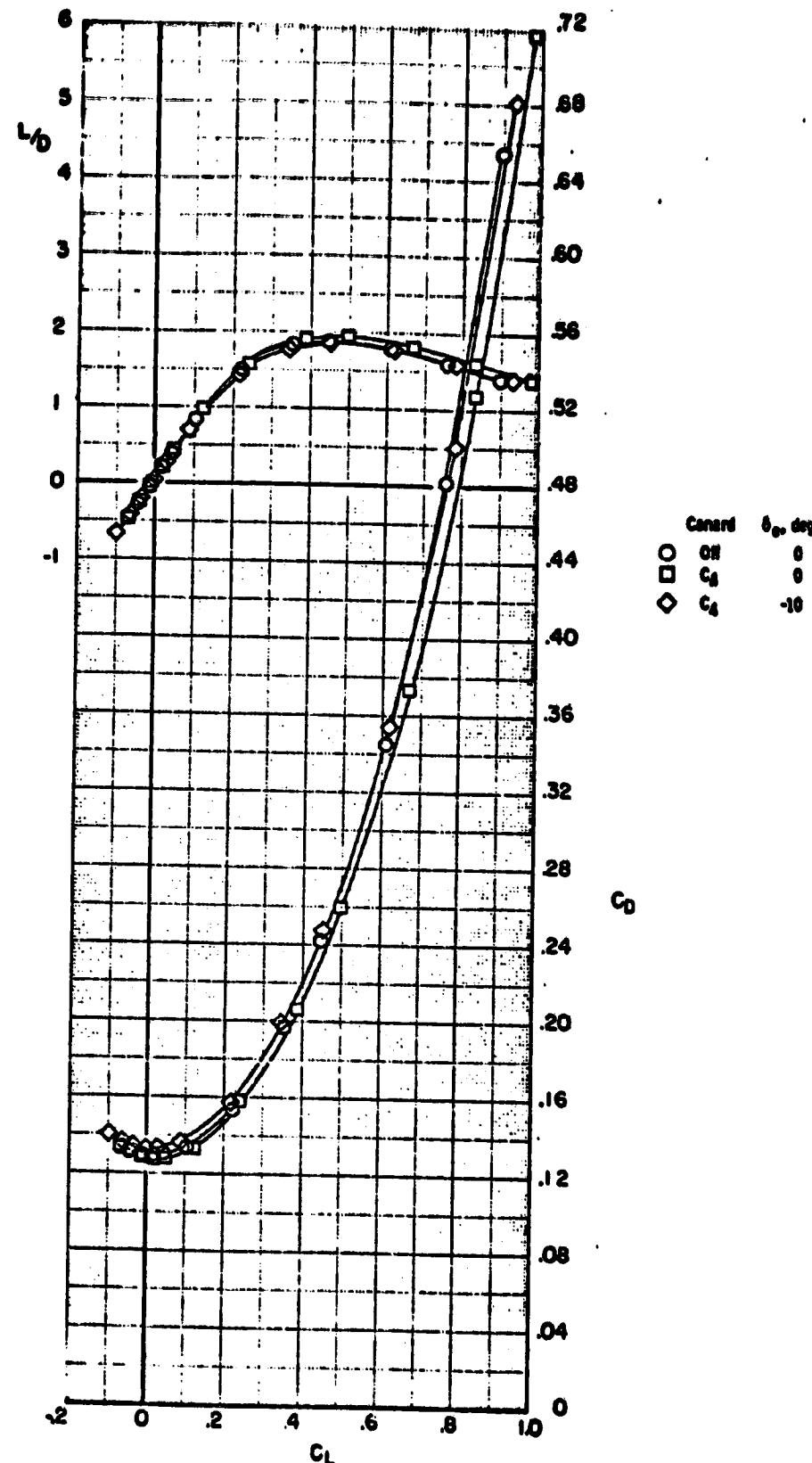
Figure 5. - Continued.



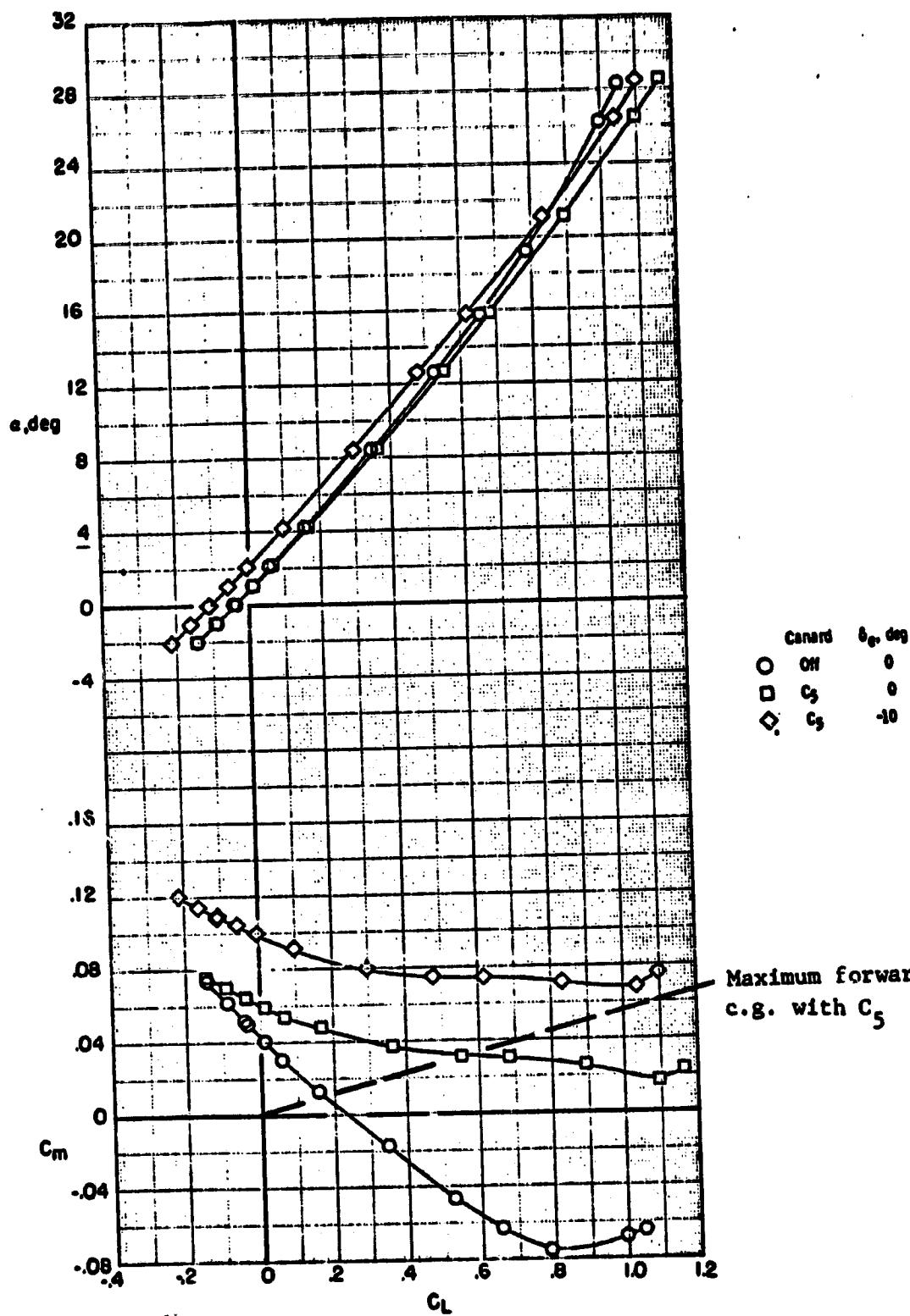
(b) Concluded.  
Figure 5. - Continued.



(c)  $M=2.5$   
Figure 5. - Continued.

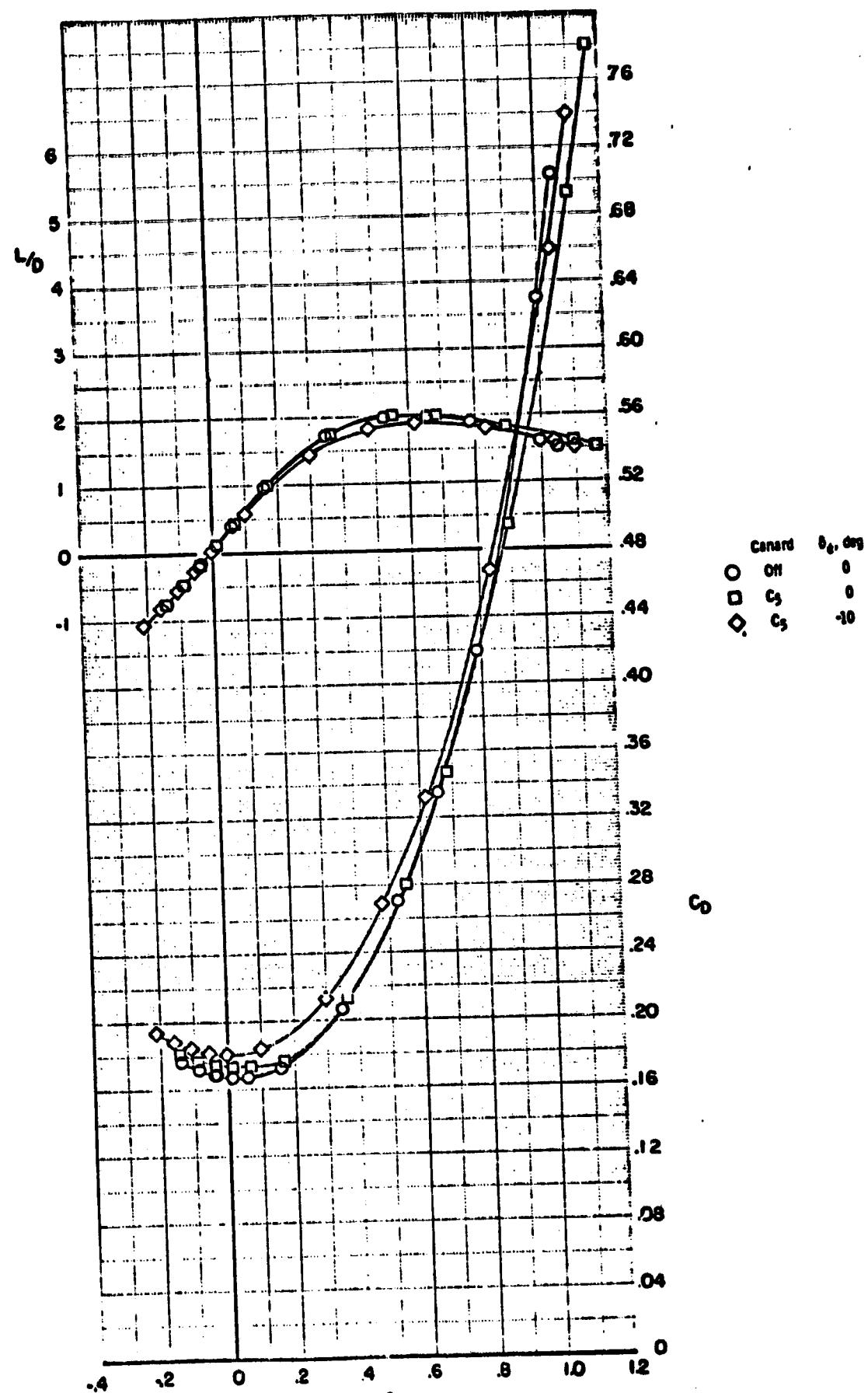


(c) Concluded.  
Figure 5. - Concluded.

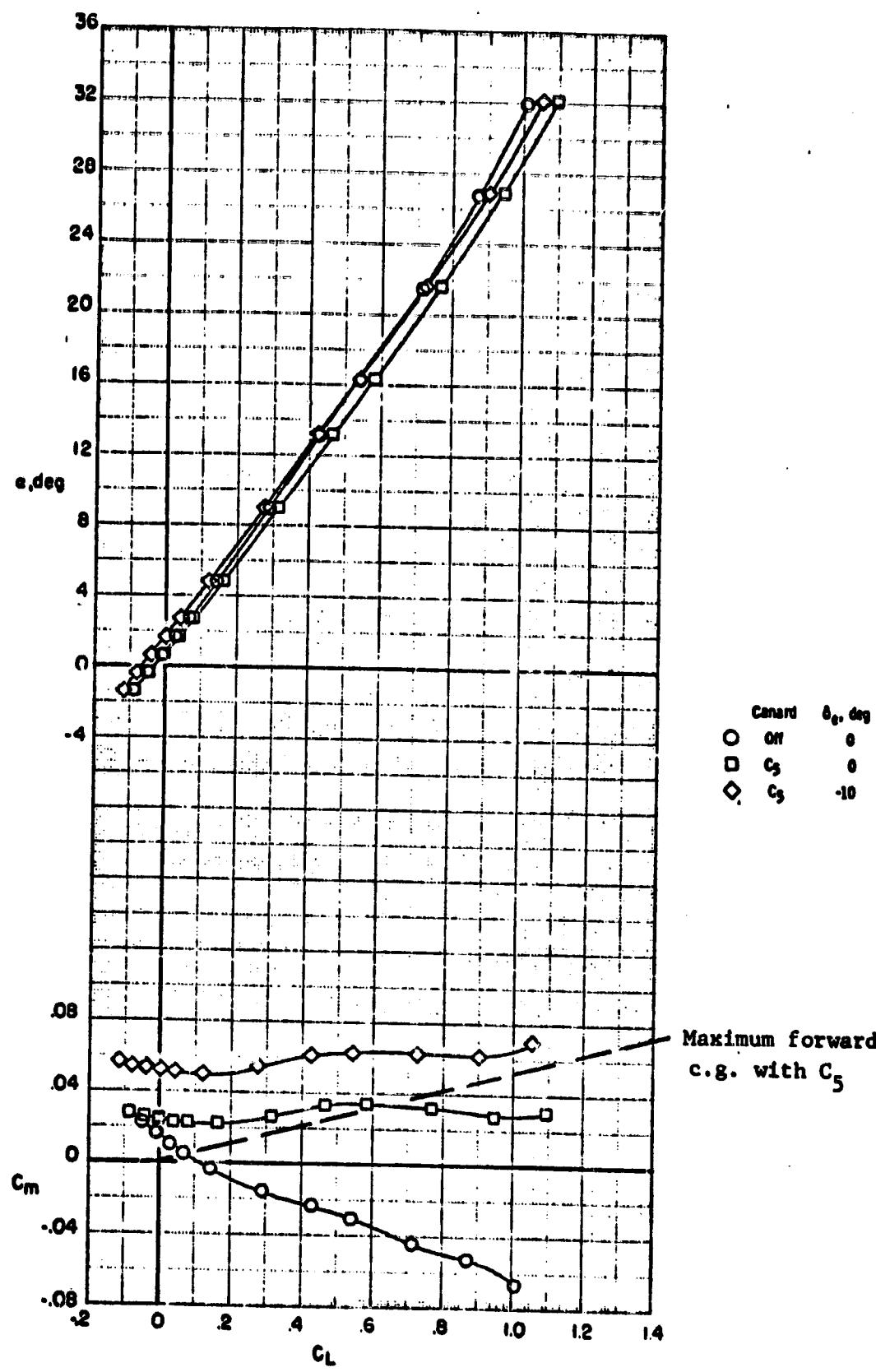


(a)  $M=1.5$

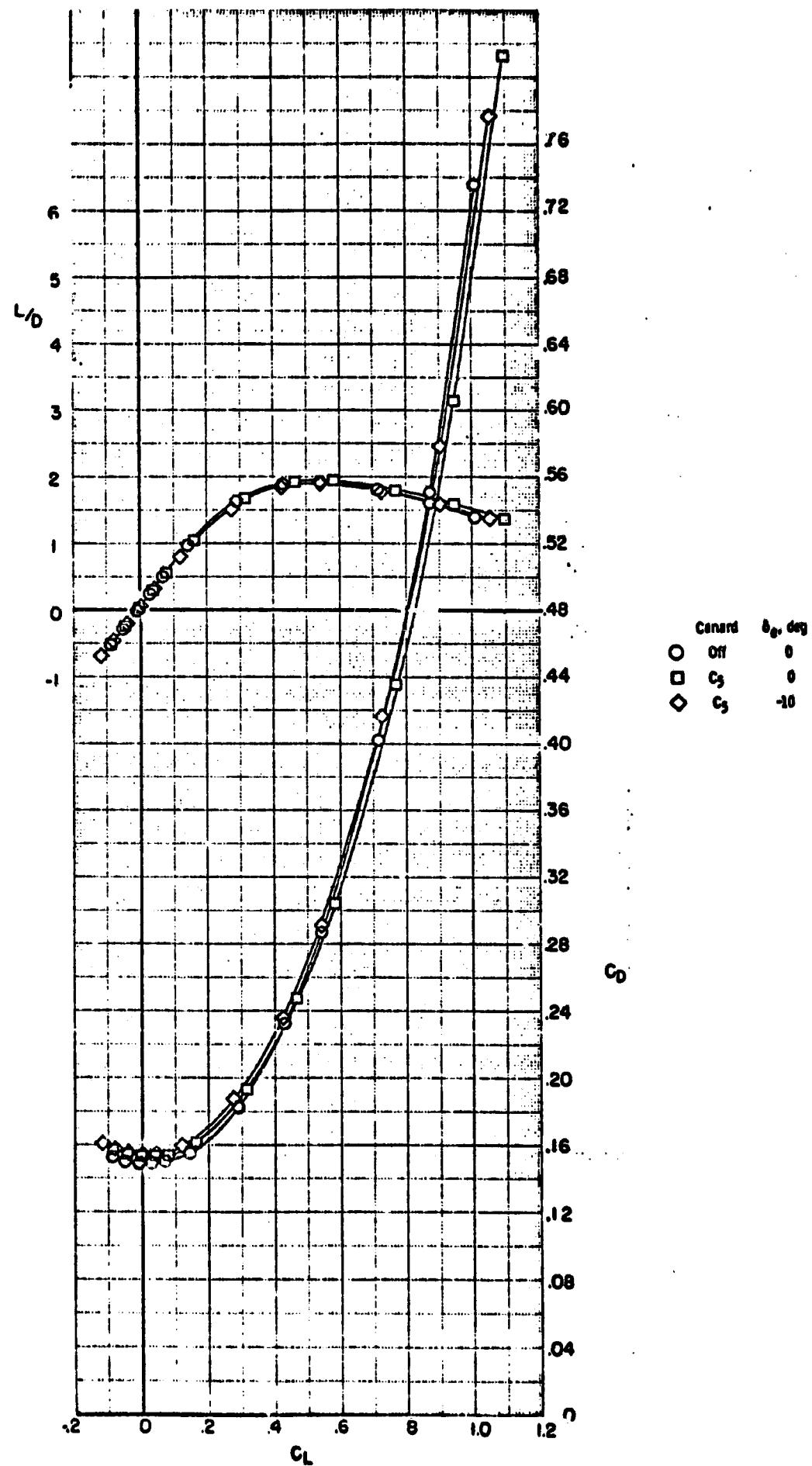
Figure 6. - Effect of canard  $C_5$  on the longitudinal aerodynamic characteristics of configuration  $B_1 WVS_0 EF$ .  $\delta_{BF} = -11.7^\circ$ ;  $\delta_{SB} = 55^\circ$



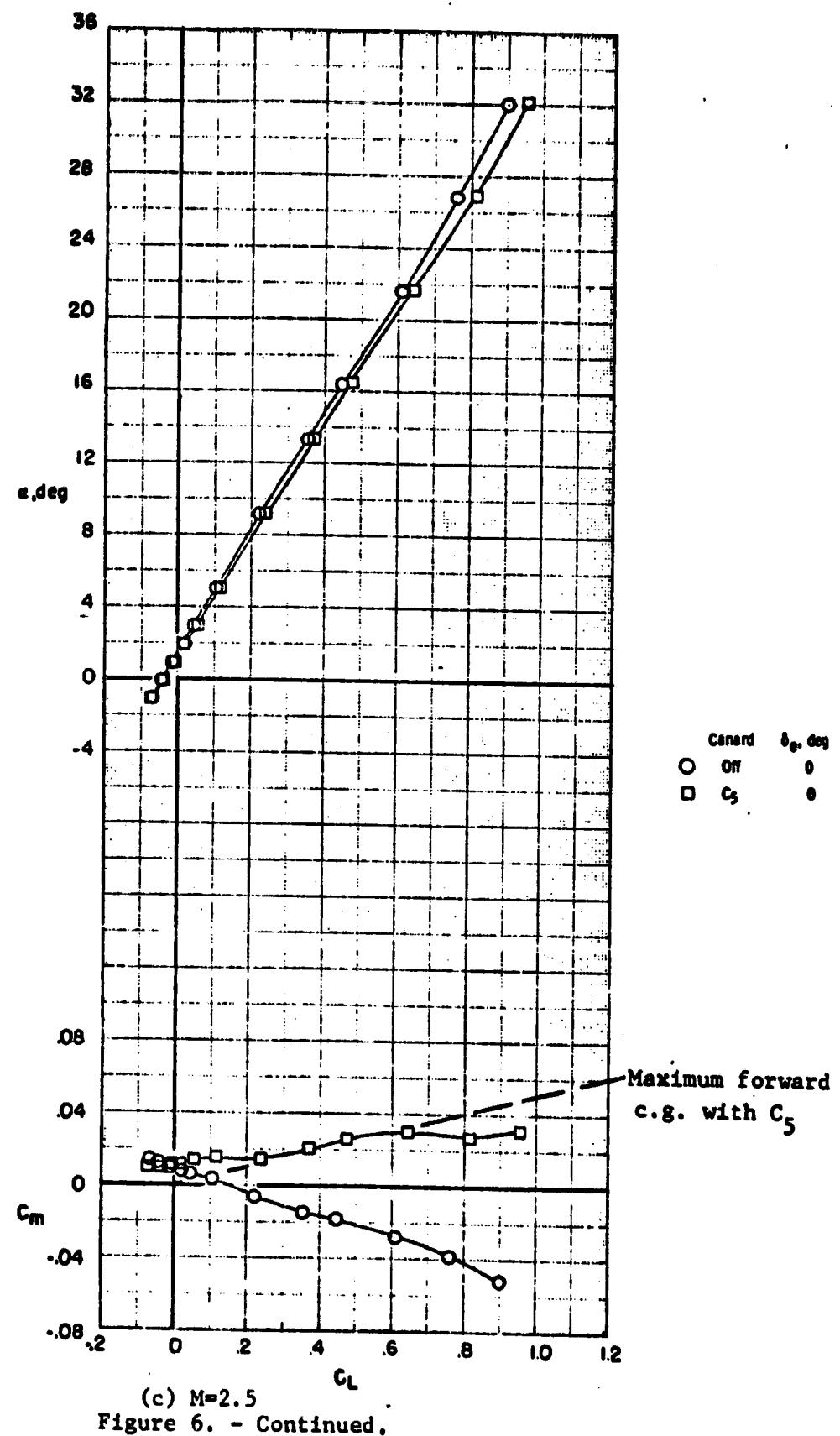
(a) Concluded.  
Figure 6. - Continued.



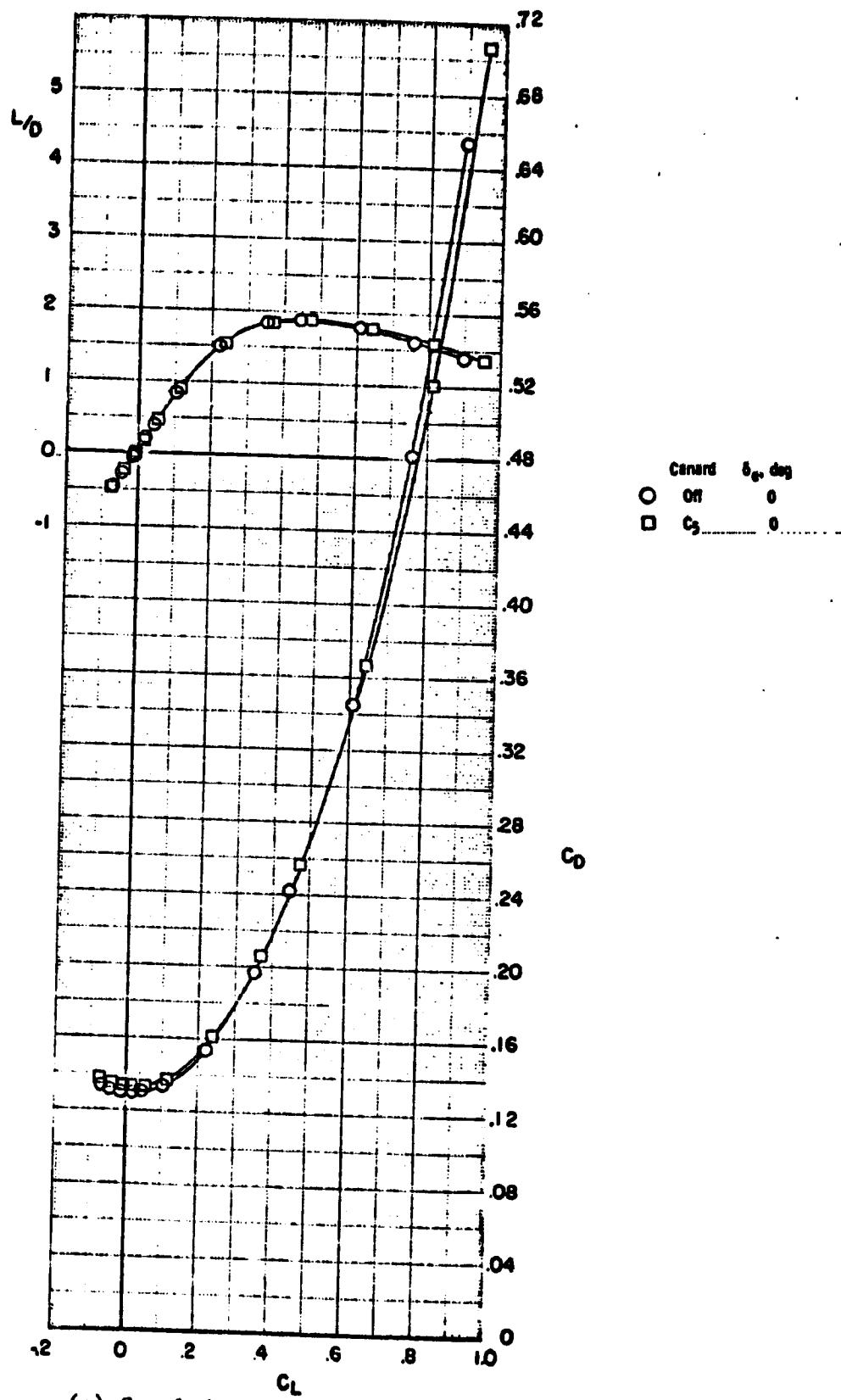
(b) M=2.0  
Figure 6. - Continued.



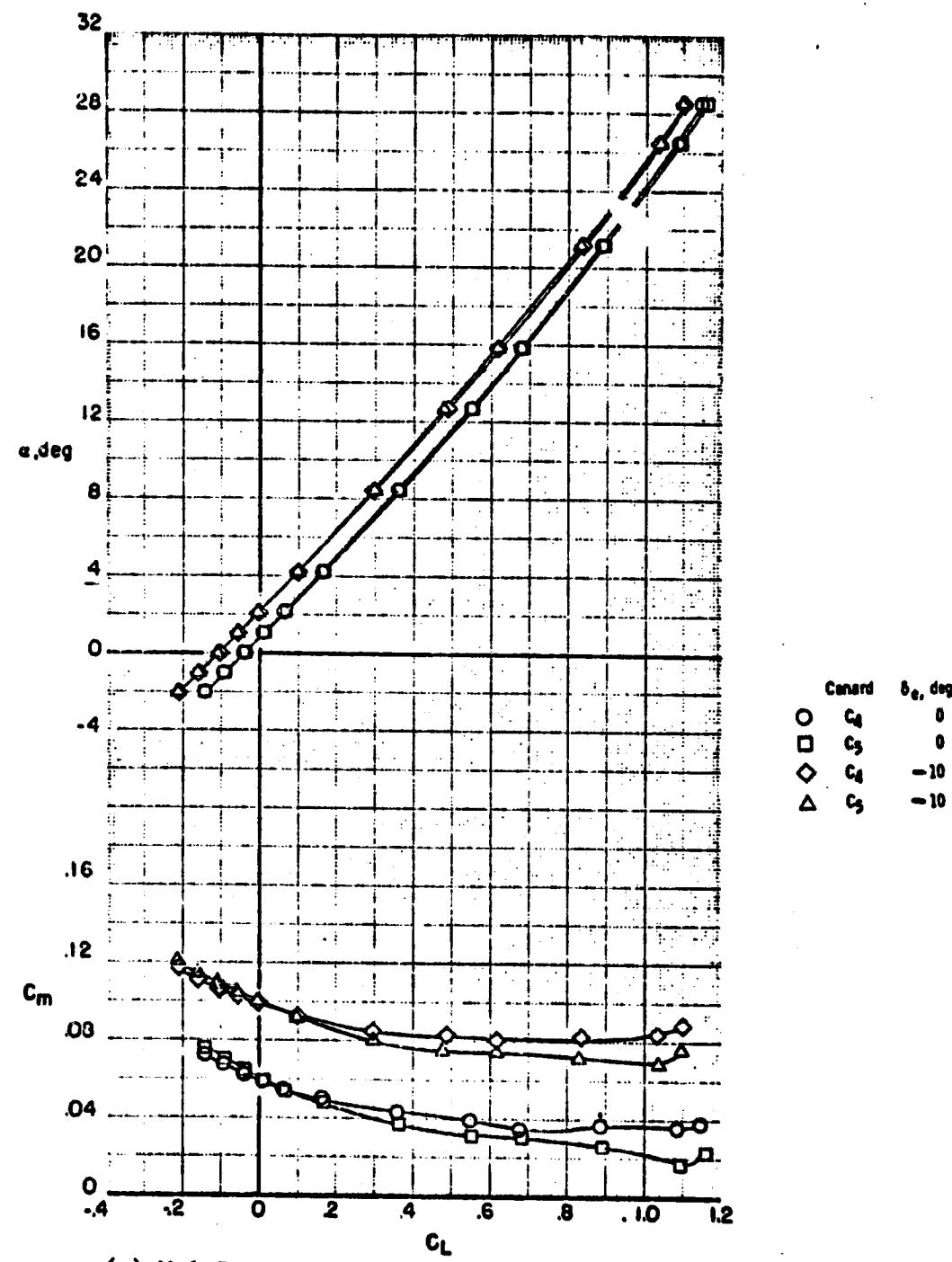
(b) Concluded.  
Figure 6. - Continued.



(c)  $M=2.5$   
Figure 6. - Continued.

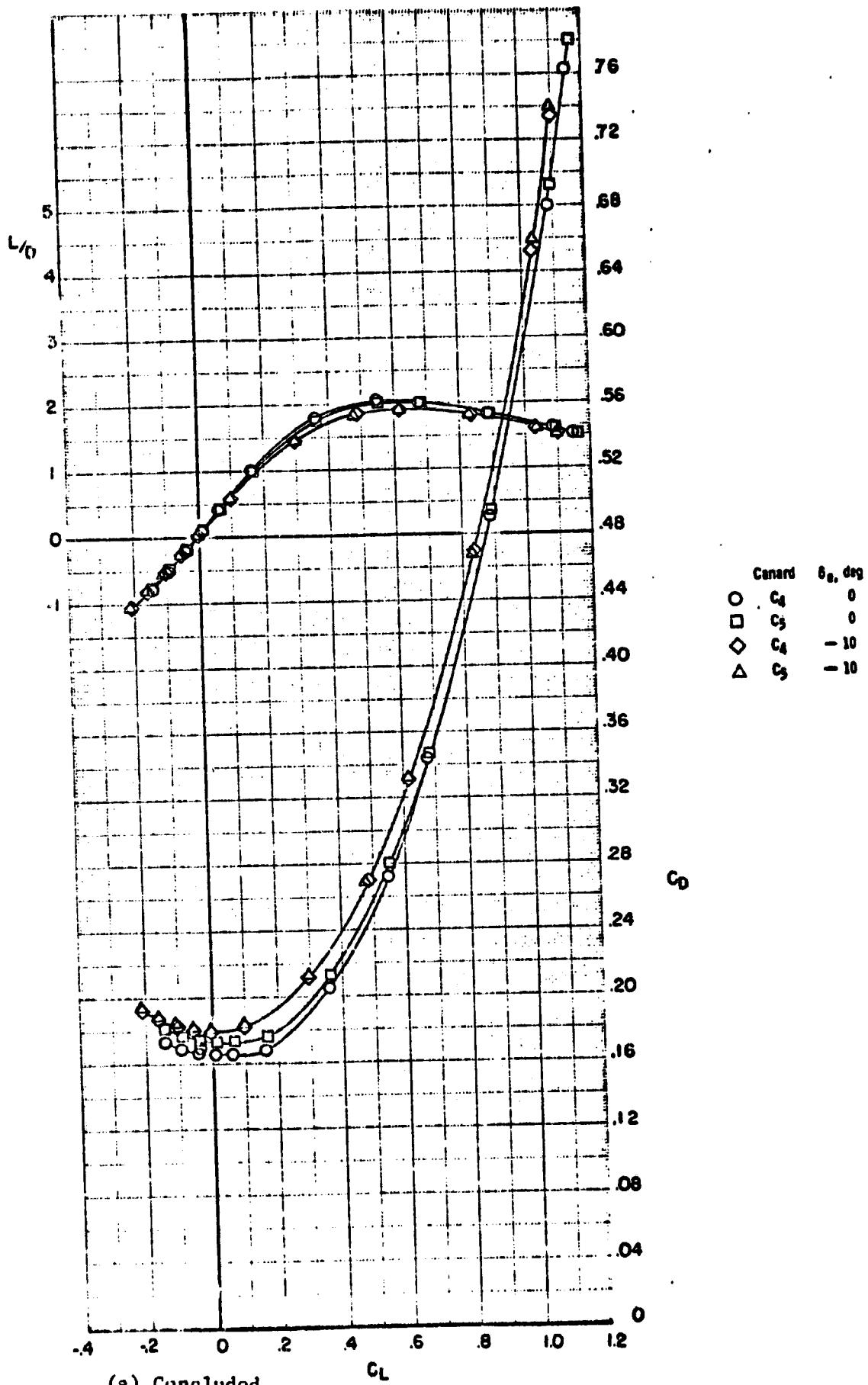


(c) Concluded.  
Figure 6. - Concluded.

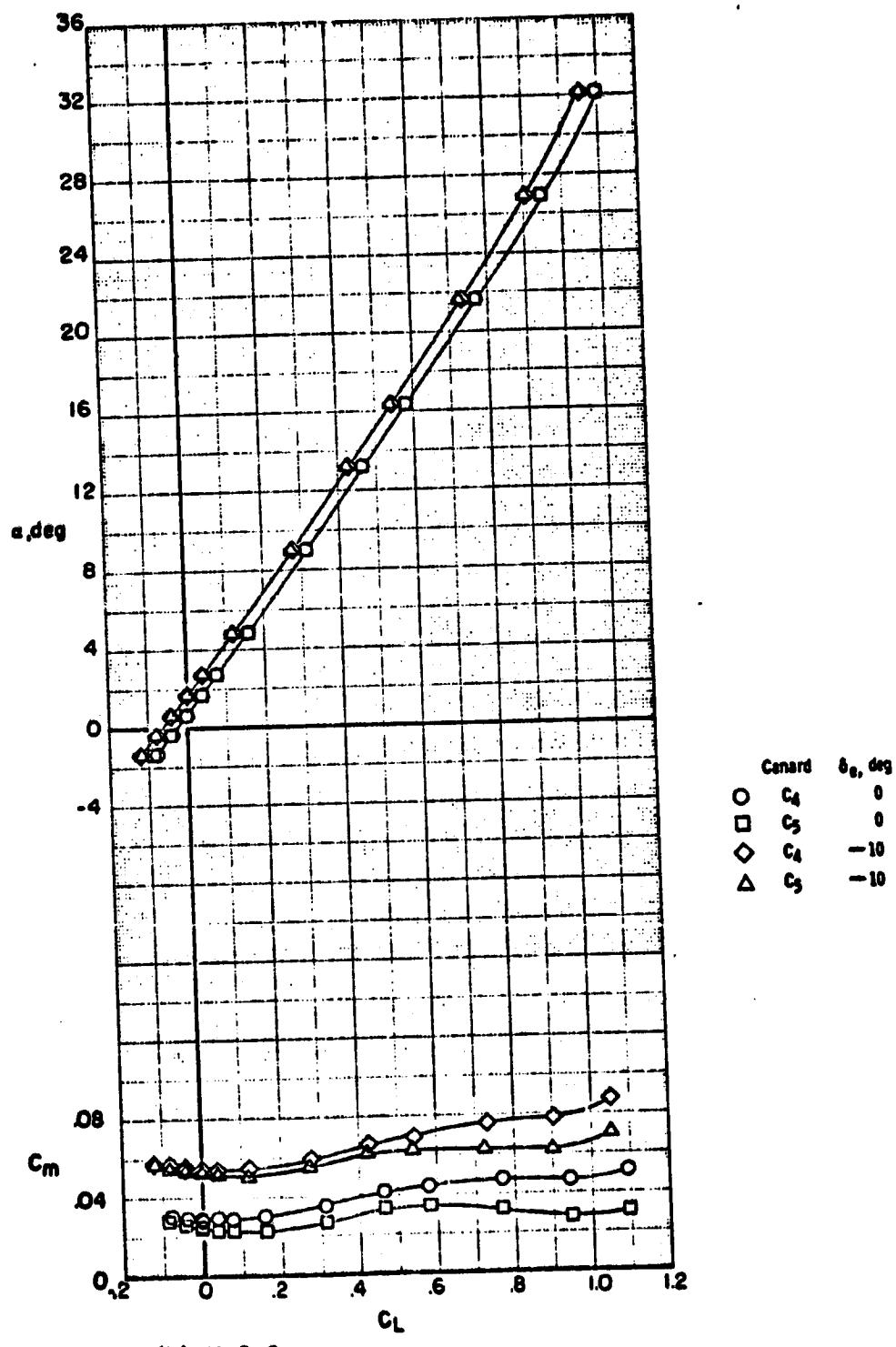


(a)  $M=1.5$

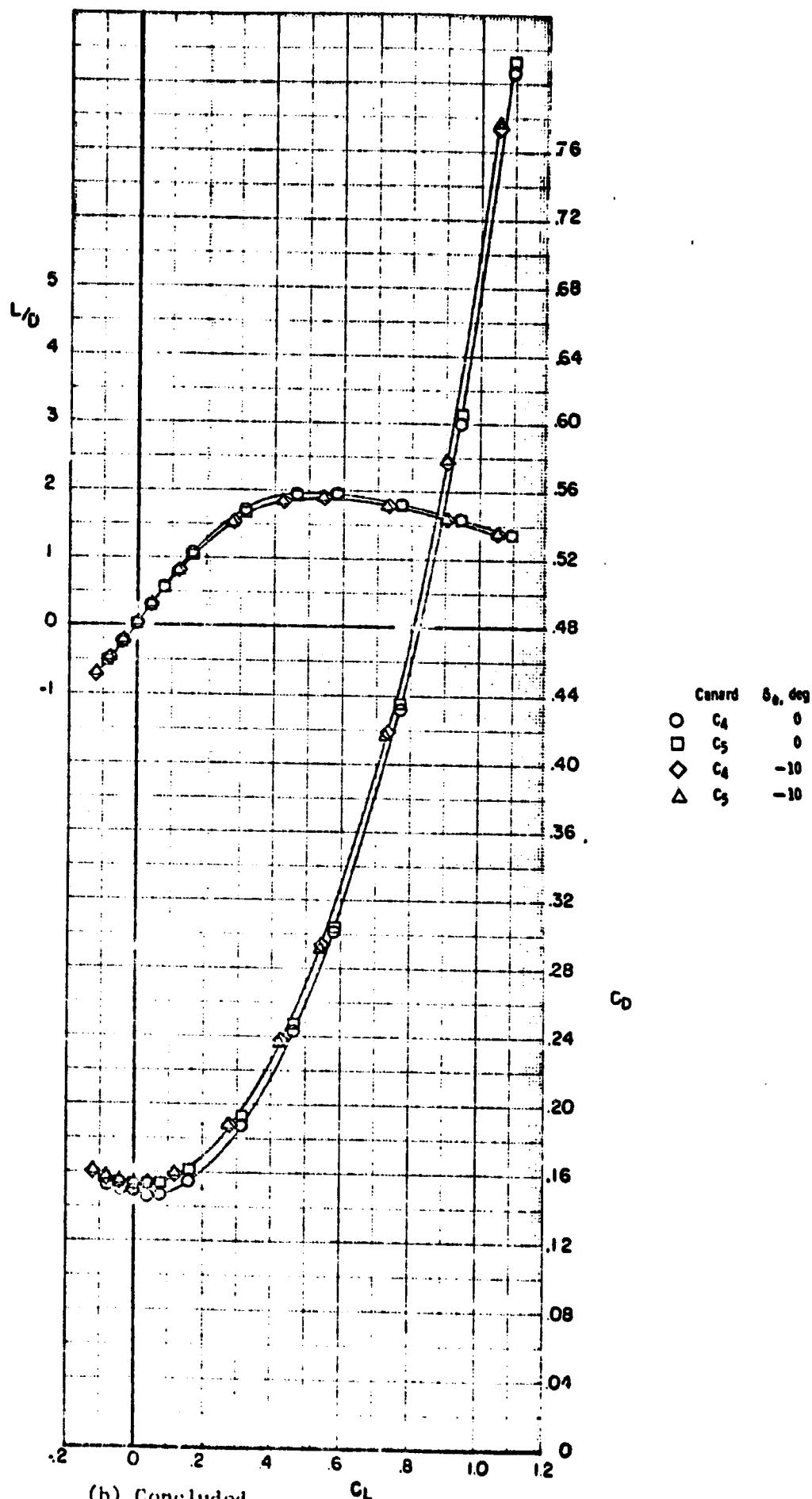
Figure 7. - Longitudinal aerodynamic characteristics of configurations  $B_1WVS_0C_4$  EF and  $B_1WVS_0C_5$  EF.  $\delta_{BF} = -11.7^\circ$ ;  $\delta_{SB} = 59^\circ$



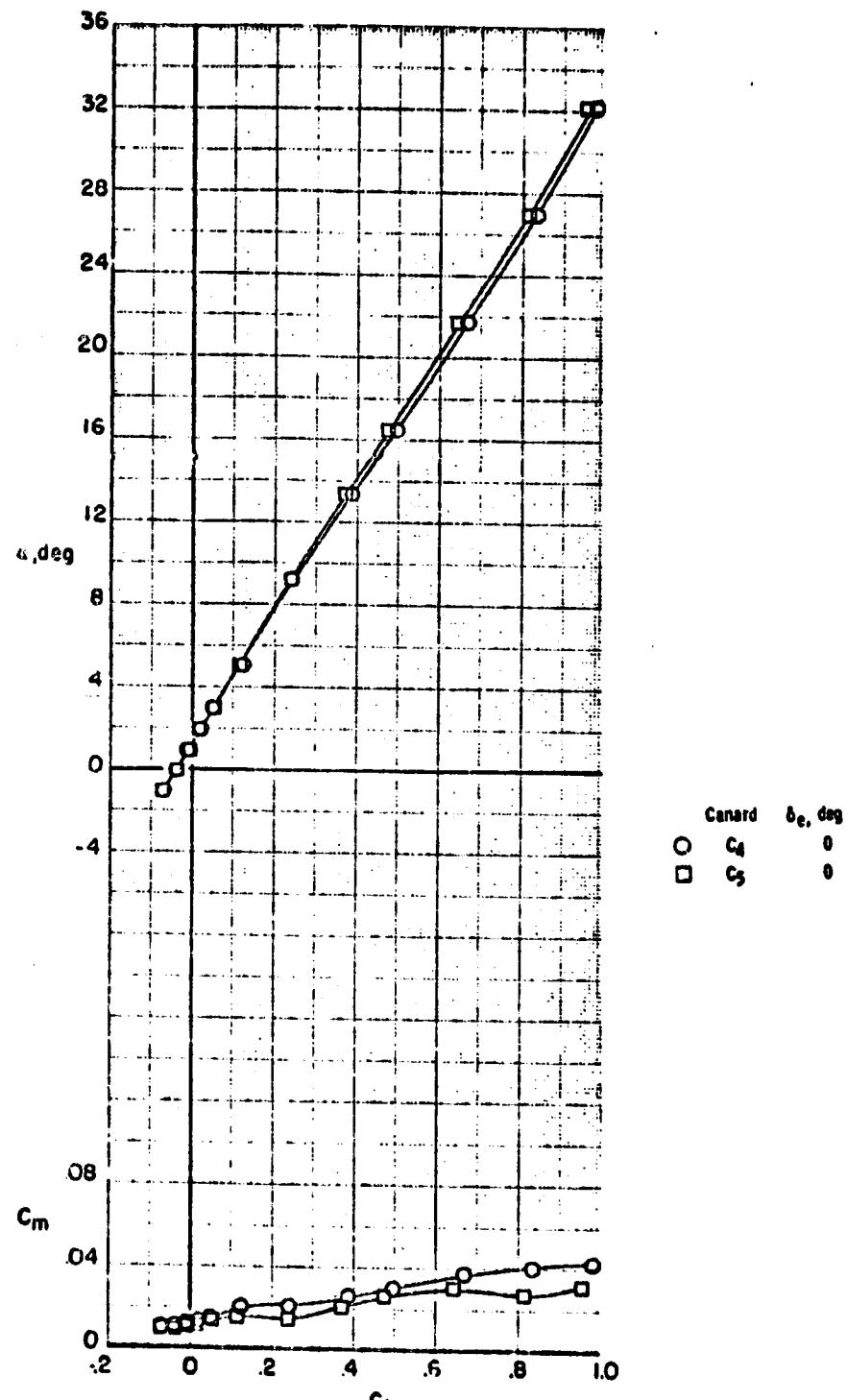
(a) Concluded.  
Figure 7. - Continued.



(b)  $M=2.0$   
Figure 7. - Continued.

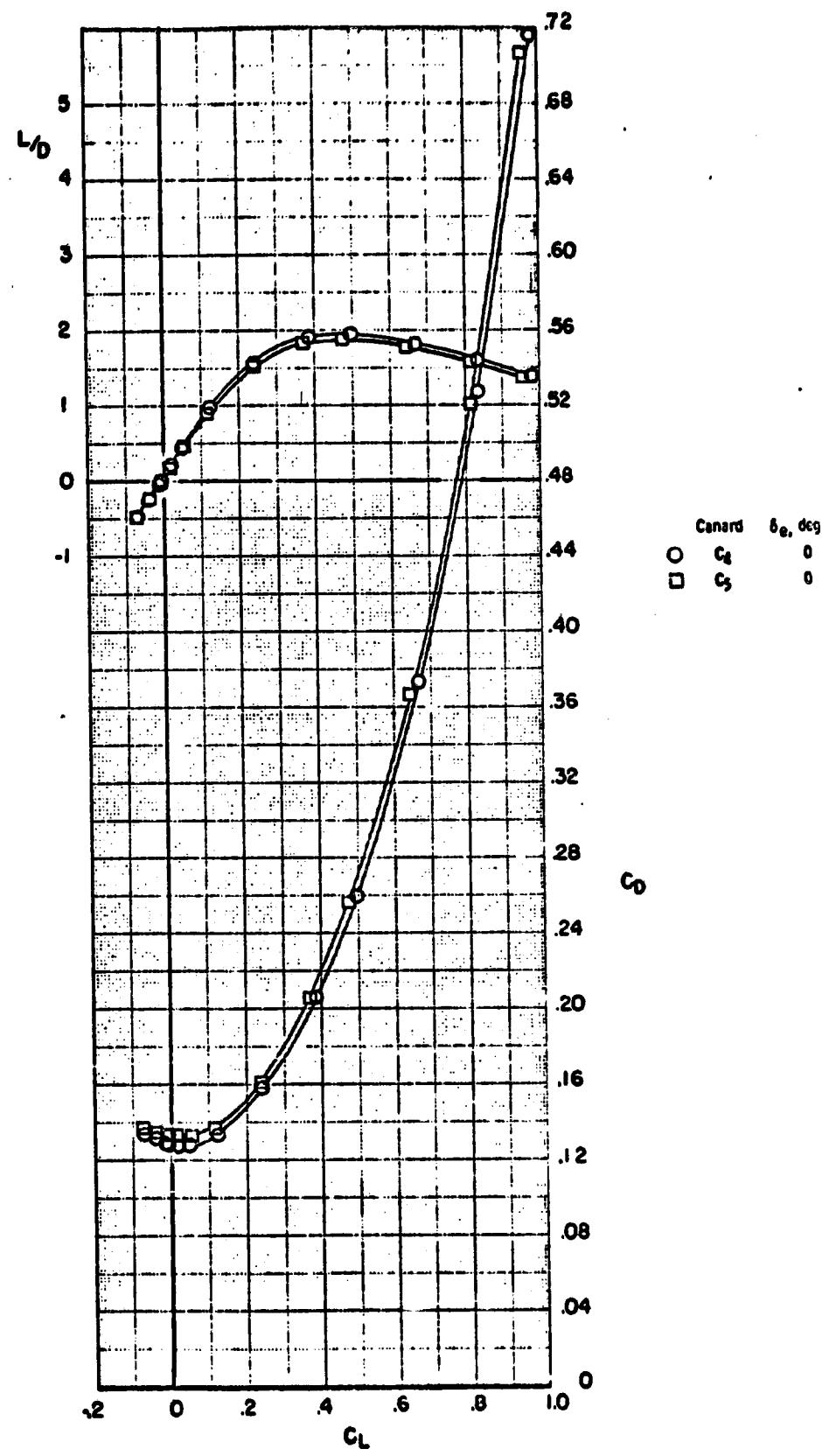


(b) Concluded.  
Figure 7. - Continued.

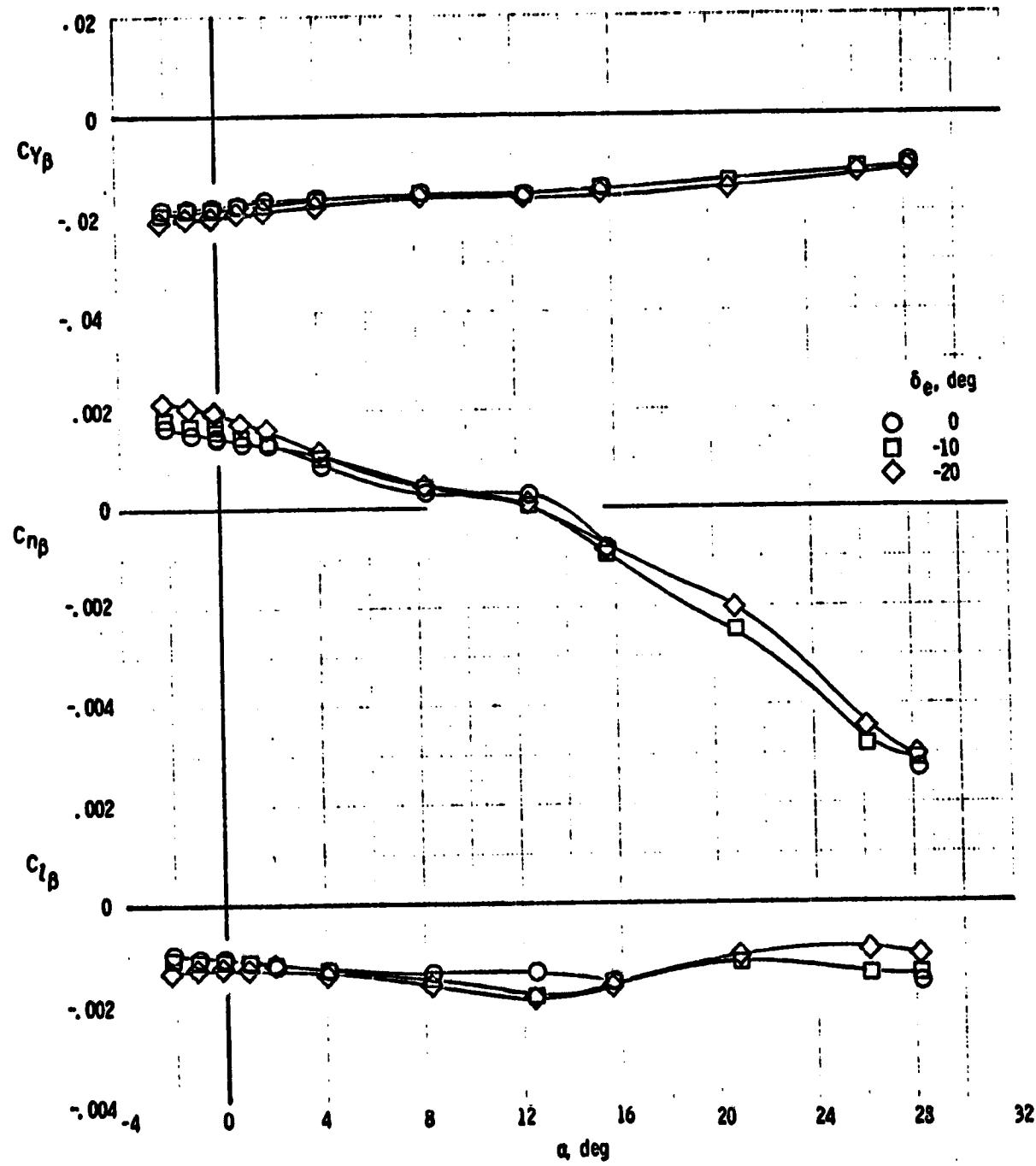


(c)  $M=2.5$

Figure 7. - Continued.

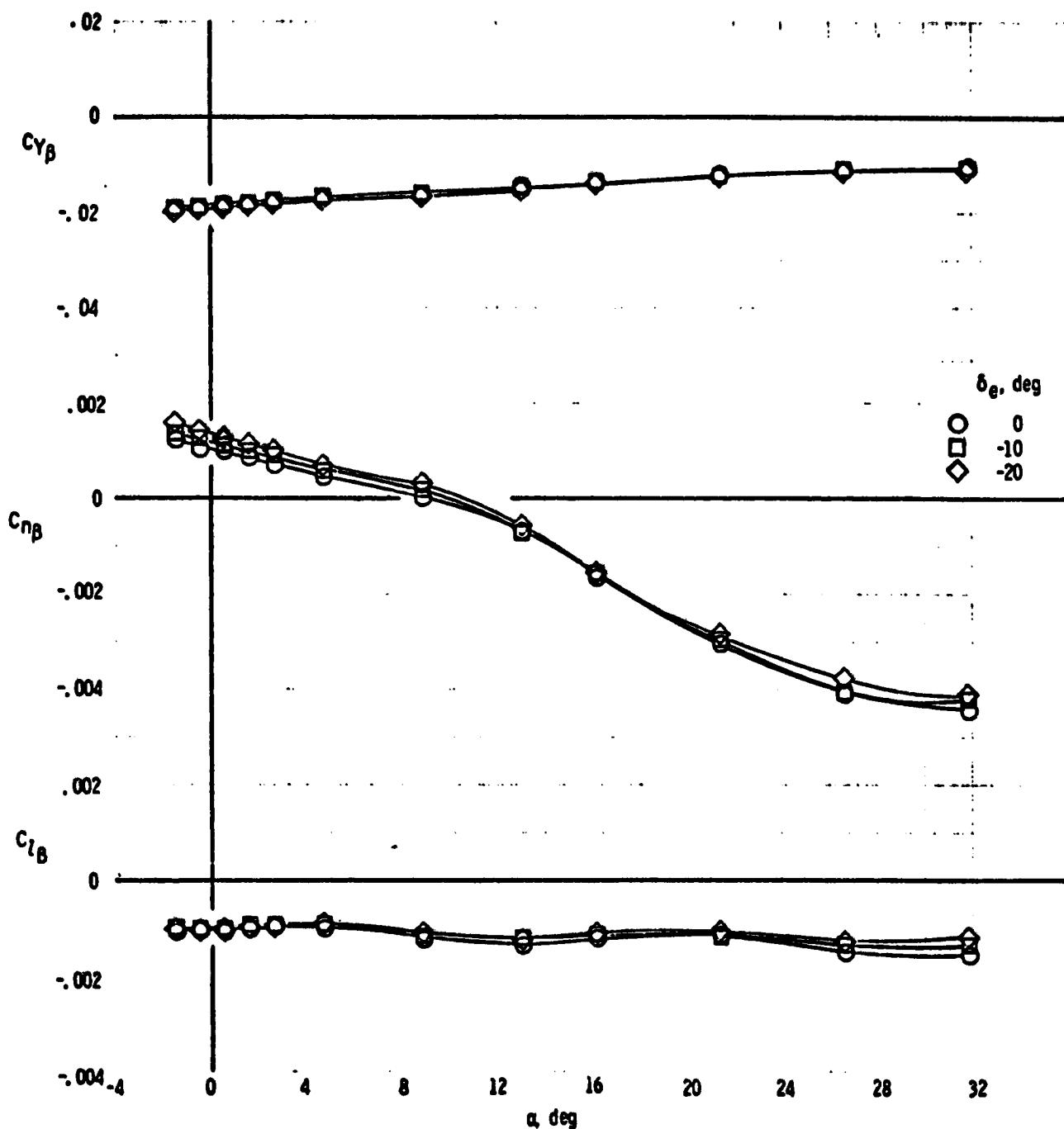


(c) Concluded.  
Figure 7. - Concluded.



(a)  $M=1.5$

Figure 8. - Lateral-directional characteristics  
for configuration  $B_1WVS_0EF$   $\delta_{BF}=-11.7^\circ$ ;  $\delta_{SB}=55^\circ$



(b)  $M=2.0$   
Figure 8. - Continued.

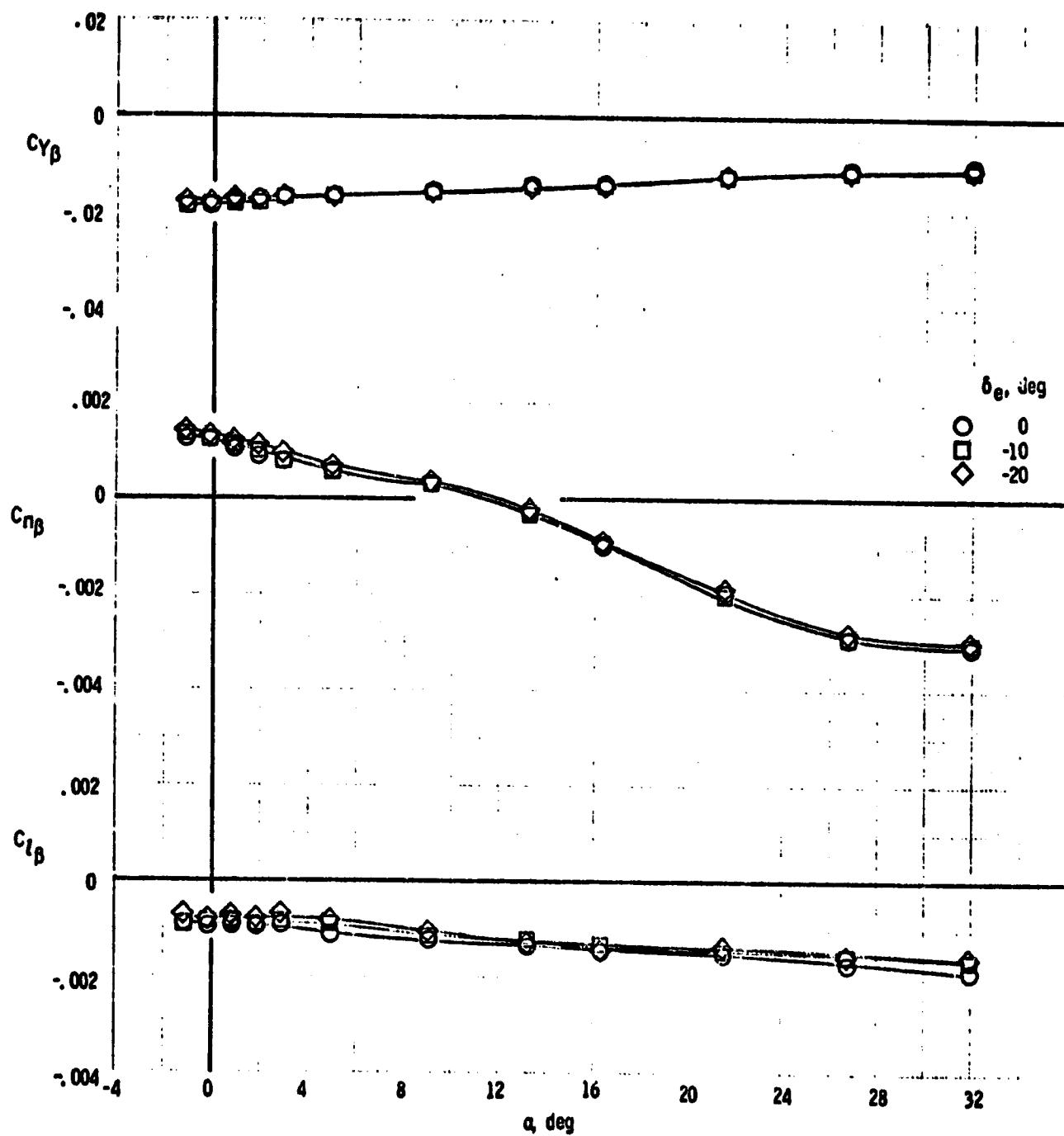
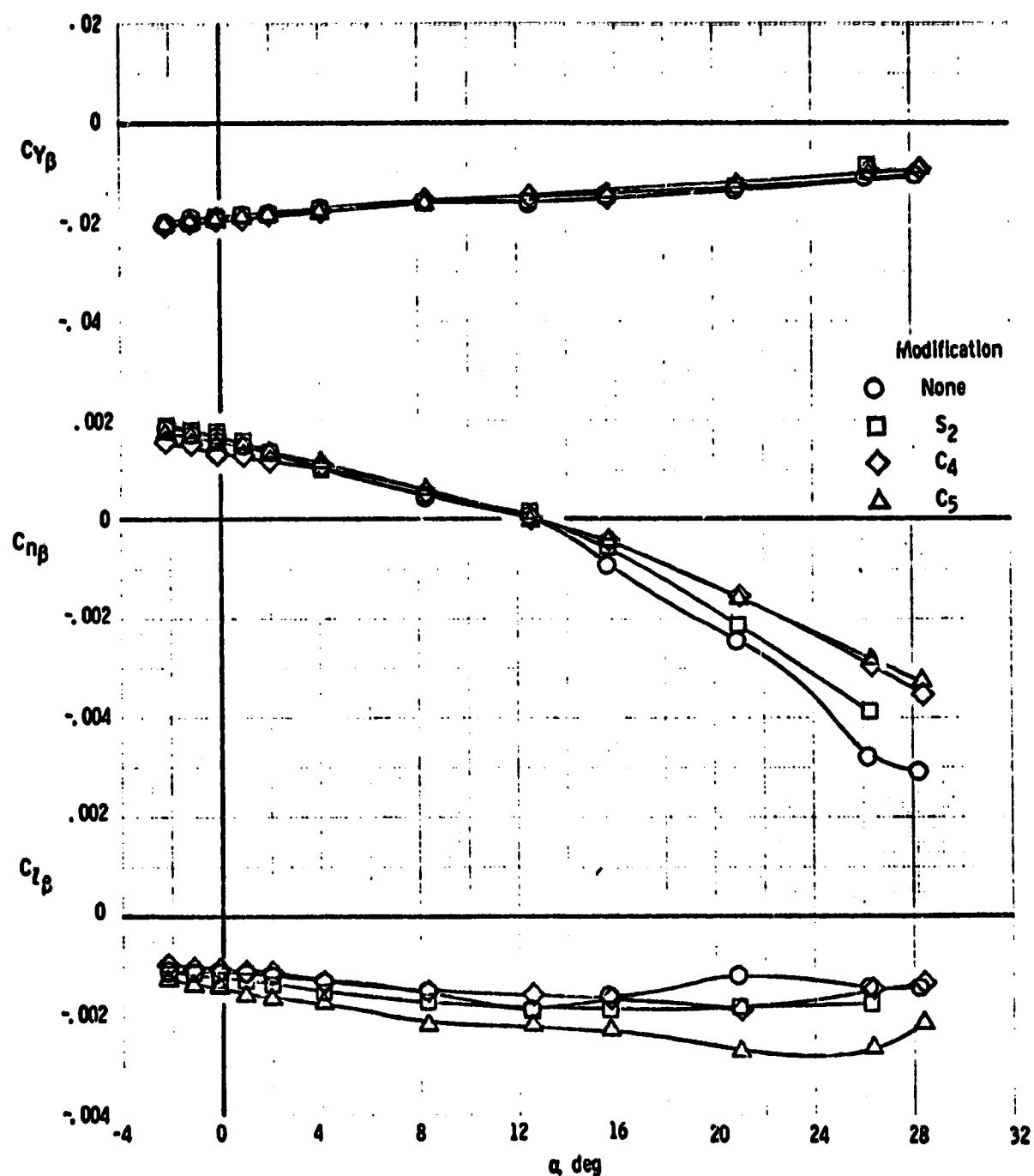
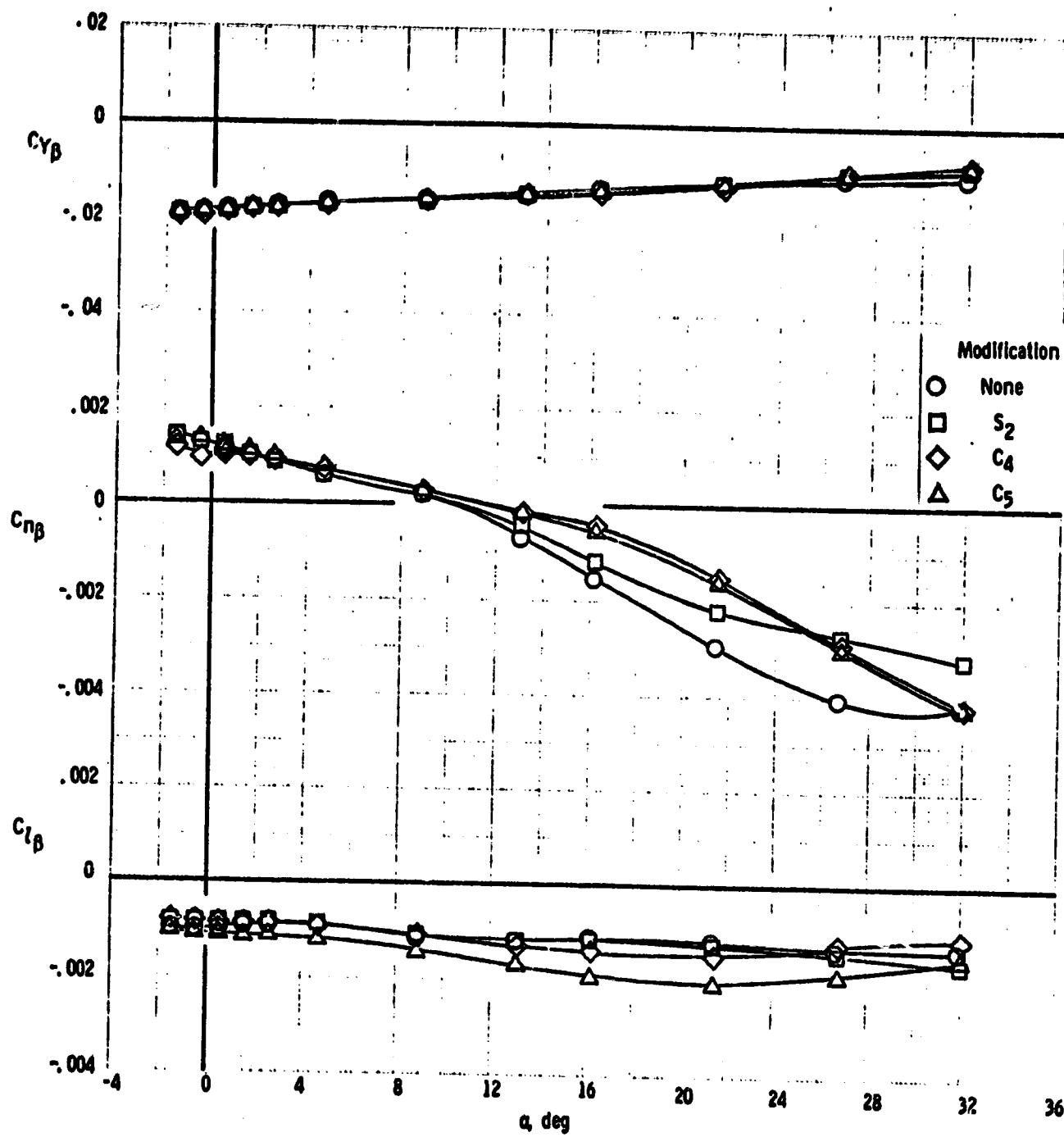
(c)  $M=2.5$ 

Figure 8. - Concluded.

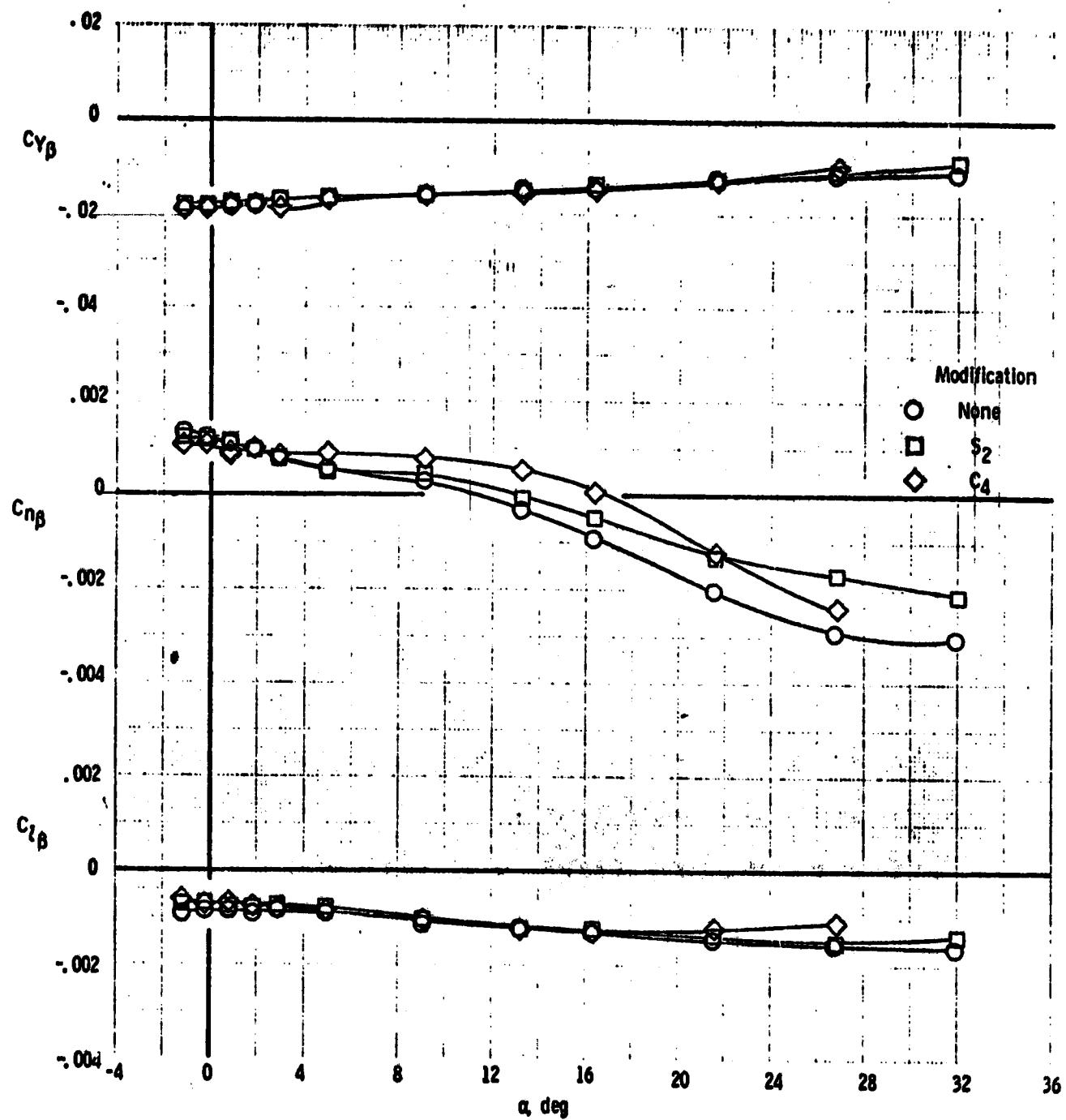


(a) M=1.5  
 Figure 9. - Effect of fillet and canard modifications  
 on lateral-directional characteristics for configuration  
 B<sub>1</sub>WVSoEF.  $\delta_e = -10^\circ$ ;  $\delta_{BF} = -11.7^\circ$ ;  $\delta_{SB} = 55^\circ$

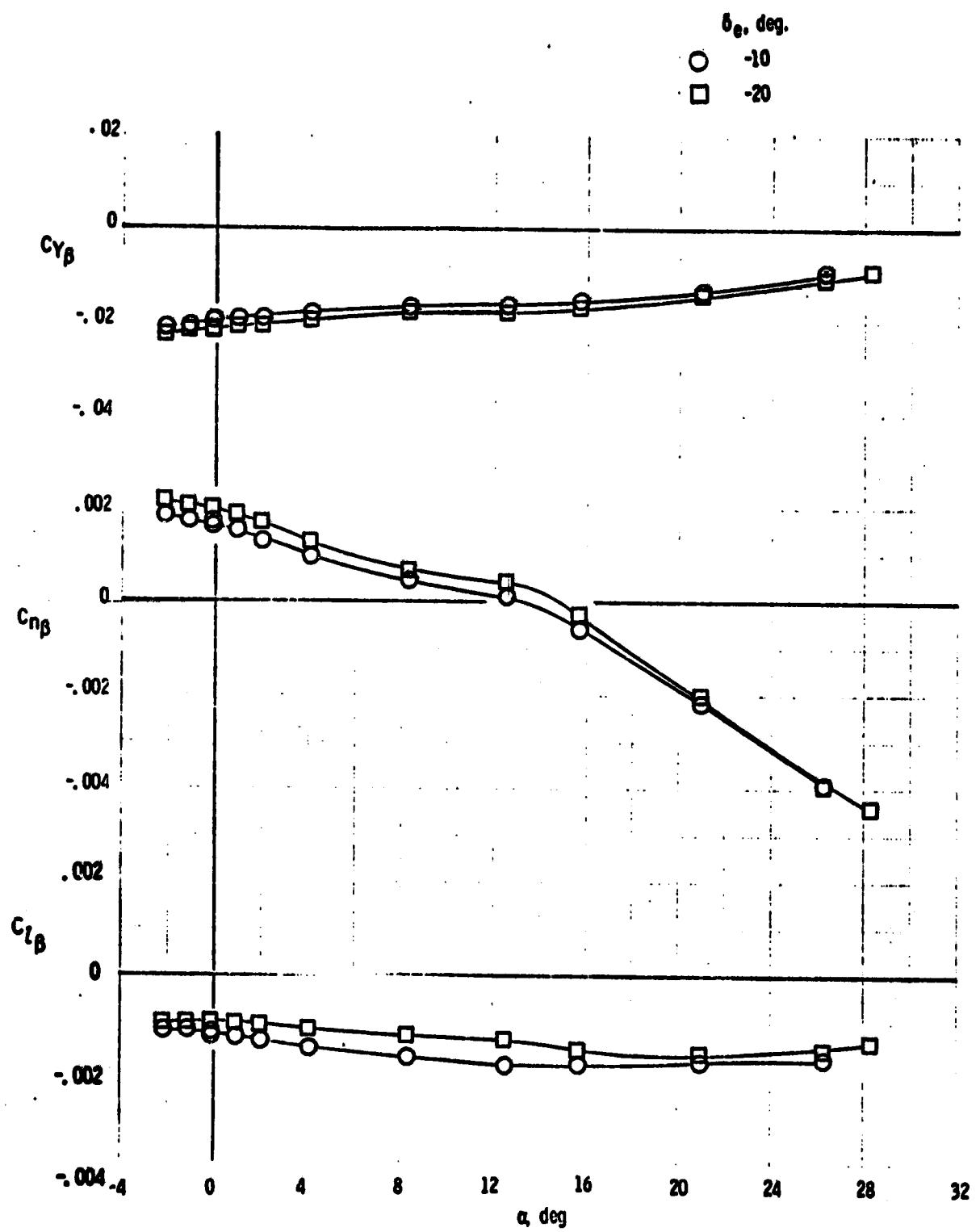


(b)  $M=2.0$

Figure 9. - Continued.

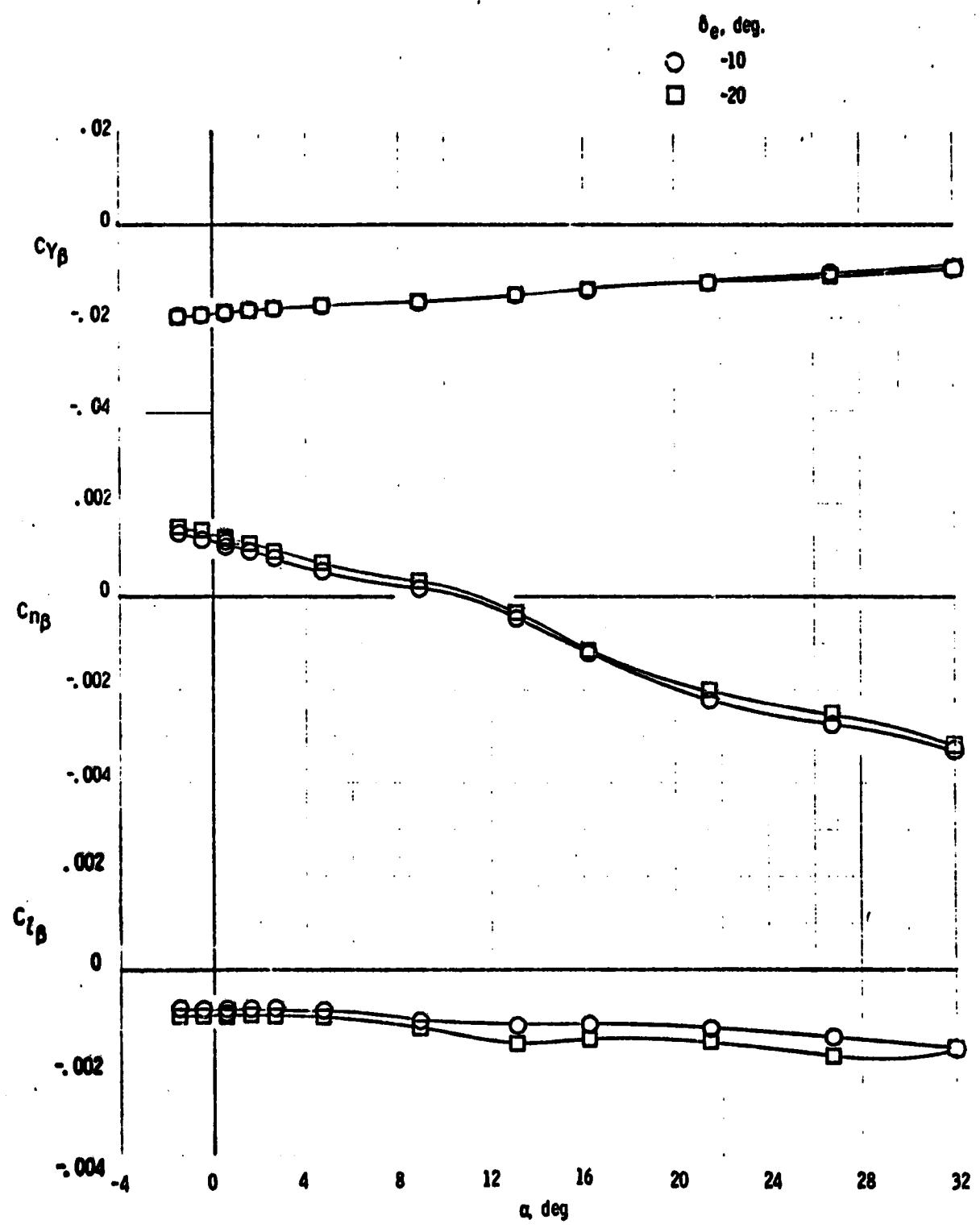


(c)  $M=2.5$   
Figure 9. - Concluded.

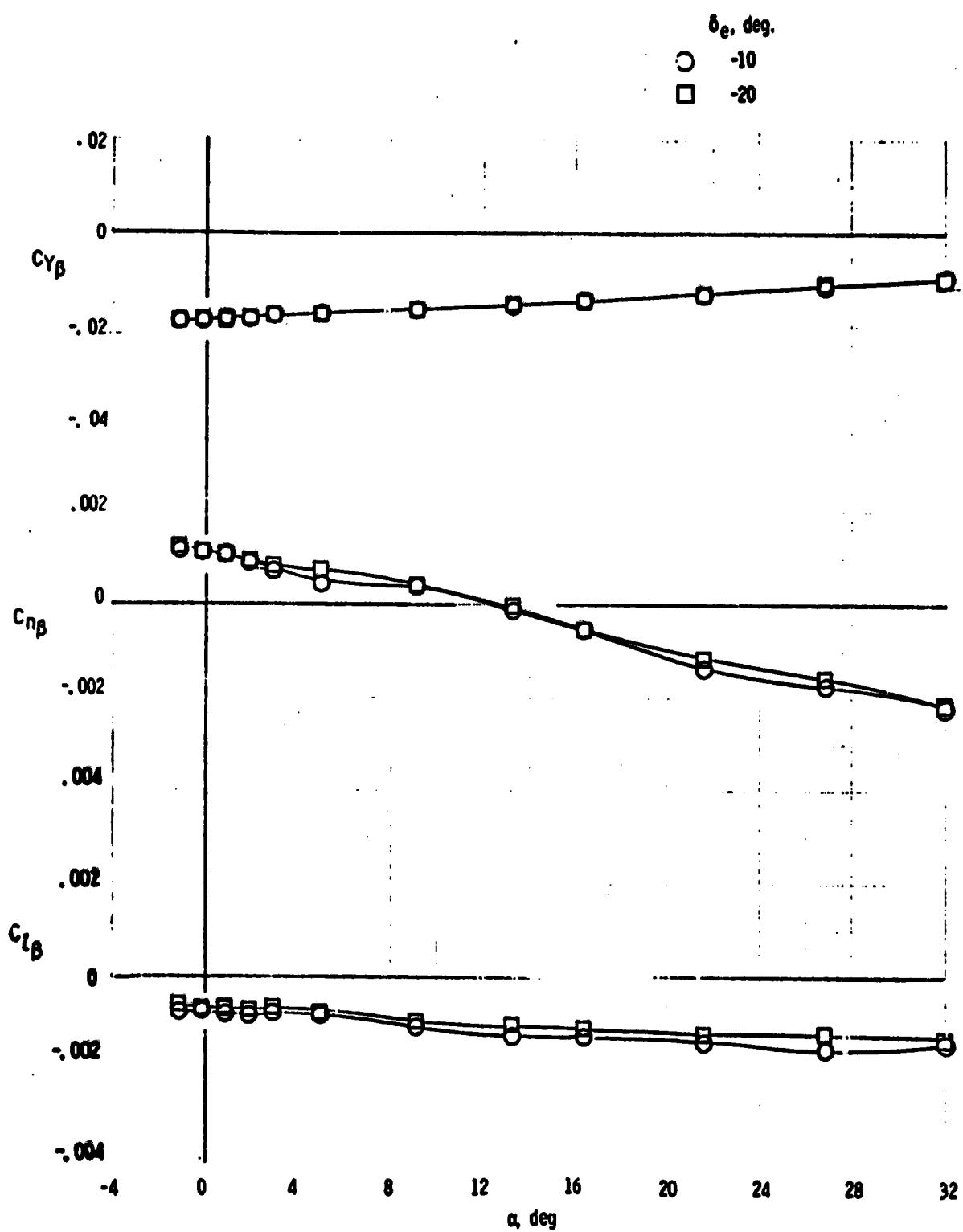


(a)  $M=1.5$

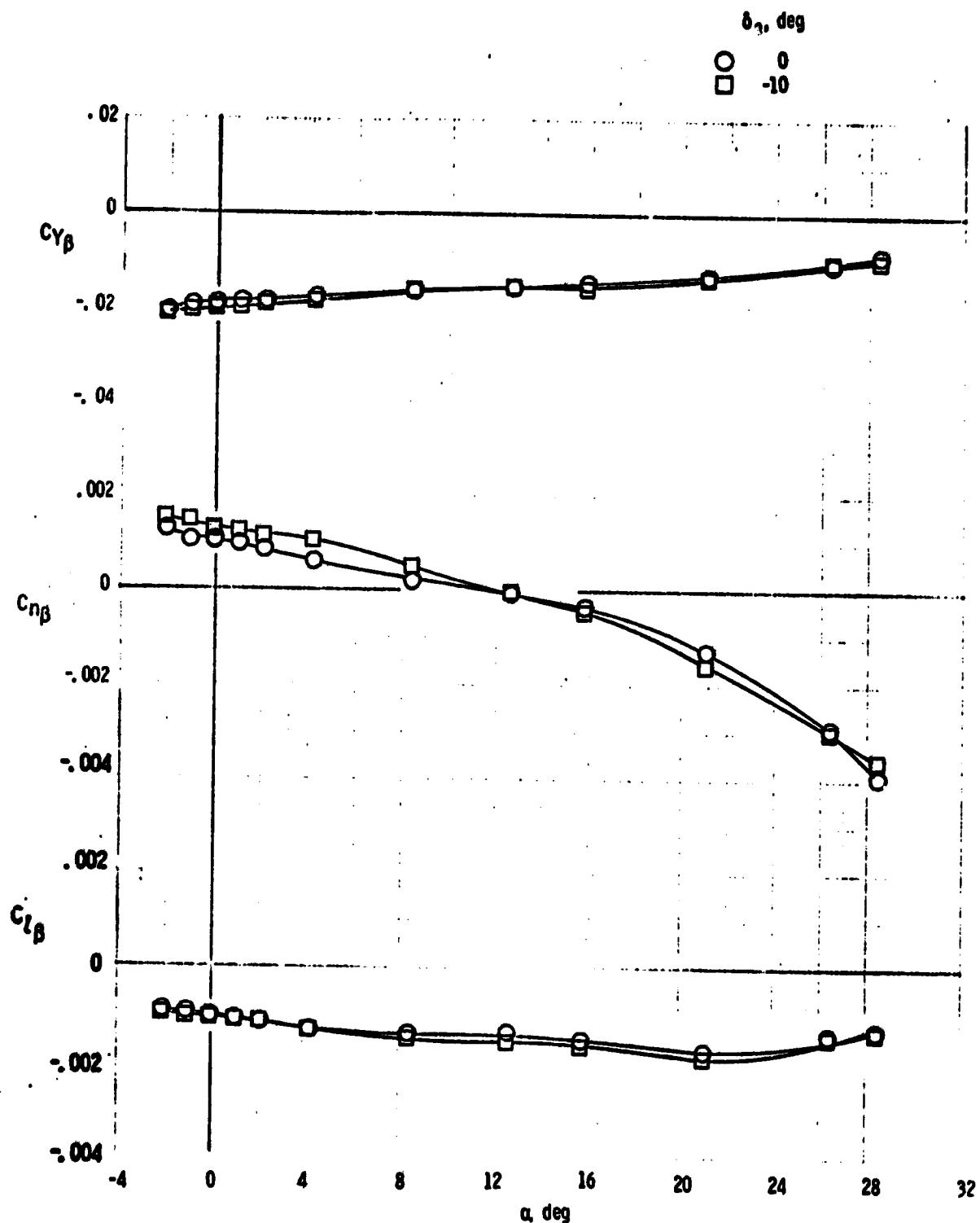
Figure 10. - Lateral-directional aerodynamic characteristics  
for configuration  $B_1WVS_2EF$ .  $\delta_{BF}=-11.7^\circ$ ;  $\delta_{SB}=55^\circ$



(b)  $M=2.0$   
Figure 10. - Continued.

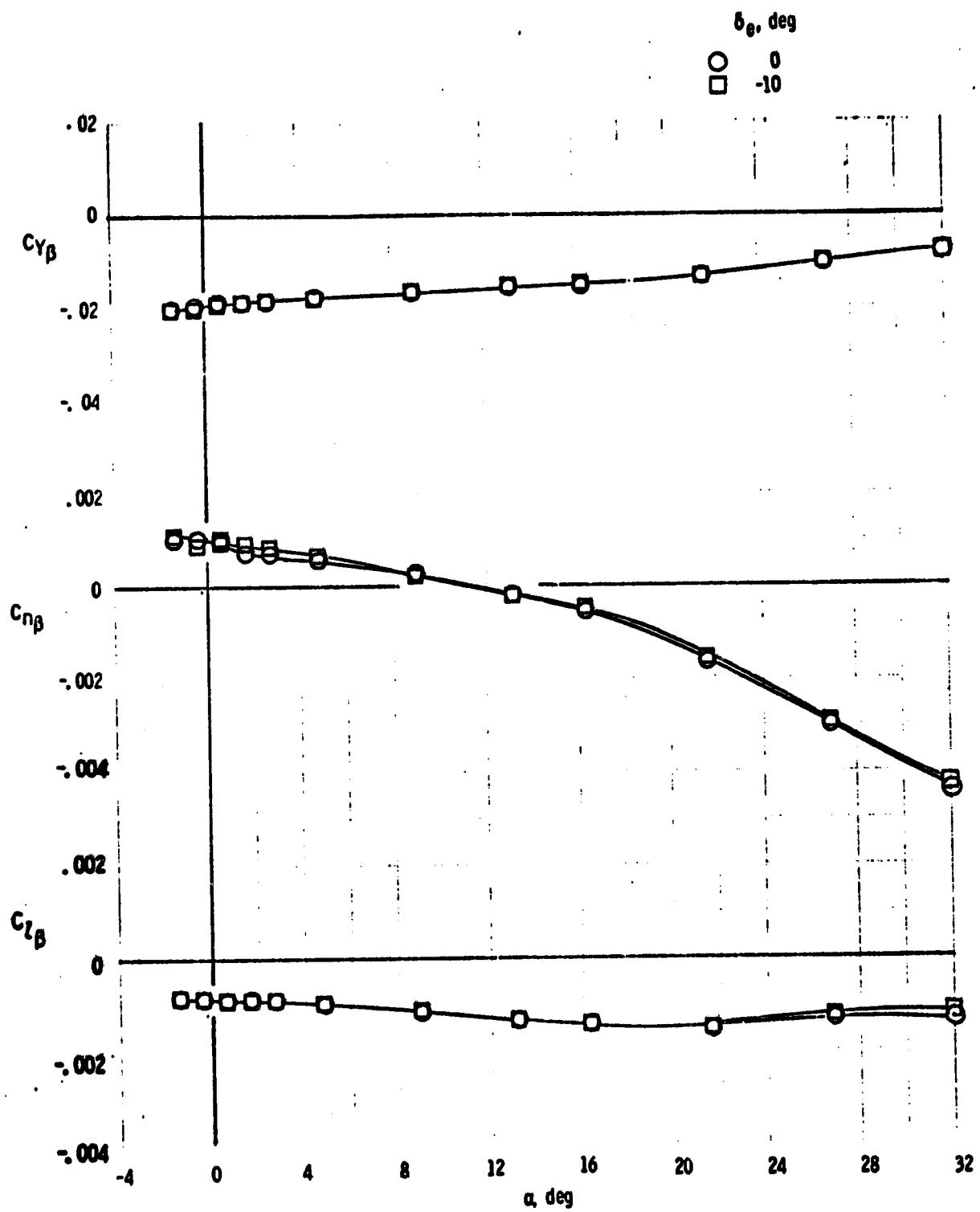


(c) M-2.5  
Figure 10. - Concluded .

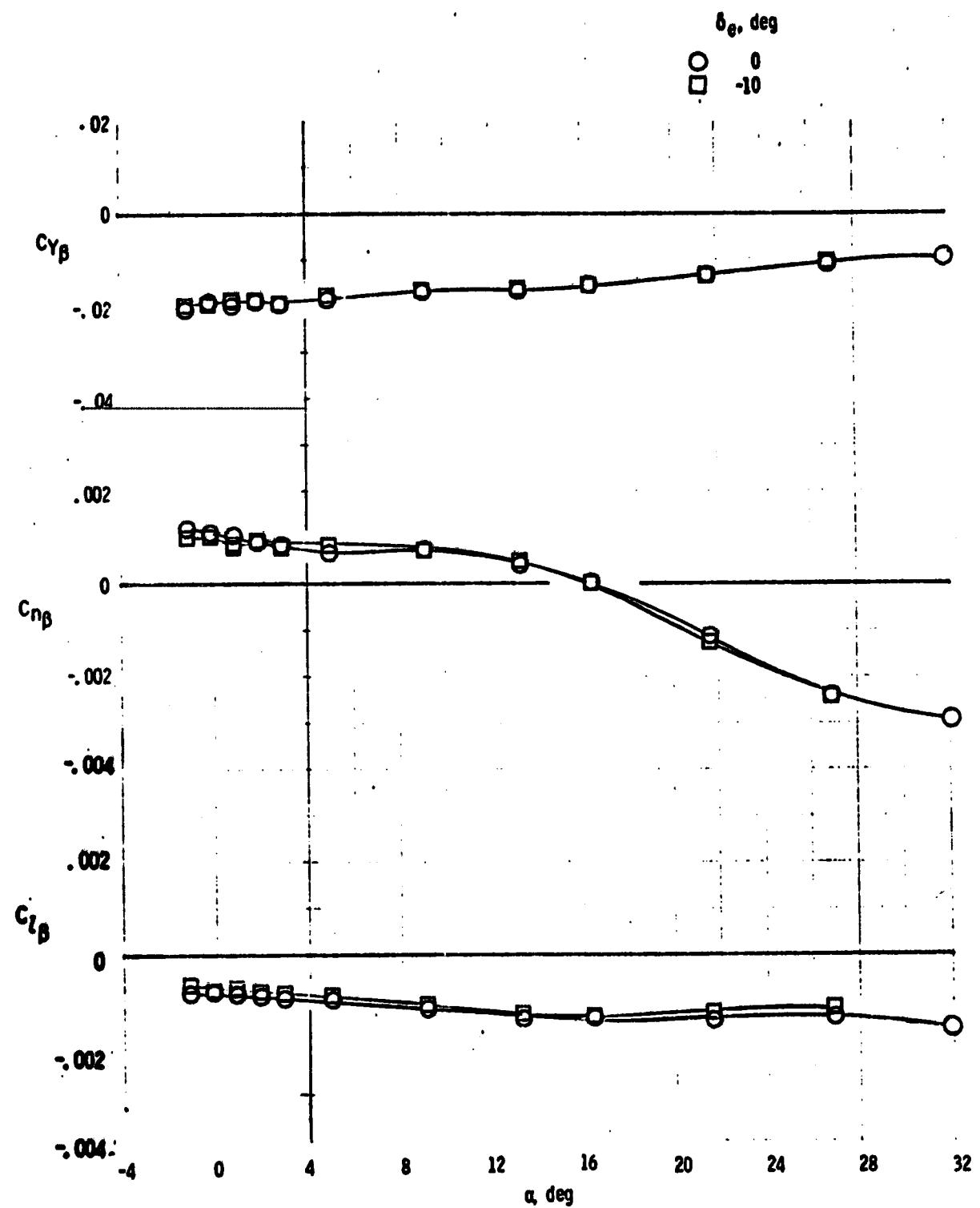


(a)  $M=1.5$

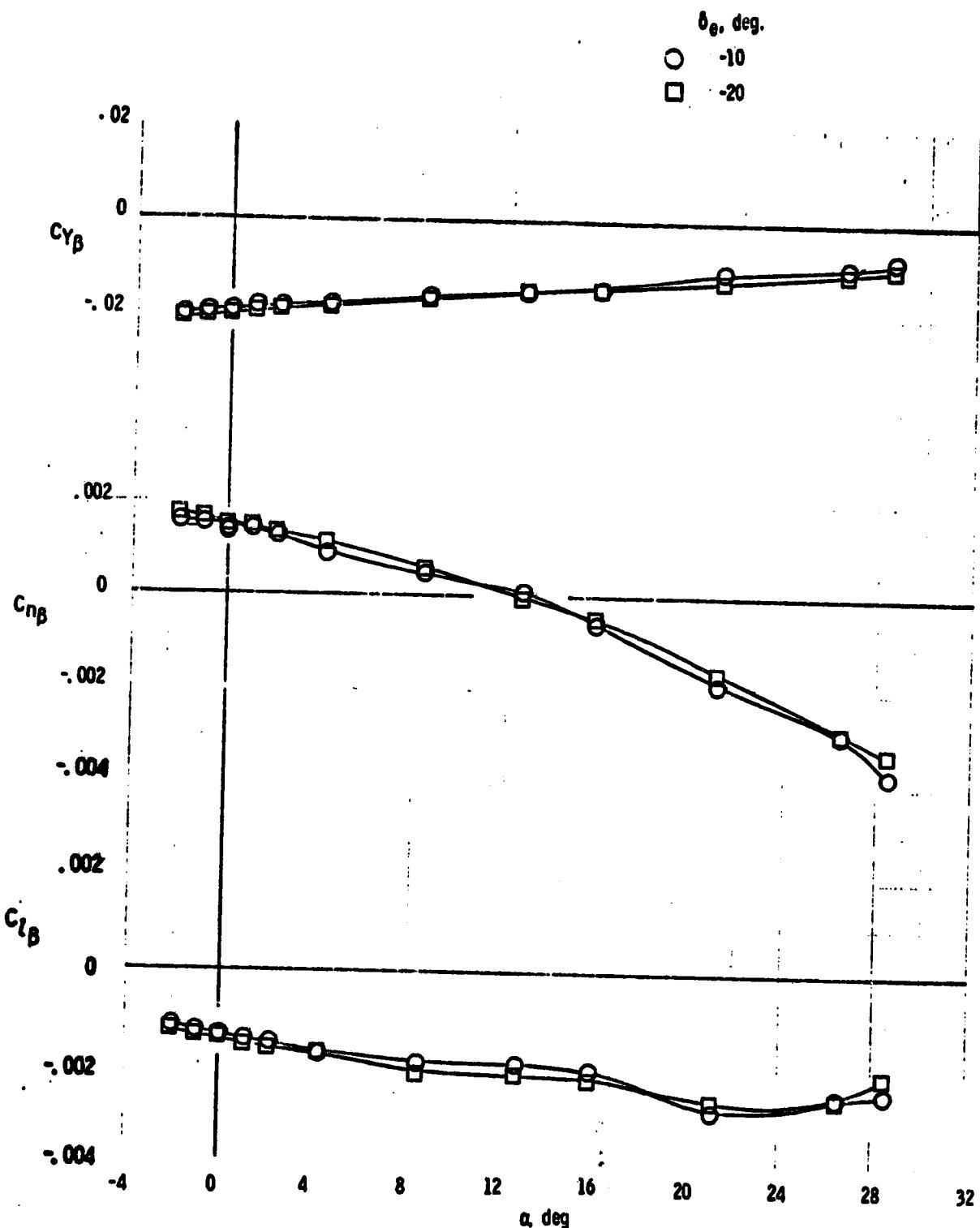
Figure 11. - Lateral-directional aerodynamic characteristics for configuration  $B_1WVS_0C_4$  EF.  $\delta_{BF}=-11.7^\circ$ ;  $\delta_{SB}=55^\circ$



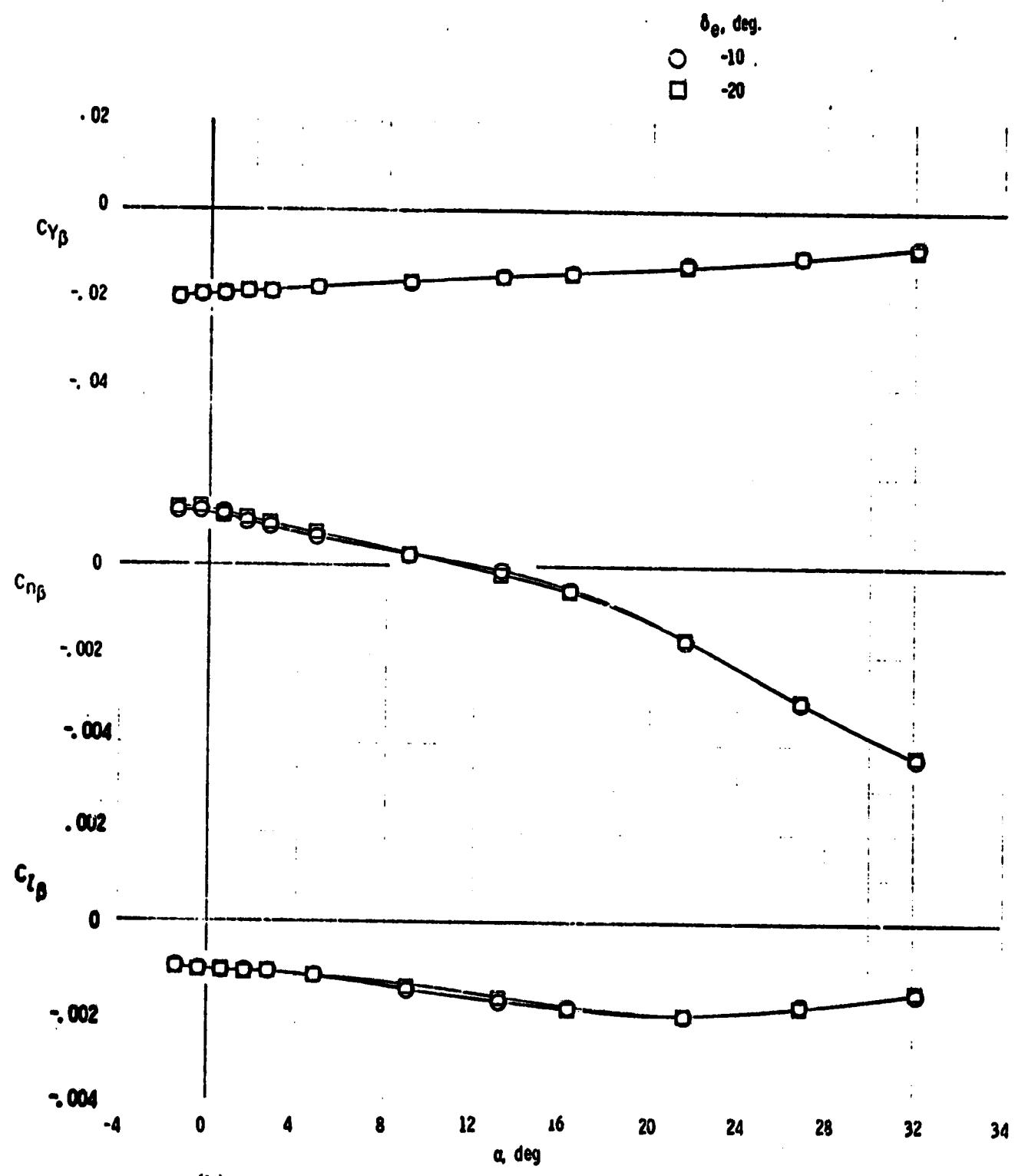
(b)  $M=2.0$   
Figure 11. - Continued.



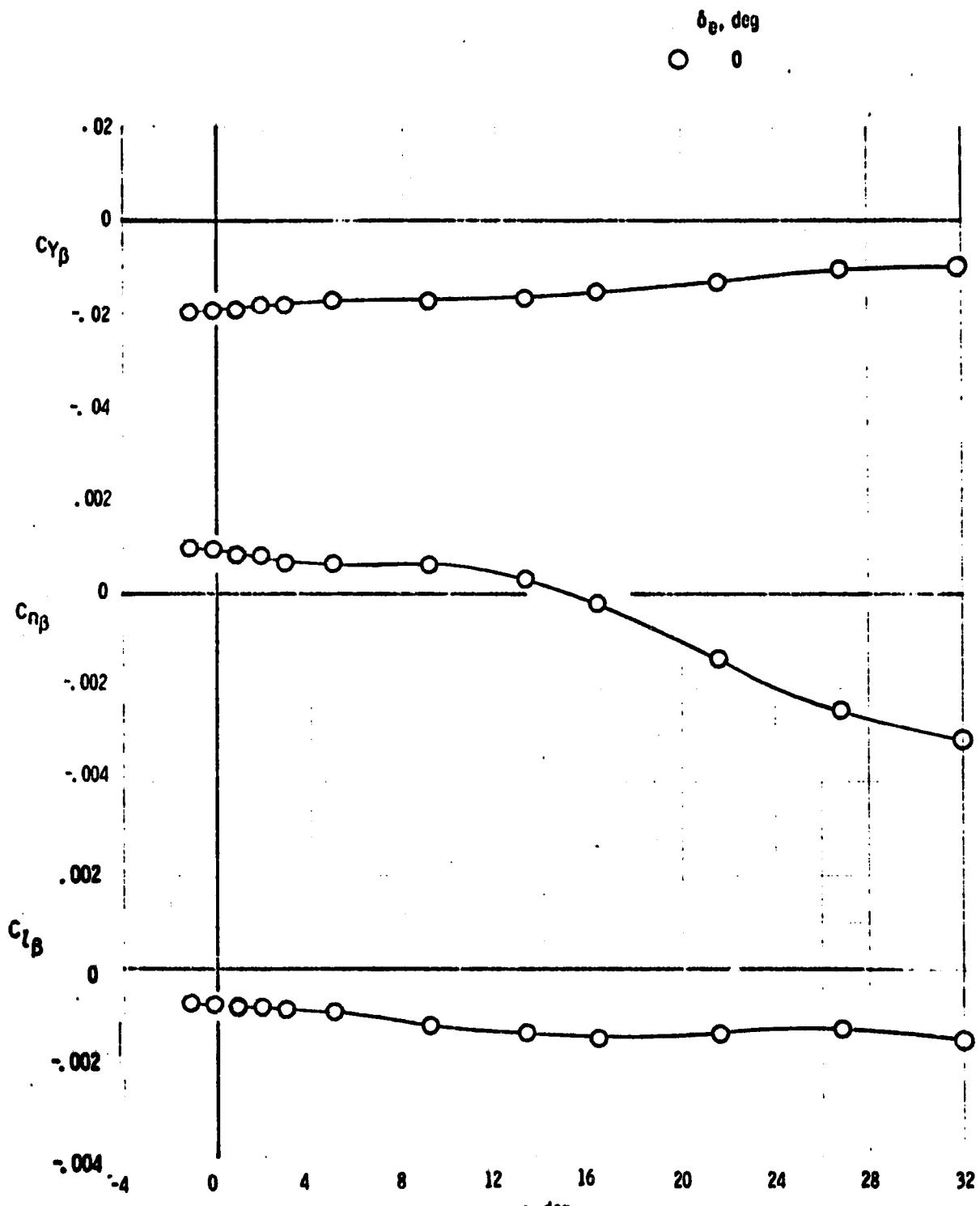
(c)  $M=2.5$   
Figure 11. - Concluded.



(a)  $M=1.5$   
 Figure 12. - Lateral-directional aerodynamic characteristics for configuration B<sub>1</sub>WVS<sub>0</sub>C<sub>5</sub>EF.  $\delta_{BF}=-11.7^\circ$ ;  $\delta_{SB}=55^\circ$



(b)  $M=2.0$   
Figure 12. - Continued.



(c)  $M=2.5$   
Figure 12. - Concluded.

**APPENDIX**  
**Tabulated Data**

The data presented herein are identified in table II (Data Set/Run Number Collation Summary) by configuration and run number. These data are also sorted on tape in the Space Shuttle Data Management System (DATAMAN) and are identified by Shuttle test number LA-46A and data set identifier letters RHG. Access to the data may be obtained by writing to the following address:

**Crysler Corporation, Space Division  
Dept. 2910, P.O. Box 29200  
New Orleans, LA 70189**

TABLE II

TEST : UPNT-1092 (LA-46A)

## DATA SET/RUN NUMBER COLLATION SUMMARY

DATE : 15 JANUARY 1975

DATA SET IDENTIFIER	CONFIGURATION	SCHD.	PARAMETERS/VALUES						NO. OF RUNS	MACH NUMBERS
			$\alpha$	$\beta$	$\delta E$	$\delta BF$	$\delta SB$	$\delta C$		
RH0001	BIWV S0	E1F1	0°	0°	-117	55°			3	13 16 20
	02		5°	0°					14	17 21
	03		0°	-10°					9	11 7
	04		5°	-10°					10	12 8
	05		0°	-20°					3	5 1
	06		5°	-20°					4	6 2
	07	S2	0°	-10°					24	26 22
	08		5°	-10°					25	27 23
	09		0°	-20°					30	32 28
	10		5°	-20°					31	33 29
	11	S0C4	0°	0°					42	44 40
	12		5°	0°					43	45 41
	13		0°	-10°					56	58 60
	14		5°	-10°					57	59 61
	15		0°	-20°					36	38 34
	16		5°	-20°					37	39 35
										75 76
										67
										61
										55
										49
										31
										37
										19
										13
										7

$\alpha$  OR  $\beta$        $\alpha(A) = -2, -1, 2, 4, 8, 16, 20, 26^{\circ}$ , 32<sup>DEGREES</sup>  
 SCHEDULES

IDVAR(11) IDVAR(12) NCV

TEST : IIPWIT=1092 (IA-46A)

DATA SET/BIN NUMBER COLLATION SUMMARY

DATE : 16 JUNE 2021

DATA SET/BIN NUMBER COLLATION SUMMARY

DATE : 16 JUNE 2001

## TABLE A/B TABULATED SOURCE DATA

UFM-1082 (LA-46) ORBITER (S1W5D1F1)

(ENCL1)

PAGE 1

PARAMETRIC DATA									
		BETA = .022	ELEVTR = .022	SETRX = .022					
		11.75	-11.75						
RUN NO.	13/0				CAL	Q	CAL	Q	CAL
MACH	ALPHA	CN	CA	CLN	CLM	CY	CN	CA	CN
1.500	-2.952	-1.14225	-17043	.07271	.07283	.00551	.00551	.00551	.00551
1.500	-1.059	-0.08791	.16282	.06378	.06370	.00552	.00552	.00552	.00552
1.500	-0.038	-0.03771	.16773	.05970	.05969	.00553	.00553	.00553	.00553
1.500	.995	.01847	.16561	.05944	.05927	.00554	.00554	.00554	.00554
1.500	2.064	.06826	.16356	.05918	.05912	.00555	.00555	.00555	.00555
1.500	4.167	-1.17357	-15893	.01189	.01174	.00556	.00556	.00556	.00556
1.500	8.366	.37708	.15228	-.01854	-.01850	.00557	.00557	.00557	.00557
1.500	12.577	.57592	.14760	-.04759	-.04754	.00558	.00558	.00558	.00558
1.500	15.717	.72461	.14598	-.08397	-.08392	.00559	.00559	.00559	.00559
1.500	19.180	.90320	.13591	-.07611	-.07606	.00560	.00560	.00560	.00560
1.500	26.226	1.17453	.12255	-.06882	-.06875	.00561	.00561	.00561	.00561
1.500	28.299	1.25845	.12991	-.06543	-.06533	.00562	.00562	.00562	.00562
RUN NO. 16/0									
MACH	ALPHA	CN	CA	CLN	CLM	CY	CN	CA	CN
2.500	-1.463	-0.08720	-14953	.02696	.02697	-.00558	-.00558	-.00558	-.00558
2.500	-0.437	-0.04750	.14869	.02155	.02155	-.00559	-.00559	-.00559	-.00559
2.500	.573	-.00424	.14795	.01543	.01543	-.00560	-.00560	-.00560	-.00560
2.500	1.629	.03663	.14732	.01936	.01935	-.00561	-.00561	-.00561	-.00561
2.500	2.671	.07871	.14751	.02495	.02495	-.00562	-.00562	-.00562	-.00562
2.500	4.735	.11561	.14761	-.02452	-.02452	-.00563	-.00563	-.00563	-.00563
2.500	8.901	.31838	.13368	-.01656	-.01656	-.00564	-.00564	-.00564	-.00564
2.500	13.072	.47449	.12754	-.02427	-.02427	-.00565	-.00565	-.00565	-.00565
2.500	16.251	.63320	.12216	-.01342	-.01342	-.00566	-.00566	-.00566	-.00566
2.500	21.445	.81638	.11953	-.00514	-.00514	-.00567	-.00567	-.00567	-.00567
2.500	26.713	1.12880	.10604	-.00341	-.00341	-.00568	-.00568	-.00568	-.00568
2.500	31.626	1.24604	.09811	-.00173	-.00173	-.00569	-.00569	-.00569	-.00569

## LA46 A/B TABULATED SOURCE DATA

PAGE 2

UFWT-1092 (LA-46A) ORBITER (B1WWSDF1)

(F0-F001)

## PARAMETRIC DATA

BETA = .000  
BDFLAP = -11.700 ELEVTR = .000  
SFCBK = 55.000

RUN NO. 20/ 0

MACH	ALPHA	CN	CA	CLM	CV	CYN	CBL	CL	CD	L/D	BETA
2.500	-1.130	.08653	.13104	.01309	.00511	.00024	-.00016	-.00363	.13233	-.46811	-.36139
2.500	-.145	-.01980	.13012	.01137	.00446	.00036	-.00013	-.0047	.13522	-.3010	-.05056
2.500	.002	-.00779	.12912	.00695	.00564	.00024	-.00012	-.00927	.12698	-.07342	-.06140
2.500	1.065	.02827	.12791	.00678	.00460	.00021	-.00012	.02404	.12877	.16573	-.06136
2.500	2.917	.05455	.12660	.00511	.00312	.00021	-.00012	.00803	.12991	.37114	-.05941
2.505	4.976	.11951	.12277	.00273	.00354	.00022	-.00011	.01842	.13267	.81716	-.05975
2.505	9.595	.24726	.11505	.00710	.00147	.00021	-.00011	.00014	.15259	1.48110	-.05794
2.500	13.240	.49211	.10874	.01571	-.02561	.00032	.00019	.19555	.18235	1.82356	-.05523
2.500	16.338	.49960	.10461	.01978	-.02596	.00019	.00021	.45128	.21101	1.86331	-.05851
2.503	19.663	.59463	.02911	-.01669	.00120	.00021	.00022	.61357	.74455	1.78139	-.05555
2.505	21.548	.69562	.08525	-.03944	-.00202	.00191	.00036	.75341	.48550	1.58248	-.05741
2.500	25.785	.89822	.07641	-.05217	-.00426	.00173	.00044	.98259	.55355	1.38816	-.06422
2.500	31.974	1.1171									

(F0-F002)

UFWT-1092 (LA-46A) ORBITER (B1WWSDF1)

## PARAMETRIC DATA

BETA = .000  
BDFLAP = -11.700 ELEVTR = .000  
SFCBK = 55.000

RUN NO. 14/ 0

MACH	ALPHA	CN	CA	CLM	CV	CYN	CBL	CL	CD	L/D	BETA
1.950	-2.060	-.13753	.17028	.06550	-.09237	.00887	-.00481	-.13123	.17619	-.74904	5.08041
1.950	-1.062	-.09171	.16580	.05926	-.09259	.00800	-.00495	-.08855	.17477	-.51641	5.38335
1.950	-.030	-.03625	.16893	.04516	-.08936	.00758	-.00501	-.03651	.16695	-.21403	5.08232
1.950	.987	.01545	.16794	.03495	-.08683	.00557	-.00526	.115518	.07467	5.38017	
2.044	1.952	.16843	.02805	-.08240	-.08666	-.00596	-.00545	.16557	.37449	5.07269	
1.950	4.146	.17260	.16175	.02787	-.08085	.00485	-.00566	.16146	.17581	.92316	5.37775
1.950	12.554	.36844	.02015	-.07583	.00253	-.00568	.36258	.25657	1.65597	5.37754	
1.950	15.713	.14133	.08190	-.07466	-.00235	-.00720	.51930	.26759	1.93691	5.38241	
1.950	20.992	.96071	.12671	-.08296	-.05112	-.00520	.65124	.33313	1.97331	5.37994	
1.950	25.604	1.14199	.12035	-.07778	-.05572	-.00235	.97784	.46246	1.84135	5.3852	
1.950	28.265	1.25726	.11556	-.07586	-.05061	-.002454	.60244	1.55238	.66203	1.62423	5.38537
1.950									.69753	1.50873	5.38177

L446 A/B TABULATED SOURCE DATA  
UFMT-1092 ((A-A6A) ORBITER 'B1WVSD1F1')

PAGE 3

(R46C52)

MACH	ALPHA	PARAMETRIC DATA						BETA	
		CN	CA	CL <sup>A</sup>	CY	CY <sup>B</sup>	CD		
2.000	-1.031	-.00583	.14676	.02305	-.00683	.01553	-.00496	-.54416	
2.000	-.435	-.04726	.14803	.01741	-.00533	.00491	-.04614	5.06724	
2.000	.572	-.05435	.14576	.01318	-.00592	.00427	-.00593	-.51055	
2.000	1.502	.03545	.14524	.01746	-.00454	.00191	-.00276	5.05346	
2.000	2.645	.07774	.1474	.00215	-.0023	.00298	-.00457	5.06554	
2.000	4.727	.15959	.14169	.00591	-.0023	.00150	-.00274	5.06216	
2.000	8.504	.31925	.13694	.01625	-.00779	.00039	.00039	5.06175	
2.000	13.075	.47771	.12924	-.12457	-.00797	-.00359	-.00643	5.06249	
2.000	16.259	.67487	.12150	-.03305	-.00680	-.00831	-.00562	5.06355	
2.000	21.443	.81141	.11763	-.04455	-.00590	-.01512	-.00540	5.06413	
2.000	26.713	.92688	.09816	-.05519	-.00557	-.00728	-.00736	5.06466	
2.000	31.921	1.25254	.09139	-.06727	-.00529	-.02179	-.00735	5.06177	
RUN NO. 17/0									
MACH	ALPHA	CN	CA	CL <sup>A</sup>	CY	CY <sup>B</sup>	CD	L/D	BETA
2.500	-1.137	-.56887	.13100	.01919	-.00456	.01634	-.00495	.13234	5.06197
2.500	-.133	-.04055	.12970	.01767	-.00310	.00634	-.00518	.12979	5.06232
2.500	.891	.03375	.12797	.01534	-.00764	.00499	-.00450	.03176	5.07716
2.500	1.862	.02295	.12689	.01363	-.00761	.00442	-.00479	.02381	5.07773
2.500	2.900	.06295	.12516	.01219	-.00809	.00389	-.00476	.05948	5.07694
2.500	4.979	.12221	.12285	-.00191	-.00827	.00287	-.00572	.11136	5.07640
2.500	9.110	.26518	.11564	-.00759	-.00871	.00164	-.00629	.23659	5.07551
2.500	13.239	.39231	.10955	-.01569	-.01611	.00128	-.00692	.35681	5.07348
2.500	16.350	.59855	.10353	-.02315	-.02315	.00422	-.00741	.45684	5.07363
2.500	21.548	.69854	.09273	-.03193	-.06650	-.00915	-.00775	.61566	5.07286
2.500	26.782	.90198	.08554	-.04332	-.08025	-.01329	-.00843	.76868	5.07159
2.500	31.970	1.11336	.07954	-.05205	-.05871	-.01468	-.02894	.65591	5.07169
RUN NO. 21/5									
MACH	ALPHA	CN	CA	CL <sup>A</sup>	CY	CY <sup>B</sup>	CD	L/D	BETA
2.500	-1.137	-.56887	.13100	.01919	-.00456	.01634	-.00495	-.06619	5.06197
2.500	-.133	-.04055	.12970	.01767	-.00310	.00634	-.00518	-.04305	5.06232
2.500	.891	.03375	.12797	.01534	-.00764	.00499	-.00450	.03176	5.07716
2.500	1.862	.02295	.12689	.01363	-.00761	.00442	-.00479	.02381	5.07773
2.500	2.900	.06295	.12516	.01219	-.00809	.00389	-.00476	.05948	5.07694
2.500	4.979	.12221	.12285	-.00191	-.00827	.00287	-.00572	.11136	5.07640
2.500	9.110	.26518	.11564	-.00759	-.00871	.00164	-.00629	.23659	5.07551
2.500	13.239	.39231	.10955	-.01569	-.01611	.00128	-.00692	.35681	5.07348
2.500	16.350	.59855	.10353	-.02315	-.02315	.00422	-.00741	.45684	5.07363
2.500	21.548	.69854	.09273	-.03193	-.06650	-.00915	-.00775	.61566	5.07286
2.500	26.782	.90198	.08554	-.04332	-.08025	-.01329	-.00843	.76868	5.07159
2.500	31.970	1.11336	.07954	-.05205	-.05871	-.01468	-.02894	.65591	5.07169

## LA46 A/B TABULATED SOURCE DATA

UFWT-1092 (LA-46) ORBITER (B1WVSD1F1)

(ENG5G3)

## PARAMETRIC DATA

BETA = .000  
 BCFLAF = -11.700  
 ELEVTR = -10.000  
 SFDRK = 55.000

RUN NO.

9 / 6

MACH	ALPHA	CN	CA	CLM	CY	CYN	CL	CC	L/C	BETA
1.500	-2.133	.20740	.17940	.11743	-.00152	.00169	.50149	-.20059	-.10750	-.05737
1.500	-1.103	-.16357	-.17631	-.10641	-.00183	.00192	.50154	-.15012	-.10863	-.05721
1.500	-.050	-.16055	-.17625	.09376	-.00161	.00183	.50133	-.10028	.17636	-.05659
1.500	.945	-.04780	-.17360	.08570	-.00191	.00186	.50135	-.09055	.17279	-.05726
1.500	2.518	.09817	.17195	.07514	-.00189	.00178	.50125	.04215	.17138	-.05626
1.500	4.106	.11026	.16475	.03751	-.00180	.00154	.50113	.09036	.17223	-.05711
1.500	8.313	.31267	.16616	.02568	-.00125	.00127	.50127	.28681	.19574	-.05749
1.500	12.534	.51790	.14760	-.01299	-.00134	.00264	.50175	.47351	.25657	1.86555
1.500	15.686	.66512	.14555	-.01378	-.00148	.00275	.50165	.60237	.31115	1.91168
1.500	20.551	.90153	.12875	-.03176	-.00536	.00271	.50139	.79549	.44260	1.79824
1.500	25.221	1.15788	.11915	-.02266	-.00146	.00199	.50123	.59559	.15782	1.55432
1.500	28.259	1.19271	.11622	-.01373	-.00189	.00270	.50124	.99553	.66716	1.49241

RUN NO.

11 / 0

MACH	ALPHA	CN	CA	CLM	CY	CYN	CL	CC	L/C	BETA
2.000	-1.473	-.12542	.15227	.50147	-.00113	.00109	.12146	.15544	-.70138	-.03905
2.000	-.489	-.08441	.15094	.06468	.00210	-.00111	.00819	.15161	-.54872	-.03979
2.000	-.536	-.08449	.14927	.04881	.00201	-.00117	.00992	.04294	.14886	-.03984
2.000	1.586	-.03289	.14795	.04301	.00187	-.00105	.00685	.14781	-.34725	-.03995
2.000	2.633	-.03999	.14593	.05376	.00134	-.00161	.00568	.33325	.14751	-.22223
2.000	4.714	-.12237	.14110	.02794	.00218	.00115	.00554	.11136	.15058	-.03843
2.000	8.874	-.28027	.13395	.01432	-.00113	.00048	.00149	.25638	.17470	1.46755
2.000	13.549	.43389	.12453	.01877	-.00140	.00101	.00143	.35647	.21924	1.79939
2.000	16.185	.56126	.11893	.01346	-.00294	.00093	.00059	.57587	.27166	1.86921
2.000	21.427	.43751	-.10790	-.00273	.00095	.00075	.00281	.38224	1.77831	1.02633
2.000	25.698	.98271	.10350	-.00326	.00158	.00051	.00364	.52461	1.59384	1.03580
2.000	31.912	1.20525	-.00553	.00082	.00071	.00058	.00031	.75531	1.39329	1.03303

## LA46 A/B TABULATED SOURCE DATA

PAGE 5

UFWT-1092 (LA-46) ORBITER (B1WNSDEF1)

(RMG003)

## PARAMETRIC DATA

BETA = .000  
BCFLAP = -11.700 SFCBRK = 55.000

RUN NO. 7/0

MACH	ALPHA	CN	CA	CLM	CY	CYN	CBL	CL	CC	L/C	BETA
2.500	-1.153	-0.99668	.13348	.02544	.00896	.00110	.00197	.13528	.65033	-.04568	
2.500	-1.147	-0.96119	.13212	.02327	.00863	.00150	.00050	.13227	.45296	-.04540	
2.500	.849	-.03125	.13053	.01056	.01052	.00072	.00583	.03318	.25114	-.04763	
2.500	1.865	-.00113	.12935	.01863	.00781	.00079	.00566	.02924	.64133	-.04585	
2.500	2.931	.51891	.12737	.01659	.00648	.00098	.00076	.02852	.22115	-.04497	
2.500	4.957	.09705	.12332	.01395	.00939	.00102	.00065	.00633	.13124	.65346	
2.500	9.524	.22765	.11452	.00639	.00748	.00102	.00069	.20672	.14913	.04759	
2.500	13.228	.37115	.11661	.00839	.00535	.00107	.00749	.33686	.16891	.04597	
2.500	16.323	.47435	.10220	-.01362	.00691	.00155	.00367	.42651	.25139	.04319	
2.500	21.537	.67101	.09219	-.70944	.00496	.00183	.00581	.59111	.33223	.04422	
2.500	26.763	.83712	.08046	-.91670	.00443	.00226	.00746	.73795	.46233	.04635	
2.500	31.931	1.37970	.06956	-.92493	.00172	.00172	.00489	.87932	.63059	.04621	

UFWT-1092 (LA-46A) ORBITER (B1WNSDEF1)

## PARAMETRIC DATA

BETA = 5.000  
BCFLAP = -11.700 SFCBRK = 55.000

RUN NO. 10/0

MACH	ALPHA	CN	CA	CLM	CY	CYN	CBL	CL	CC	L/C	BETA
1.500	-2.143	-2.0913	.17659	.11273	-.10748	.01167	-.00428	-.120238	.18428	-.059818	
1.500	-1.113	-1.5407	.17528	.10178	-.10295	.01044	-.00443	-.15063	.17824	-.04512	
1.500	-1.107	-1.12296	.17416	.09229	-.10329	.01026	-.00457	-.17263	.17435	-.059272	
1.500	-946	-.05019	.17277	.08196	-.09955	.00922	-.00466	-.05303	.17152	-.059818	
1.500	2.013	.07362	.17792	.07206	-.09717	.00849	-.00455	-.10235	.17095	-.01376	
1.500	4.099	.10605	.16633	.05576	-.09161	.00569	-.00384	-.09398	.17348	.04125	
1.500	8.309	.31081	.15777	.02393	-.08634	.00425	-.00357	-.08475	.20103	.14164	
1.500	12.523	.51184	.14756	-.00213	-.08911	.00277	-.00399	-.03277	.25503	.03376	
1.500	15.667	.65554	.13695	-.01626	-.08276	-.00222	-.00366	-.01022	.31081	.19133	
1.500	20.945	.89768	.12270	-.03263	-.07795	-.01016	-.00486	-.00457	.43549	.09176	
1.500	26.207	1.16319	.11597	-.02583	-.06307	-.02159	-.00638	-.00638	.59339	.15927	
1.500	28.243	1.18598	.11147	-.02304	-.06273	-.02368	-.00722	-.00723	.65942	.15041	

## PARAMETRIC DATA

BETA = 5.000  
BCFLAP = -11.700 SFCBRK = 55.000

LW46 A/B TABULATED SOURCE DATA  
UPMT-1092 (LA-46A) ORBITER (B1WPSDF1)

## (INHCGDATA)

BETA = 5.000 ELEVTR = -10.000  
BDFAP = -11.700 SPDRK = 55.000

## PARAMETRIC DATA

MACH	ALPHA	CN	CA	CLW	CY	CYN	CPB	CL	CD	CQ	LC	BETA
2.000	-1.493	-1.1274	-15176	.55727	-.05966	.05666	-.00055	-.12353	.5497	-.79712	5.09133	
2.000	-1.494	-15844	.05226	-.06669	.06615	-.00026	-.00027	.51112	-.31820	-.55762	5.09094	
2.000	-1.495	-0.98569	.04756	-.06312	.05533	-.00033	-.00020	.51750	.1864	-.24695	5.08854	
2.000	-1.496	.546	14919	.04756	-.06312	.05533	-.00033	-.00026	.51747	-.21114	5.08555	
2.000	1.586	-1.52844	14915	-.04115	-.05970	.05616	-.00016	.51119	.14770	.70180	5.09432	
2.000	2.626	14912	.03792	-.05964	.05614	-.00016	-.00025	.51629	.51593	1.43675	5.08451	
2.000	4.707	1.18032	.02628	-.05835	.05288	-.00028	-.00026	.51254	.51253	1.78674	5.08398	
2.000	8.870	.27650	.01278	-.05127	.05127	-.00016	-.00026	.50581	.39564	.22186	5.08337	
2.000	13.051	12691	.05794	-.05794	.05794	-.00026	-.00026	.51314	.26991	1.86459	5.08322	
2.000	16.175	.55811	.01187	-.05727	.05727	-.00021	-.00021	.51721	.51320	.67927	1.79114	
2.000	21.422	.77305	.01044	-.05660	.05660	-.00028	-.00028	.51694	.05336	.51329	1.59288	
2.000	28.687	.97977	.00919	-.05454	.05454	-.00051	-.00051	.51495	.03355	.51319	5.08333	
2.000	31.895	1.19412	.00351	-.02144	.02144	-.00110	-.00110	.50510	.96971	.75183	1.38169	
2.000	31.952	1.07613	.02349	-.02144	.02144	-.00110	-.00110	.50510	.96971	.63236	1.38156	

RUN NO. 8/0

MACH	ALPHA	CN	CA	CLW	CY	CYN	CPB	CL	CD	CQ	LC	BETA
2.500	-1.149	-.02005	.01293	.02199	.01953	.00743	-.00382	-.00756	.13471	-.64652	5.07769	
2.500	-1.172	-.06377	.13128	.01974	-.08865	.01677	-.00403	-.01318	.13146	-.59301	5.07813	
2.500	.853	-.02274	.12917	.01758	-.08323	.01614	-.00403	-.02266	.12924	-.17559	5.07324	
2.500	1.059	.00330	.12817	.01499	-.08965	.01522	-.00403	-.01811	.12811	-.07668	5.07639	
2.500	2.911	.03916	.12634	.01355	-.08667	.01453	-.00403	-.03273	.12817	-.25534	5.07246	
2.500	4.961	.11200	.12297	.01144	-.07886	.01356	-.00395	.09168	.13139	.69778	5.07701	
2.500	6.091	.23564	.11498	.01439	-.07339	.01227	-.00393	.21471	.15080	1.42376	5.06931	
2.500	13.225	.36981	.10811	-.01352	-.07196	-.00383	-.00383	.33535	.88987	1.76629	5.06932	
2.500	16.325	.47929	.10171	-.01046	-.05922	-.00343	-.00343	.43138	.43138	.22233	5.06927	
2.500	21.537	.67139	.08939	-.01322	-.05656	-.00374	-.00374	.59449	.59449	.33072	5.06711	
2.500	26.760	.86601	.08657	-.01962	-.05571	-.00384	-.00384	.73832	.46366	1.59237	5.06729	
2.500	31.952	1.07613	.07299	-.05689	-.01366	-.00366	-.00366	.87622	.63236	1.38156	5.06901	

UWLT-1592 (LA-46A) ORBITER (81WVSDE1F1) (EMG.2005.1)

SIGNIFICANT DATA

## LANG A/B TABULATED SOURCE DATA

PAGE 6

UPT-1092 (LA-46A)ORBITER (B1W5D1F1)

(RNGD05)

## PARAMETRIC DATA

BETA = .000  
EDFLAP = -11.700  
SFDBRK = -00.000  
ELEVTR = -00.000  
L/D = 55.000

RUN NO. 1 / 0

MACH	ALPHA	CN	CA	CLN	CV	CYN	CL	CD	L/D	BETA
2.900	-1.164	-.12375	.14298	.04499	.003593	.00104	.00240	.12082	.03057	.04463
2.900	-.173	-.09411	.14119	.04202	.01046	.00291	.00280	.09369	.1146	.04643
2.900	.813	-.28582	.13942	.03937	.00367	.00287	.00287	.06780	.1947	.04615
2.900	1.842	-.03082	.13726	.03635	.00344	.00281	.00281	.03522	.1620	.04725
2.900	2.877	-.02007	.13514	.03389	.00307	.00287	.00287	.00749	.13494	.04656
2.900	4.932	.07265	.12955	.02990	.00112	.00112	.00063	.05925	.13515	.04674
2.900	9.960	.20335	.11964	.02144	.00091	.00121	.00055	.18198	.19017	.04733
2.900	13.209	.34261	.11207	.01559	.00769	.00115	.00241	.30794	.18739	.04630
2.900	16.306	.44576	.10548	.01273	.00810	.00159	.00332	.39793	.17532	.04684
2.900	21.516	.63997	.09366	.00781	.00470	.00176	.00313	.56122	.32290	.04430
2.900	26.745	.83791	.08397	.00485	.00357	.00221	.00396	.71053	.45198	.04327
2.900	31.926	1.04116	.07216	.00323	.00168	.00168	.00249	.84551	.61183	.04293

## PARAMETRIC DATA

BETA = .000  
EDFLAP = -11.700  
SFDBRK = -00.000  
ELEVTR = -00.000  
L/D = 55.000

UPT-1092 (LA-46A)ORBITER (B1W5D1F1)

(RNGD06)

RUN NO. 4 / 0

MACH	ALPHA	CN	CA	CLN	CV	CYN	CL	CD	L/D	BETA
1.900	-2.194	-.27681	.19516	-.12234	-.11585	.01272	-.00613	-.29914	.20564	.03295
1.900	-1.161	-.22155	.19353	-.14134	-.11231	.0121	-.00614	-.21758	.19798	.03052
1.900	-.146	-.16874	.19169	-.13640	-.10960	.01149	-.00520	-.16824	.19212	.037848
1.900	.979	-.11369	.18958	-.11917	-.10714	.01059	-.00630	-.11860	.18776	.037570
1.900	1.967	-.09689	.18741	-.10815	-.10403	.00979	-.00614	-.0626	.18535	.034130
1.900	4.056	.05974	.18268	-.08945	-.09883	.01736	-.00763	-.03769	.18582	.029285
1.900	8.273	.24997	.17311	.06100	-.09217	.01231	-.00888	-.22246	.20728	.037326
1.900	12.463	.45506	.16085	.03418	-.09438	.01130	-.00959	-.40954	.25541	.037345
1.900	15.628	.59747	.15112	.02305	-.08667	.01164	-.00979	-.53467	.30649	.037361
1.900	20.591	.83362	.13512	.01160	-.08581	-.00837	-.00557	-.73037	.42362	.037257
1.900	26.167	1.03983	.12433	.01283	-.07075	-.02110	-.00549	-.87843	.57015	.034769
1.900	28.215	1.13225	.11979	.01559	-.06713	-.02300	-.00655	-.94137	.64788	.037842

## LA46 A/B TABULATED SOURCE DATA

UPMT-1092 (LA-46) ORBITER (B11WSEDF1)

PAGE 9

(RA46C6)

## PARAMETRIC DATA

BETA = 5.000 ELEVTR = -20.000  
 BCFLAP = -11.700 SPARK = 55.000

RUN NO. 6 / 0

MACH	ALPHA	CN	CA	CLW	CY	CYH	CBL	Q	CD	L/D	BETA
2.000	-1.500	-1.16989	.16407	.08432	-.10421	.00734	-.00494	.16354	.16047	.98282	5.09530
2.000	-.493	-1.12952	.16239	.07958	-.10167	.00661	-.102520	.16350	.16350	.78561	5.09477
2.000	-.521	-.08758	.16247	.07361	-.09894	.00670	-.005056	.15967	.15967	.55764	5.09291
2.000	1.557	-.04414	.15819	.06816	-.09689	.00520	-.00497	.15693	.15693	.31082	5.09193
2.000	2.597	-.02416	.15657	.06125	-.09450	.00457	-.00497	.15622	.15622	.07204	5.09204
2.000	4.687	-.07839	.15236	.05310	-.09156	.00269	-.00488	.15824	.15824	.41519	5.09314
2.000	8.848	.24282	.14399	.03841	-.09219	.00144	-.00595	.21778	.17962	1.21243	5.09567
2.000	13.150	.05279	.13367	.03345	-.08333	-.00315	-.00647	.36228	.22104	1.63894	5.09639
2.000	16.154	.52423	.12498	.02858	-.07596	-.00819	-.00578	.46376	.26590	1.76293	5.09697
2.000	21.397	.73161	.11048	.01803	-.07052	-.01488	-.00553	.64068	.36977	1.73317	5.09919
2.000	26.660	.93969	.09831	.01572	-.06534	-.01971	-.00703	.79568	.59468	1.56173	5.09876
2.000	31.872	1.13277	.08722	.01222	-.06702	-.02105	-.00660	.93291	.68276	1.36637	5.09912

RUN NO. 2 / 0

MACH	ALPHA	CN	CA	CLW	CY	CYH	CBL	Q	CD	L/D	BETA
2.500	-1.182	-1.12016	.14288	.04127	-.08043	.01794	-.00337	.12520	.14549	-.06564	5.07355
2.500	-.182	-.08956	.14025	.03865	-.08664	.01731	-.00352	.08917	.14550	-.63462	5.07131
2.500	.824	-.06252	.13835	.03639	-.08219	.00675	-.00338	.06450	.13744	-.66653	5.06976
2.500	1.873	-.02437	.13588	.03287	-.08338	.00618	-.00350	.02880	.13511	-.21332	5.07161
2.500	2.890	.02787	.13373	.03054	-.07964	.00522	-.00359	.01112	.13395	.09837	5.06314
2.500	4.929	.05848	.12976	.02674	-.07825	.00429	-.00360	.05708	.13516	.42233	5.06897
2.500	9.069	.21020	.12620	.01932	-.07119	.00277	-.00368	.18853	.15164	1.24233	5.06583
2.500	13.214	.34662	.11258	.01317	-.07050	.00124	-.00324	.07631	.31365	1.65701	5.06865
2.500	16.319	.45616	.10554	.00842	-.06932	-.00323	-.00315	.41077	.23093	1.78267	5.06816
2.500	21.515	.64136	.09373	.00443	-.06324	-.00304	-.00300	.58250	.32241	1.74494	5.06576
2.500	26.741	.83405	.08805	.00130	-.05504	-.00234	-.00270	.77658	.45235	1.56583	5.06586
2.500	31.932	1.04991	.07027	-.00153	-.05471	-.00172	-.00172	.61692	1.37135	5.06579	

## LA46 A/B TABULATED SOURCE DATA

INPUT-1052 (LA-46A) ORBITER (B1W5ZEF1)

(RMC0071)

PAGE 10

## PARAMETRIC DATA

BETA = .000  
BETALAP = -11.750  
ELEVN = -90.000  
SPCRK = 55.000

RUN NO. 24/0

	CN	CA	CLN	CY	CYN	CLB	QB	L/D	BETA
MACH	.20981	.16093	.11570	-.00096	.00116	.00035	-.00262	.1663	-1.37573
ALFA	-2.136	-1.9763	.17943	.02077	.02111	.0023	.1524	.18246	-.03964
BETA	-1.120	-1.9677	.09821	-.01263	.01953	.0023	.1032	.17695	-.59168
GAMMA	-1.0562	.17768	.09821	-.01263	.01953	.0023	.0520	.17432	-.03862
DELTA	-1.056	-.096	.17517	.08959	.01156	.0018	.0520	.17432	-.03862
EPSILON	.962	-.04908	.17517	.08959	.01156	.0018	.0520	.17432	-.03862
ZETA	.950	2.021	.020641	.17253	.08222	.0028	.0139	.0016	.17110
ETA	.950	4.114	.19877	.16673	.06904	.0014	.02149	.0004	.09653
THETA	.950	8.355	.15423	.04659	.01254	.00270	.0209	.29337	.19895
PSI	.950	12.518	.52321	.14724	.03211	.00385	.0242	.0043	.47660
NU	.950	15.714	.65893	.14270	.02997	.00246	.0246	.0064	.25748
OMEGA	.950	21.910	.91297	.15288	.03706	.00377	.0279	.0094	.605912
RHO	.950	26.333	1.16371	.11722	.05475	-.00319	.0222	.0164	.1.0515
SIGMA	.950	28.399	1.27201	.11134	.05904	-.00235	.0255	.0065	.0.4950

RUN NO. 26/0

	CN	CA	CLN	CY	CYN	CLB	QB	L/D	BETA
MACH	ALPHA	-1.12159	.15309	.00241	.0021	.0012	-.11762	.19616	-.03222
2.000	-1.472	-.07623	.1571	.0361	.0059	.0016	-.07720	.19563	-.03218
2.000	-4.95	-.03894	.15976	.04856	.0242	.00769	-.06322	.19537	-.03216
2.000	-557	-.02236	.14935	.04503	.01226	.0038	-.03115	.19536	-.03215
2.000	1.565	2.638	.04556	.04108	.0175	.0028	-.03019	.19522	-.03214
2.000	4.721	.12696	.14177	.03620	.02224	.0036	-.03013	.11467	.1.05111
2.000	8.898	.26693	.13393	.03352	.0105	.0012	-.02275	.17660	-.03208
2.000	13.069	.44893	.12736	.04042	.02161	.0018	-.02242	.45751	.22551
2.000	16.223	.57465	.12230	.04601	-.01227	.00165	-.02051	.51780	.27804
2.000	21.493	.79895	.11187	.05386	-.01187	.00248	-.02077	.71241	.1.77713
2.000	26.789	1.03393	.09660	.05621	-.00669	.00263	-.02094	.87887	.55193
2.000	32.033	1.27375	.08378	.06387	-.01328	.01274	-.02177	.74613	1.38111

LINEAR TRANSIENT SOURCE DATA

UPUT-1096 (16-A-16A) OBLITERE (B1/WNDETFI)

126

FACE 11

UFMFT-1092 (LA-464) OMEBITER (B1WWS2E1F1)

GRAMMATICAL

$$\text{BETA} = 5.000 \quad \text{ELEVIR} = -10.000$$

	CA	CN	CH	CH	CH	CH
ALPHA						
-2.140	.500	-.2051	.17775			
-1.124	.500	-.15979	.17699			
-1.109	.500	-.10564	.17591			
MACH						
.500	.500	.956	-.05148	.17457		
.500	.500	2.012	.50488	.17239		
.500	.500	4.106	.10740	.16751		
.500	.500	6.327	.31643	.15658		
WACH						
.500	.500	.51751	.51763	.14687		
.500	.500	15.711	.66887	.13969		
.500	.500	25.996	.97982	.12456		
.500	.500	26.306	1.13665	.11631		
WCH						
.500	.500	27.733	1.19913	.11574		

PARAPHRATIC D

<b>BETA</b>	<b>5.15731</b>
<b>5.09432</b>	<b>5.09432</b>
<b>5.06921</b>	<b>5.06921</b>
<b>5.03828</b>	<b>5.03828</b>
<b>5.00442</b>	<b>5.00442</b>
<b>4.9672</b>	<b>4.9672</b>
<b>4.9211</b>	<b>4.9211</b>
<b>4.8725</b>	<b>4.8725</b>
<b>4.8196</b>	<b>4.8196</b>
<b>4.7617</b>	<b>4.7617</b>
<b>4.7033</b>	<b>4.7033</b>
<b>-10.000</b>	<b>-10.000</b>
<b>55.000</b>	<b>55.000</b>

PARAPHRASE DATA

126

BET <sub>1</sub>	=	-10.000
BET <sub>2</sub>	=	-11.700
SLV <sub>1</sub>	=	-0.000
SLV <sub>2</sub>	=	55.000

三

<b>BETA</b>	.70	.75	.80	.85	.90
64492	-.765677				
45200	-.054659				
21463	-.065559				
55216	-.055447				
24295	-.056558				
69277	-.060803				
43369	-.065117				
76812	-.055322				
84215		-.061436			
77397		-.055443			
59200		-.065115			
336742		-.055237			

$$\Delta H = -10,000$$

78

## LWS A/B TABULATED SOURCE DATA

PAGE 12

INPUT-1092 (LA-46A) ORBITER (B1WNS2E1F1)

(REFDSS1)

## PARAMETRIC DATA

BETA = 5.000 EFLAT = -10.000  
 BCFLAP = -11.700 SPKAN = 55.000

RUN NO. 27 / 0

MACH	ALPHA	CN	CA	CLW	CY	CYN	CLB	QA	CD	UD	BETA
2.000	-1.462	-.12371	.15183	.05403	-.09668	.00713	-.00427	-.11976	.15494	-.77316	5.39370
2.000	-1.454	-.08160	.15057	.05092	-.09644	.00578	-.00331	-.08950	.15121	-.93344	5.38380
2.000	-.04273	.04273	.14923	.06995	-.09510	.00630	-.00420	-.04116	.14861	-.23691	5.38322
2.000	.559	-.04273	.14768	.04336	-.09240	.00327	-.00423	-.00376	.14763	-.52349	5.38345
2.000	1.654	.09237	.14646	.03941	-.09138	.00444	-.00416	.03456	.14822	.23119	5.38329
2.000	2.647	.04137	.14646	.03947	-.08744	.00368	-.00444	.11452	.15231	.74559	5.38371
2.000	4.711	.12614	.14243	.03457	-.08576	.00233	-.00539	.26245	.17698	1.48295	5.38352
2.000	8.894	.26656	.13427	.03197	-.08576	.00576	-.00577	.49811	.22630	1.81142	5.38357
2.000	13.990	.48876	.12799	.04120	-.07894	.00776	-.00578	.51193	.27583	1.88169	5.38322
2.000	16.221	.57542	.11987	.04395	-.07431	.00463	-.00544	.56470	.30572	.39556	5.37656
2.000	21.491	.79675	.10626	.04882	-.06470	-.00699	-.00572	.77246	.56445	.54732	5.37222
2.000	26.782	1.02354	.09647	.05720	-.05676	-.01131	-.02645	.87928	.102263	1.37671	5.36763
2.000	32.020	1.26569	.08759	.06248	-.04858	-.01394	-.02764	.74280			

RUN NO. 23 / 0

MACH	ALPHA	CN	CA	CLW	CY	CYN	CLB	QA	CD	UD	BETA
2.500	-1.135	-.08361	.13167	.02332	-.08797	.00751	-.00354	-.00366	.13450	-.62425	5.35344
2.500	-.153	-.05740	.13160	.02083	-.08906	.00697	-.00356	-.05715	.13173	-.43335	5.35383
2.500	.863	-.02388	.13042	.01968	-.08526	.00661	-.00356	-.02583	.13025	-.19833	5.35270
2.500	1.875	.05663	.12926	.01815	-.08656	.00586	-.00364	.02239	.12941	.91646	5.35443
2.500	2.910	.04463	.12763	.01633	-.08140	.00515	-.00367	.03810	.12973	.29356	5.35447
2.500	4.963	.11696	.12455	.01868	-.07653	.00382	-.00355	.10370	.13423	.76741	5.36789
2.500	9.105	.26883	.11779	.02339	-.07595	.00367	-.00498	.22459	.15521	1.44377	5.36735
2.500	13.269	.39301	.11103	.02614	-.07340	.00114	-.00571	.35703	.19827	1.82069	5.36755
2.500	16.372	.50023	.10593	.02913	-.06865	-.01110	-.00576	.45996	.24264	1.85395	5.36389
2.500	21.569	.75825	.09468	.03387	-.06920	-.01431	-.00656	.62956	.34675	1.78225	5.36249
2.500	26.864	.92329	.08446	.04168	-.05128	-.05522	-.00561	.79304	.49526	1.59650	5.36545
2.500	32.025	1.15983	.07969	.04837	-.04261	-.05810	-.00614	.92320	.67516	1.36032	5.36194

LMS M8 TABULATED SOURCE DATA

一

BIMINERIAL DATA

BLT1	=	1.354	=	11.765	=	55.000
		REV1	=	1.000	=	-50.000

LA46 A/B TABULATED SOURCE DATA  
UFUT-1092 (LA-46A)ORBITER (B1WMS2E1F1)

PAGE 14

(FMG309)

PARAMETRIC DATA

MACH	ALPHA	CN	CA	CLN	CY	CYN	CLL	QA	CD	L/C	BETA	
2.500	-1.216	-1.12380	.14090	.03994	.03703	.03739	.02012	.12026	.14350	.04227	-2.0613	
2.500	-.167	-.09375	.13896	.03824	.03623	.03644	.02037	.08235	.13921	.59873	-2.0658	
2.500	.819	-.05312	.11743	.03693	.03617	.03734	.02026	.05508	.13566	.05373	-2.0654	
2.500	1.881	-.01625	.13611	.03582	.03724	.03747	.02037	.08271	.13544	.16768	-2.0659	
2.500	2.893	.01639	.13394	.03493	.03694	.03694	.02019	.02019	.01162	.13479	.08626	-2.0659
2.500	4.938	.07442	.13012	.03472	.03665	.03665	.02020	.05529	.05294	.13605	.46265	-2.06516
2.500	9.096	.21636	.12102	.03349	.02672	.02672	.02025	.02025	.19453	.15367	.126597	-2.06519
2.500	13.235	.35338	.11314	.04016	.02398	.02398	.02026	.02026	.32713	.19150	.137119	-2.0653
2.500	16.355	.46395	.10848	.04695	.02515	.02515	.02017	.02017	.41571	.21551	.176891	-2.06485
2.500	21.566	.65776	.09801	.05952	.02417	.02417	.02016	.02016	.57569	.33292	.172922	-2.06396
2.500	26.814	.87389	.08624	.05622	.02388	.02388	.02015	.02015	.74153	.47116	.157273	-2.06350
2.500	32.323	1.08745	.07649	.07623	.02352	.02352	.02014	.02014	.88138	.64145	.137405	-2.06321

UFUT-1092 (LA-46A)ORBITER (B1WMS2E1F1) (FMG309)

PARAMETRIC DATA

MACH	ALPHA	CN	CA	CLN	CY	CYN	CLL	QA	CD	L/C	BETA
1.500	-2.199	-.27557	.19547	.14677	-.11534	.01219	-.02490	-.26767	.20590	-.13006	5.06261
1.500	-1.169	-.22024	.19430	.13770	-.11164	.01153	-.02469	-.21263	.19873	-.10672	5.07951
1.500	-.136	-.16229	.19275	.12880	-.10938	.01100	-.02491	-.16183	.19314	-.03768	5.07760
1.500	.911	-.10793	.19554	.11974	-.10752	.01026	-.02513	-.11995	.18880	-.58768	5.07669
1.500	1.962	-.05468	.16888	.11226	-.10534	.00920	-.02531	-.06111	.16689	-.32770	5.07567
1.500	4.570	.05387	.18534	.09445	-.09966	.02697	-.02617	.04058	.18869	.21538	5.07296
1.500	6.286	.26591	.17458	.07547	-.09393	.00549	-.02687	.23310	.25986	.11374	5.06958
1.500	12.517	.46624	.16296	.06004	-.09553	.02137	-.02073	.42227	.25819	.162776	5.07191
1.500	15.670	.61133	.15101	.05348	-.09945	.03136	-.02816	.54782	.31052	.176320	5.07722
1.500	20.963	.85334	.13416	.07169	-.07794	.00721	-.02774	.74867	.43937	.173923	5.06567
1.500	26.275	1.09639	.12298	.09203	-.05637	.01823	-.02696	.92660	.59561	.153820	5.06789
1.500	28.314	1.18246	.12771	.07649	-.04655	.02344	-.02578	.66377	.147456	.105613	

## LAMS A/B TABULATED SOURCE DATA

INPUT-1082 (LA-46A) ORBITER @1WSE1F1

PAGE 15

(CONT'D)

## PARAMETRIC DATA

BETA = 5.370 ELEV = -20.000  
 BCFAP = -11.763 SPARK = 55.000

RUN NO. 33/0						
MACH	ALPHA	CN	CA	CLW	CY	CYN
2.000	-1.497	-15470	.16250	.07523	-.10220	.01767
2.050	-476	-11309	.16037	.07185	-.09954	.02721
2.070	-535	-97114	.15876	.06905	-.09741	.02558
2.090	1.583	-22846	.15726	.06447	-.09591	.02372
2.090	2.513	.01237	.15612	.06136	-.09323	.02165
2.070	4.696	.09443	.15244	.05584	-.08715	.01936
2.070	8.976	.25620	.1452	.05246	-.08649	.01652
2.070	13.975	.41758	.13262	.05175	-.08756	.01392
2.070	16.223	.54272	.12624	.05606	-.07446	.01174
2.070	21.467	.76381	.11082	.07241	-.06735	.00863
2.070	26.761	.99463	.09983	.08119	-.06123	.00602
2.070	31.995	1.222317	.09143	.05105	-.05113	.00411

RUN NO. 29/0						
MACH	ALPHA	CN	CA	CLW	CY	CYN
2.500	-1.154	-10946	.14954	.05595	-.08771	.02674
2.500	-229	.28732	.13886	.05463	-.08558	.02566
2.500	-875	.04946	.13705	.05329	-.08728	.02556
2.500	1.041	-.01645	.13477	.03185	-.08519	.02518
2.500	2.987	.01746	.13271	.03566	-.08229	.02472
2.500	4.933	.08247	.12856	.02342	-.08156	.02418
2.500	9.987	.21498	.12126	.03070	-.07684	.02394
2.500	13.232	.35150	.11341	.03967	-.07147	.02046
2.500	16.339	.46486	.10715	.0466	-.06821	.01717
2.500	21.556	.66371	.09451	.03510	-.06120	.01421
2.500	26.857	.87753	.08461	.05936	-.05955	.01156
2.500	32.314	1.08225	.07799	.07534	-.04510	.00835

RUN NO. 33/1						
MACH	ALPHA	CN	CA	CLW	CY	CYN
2.000	5.3734	5.3722	5.3719	5.3716	5.3713	5.3710
2.050	5.3733	5.3721	5.3718	5.3715	5.3712	5.3709
2.070	5.3732	5.3720	5.3717	5.3714	5.3711	5.3708
2.090	5.3731	5.3719	5.3716	5.3713	5.3710	5.3707
2.090	5.3730	5.3718	5.3715	5.3712	5.3709	5.3706
2.070	5.3729	5.3717	5.3714	5.3711	5.3708	5.3705
2.070	5.3728	5.3716	5.3713	5.3710	5.3707	5.3704
2.070	5.3727	5.3715	5.3712	5.3709	5.3706	5.3703
2.070	5.3726	5.3714	5.3711	5.3708	5.3705	5.3702
2.070	5.3725	5.3713	5.3710	5.3707	5.3704	5.3701
2.070	5.3724	5.3712	5.3709	5.3706	5.3703	5.3700
2.070	5.3723	5.3711	5.3708	5.3705	5.3702	5.3700
2.070	5.3722	5.3710	5.3707	5.3704	5.3701	5.3700
2.070	5.3721	5.3709	5.3706	5.3703	5.3700	5.3700
2.070	5.3720	5.3708	5.3705	5.3702	5.3700	5.3700
2.070	5.3719	5.3707	5.3704	5.3701	5.3700	5.3700
2.070	5.3718	5.3706	5.3703	5.3700	5.3700	5.3700
2.070	5.3717	5.3705	5.3702	5.3700	5.3700	5.3700
2.070	5.3716	5.3704	5.3701	5.3700	5.3700	5.3700
2.070	5.3715	5.3703	5.3700	5.3700	5.3700	5.3700
2.070	5.3714	5.3702	5.3700	5.3700	5.3700	5.3700
2.070	5.3713	5.3701	5.3700	5.3700	5.3700	5.3700
2.070	5.3712	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3711	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3710	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3709	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3708	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3707	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3706	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3705	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3704	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3703	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3702	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3701	5.3700	5.3700	5.3700	5.3700	5.3700
2.070	5.3700	5.3700	5.3700	5.3700	5.3700	5.3700

## LA46 A/B TABULATED SOURCE DATA

(REFC011)

UFT-1092 (LA-46) ORBITER (B1WSE4EF1)

MACH	ALPHA	PARAMETRIC DATA						BETA = .070 BOFLP = -11.700	ELEVTR = .070 SPARK = 55.000	
		CN	CA	CLW	CY	CYN	CP			
1.500	-2.091	-.14534	.16701	.0721	-.00040	.00213	.00041	-.13915	.17221	-.00005
1.500	-1.070	-.09347	.16624	.06646	-.30260	.00246	.00033	-.00035	.16795	-.53792
1.500	-.638	-.03916	.16549	.06138	-.00146	.00214	.00034	-.03957	.65550	-.23658
1.500	1.004	.01468	.16435	.05760	-.00151	.00234	.00022	.01201	.64558	-.05870
1.500	2.066	.07752	.16219	.05349	-.00081	.00224	.00039	.06463	.16463	-.05863
1.500	4.178	.17697	.15451	.04915	-.00291	.00338	.00017	.16524	.16699	-.00001
1.500	8.410	.38872	.14081	.04237	-.00354	.00358	.00010	.36276	.21495	1.77776
1.500	12.647	.59729	.14363	.03822	-.00519	.00361	.00024	.51315	.27092	2.53513
1.500	15.885	.74824	.14451	.03371	-.01648	.00247	.00041	.68059	.14265	1.96513
1.500	21.110	1.02658	.13663	.03583	-.00827	.00258	.00037	.86981	.49521	1.81585
1.500	26.441	1.27725	.12347	.03481	-.00995	.00233	-.00016	.98867	.67927	1.62269
1.500	28.493	1.37437	.12117	.03718	-.01105	.00304	.00033	1.15010	.76213	1.57975
<hr/>										
MACH	ALPHA	CN	CA	CLW	CY	CYN	CP	CD	L/C	BETA
2.000	-1.430	-.07635	.14982	.02918	.00259	.00144	.00012	-.07459	.15173	-.49197
2.000	-.413	-.03590	.14991	.02617	.00211	.00136	.00019	-.03482	.14916	-.23345
2.000	-.693	.00461	.14937	.02673	.00343	.00220	.00019	.01356	.18411	-.02181
2.000	1.647	.04707	.14333	.12814	.00179	.00197	.00020	.04291	.15113	.29568
2.000	2.681	.08773	.14201	.02749	.00121	.00131	.00010	.58199	.15956	.55490
2.000	4.783	.15966	.13958	.02898	-.00226	.00160	.00017	.6312	.15380	1.06559
2.000	8.963	.34213	.13512	.03374	-.00174	.00150	.00024	.31691	.16668	1.69765
2.000	13.156	.51090	.12919	.04078	-.00247	.00165	.00034	.46809	.24216	1.93363
2.000	16.297	.64513	.12225	.04314	-.00346	.00178	.00036	.58434	.30129	1.44594
2.000	21.580	.87765	.11684	.04615	-.00519	.00218	.00039	.77342	.47314	1.79356
2.000	26.876	1.11563	.10545	.04557	-.00681	.00138	.00046	.94699	.59631	1.58013
2.000	32.127	1.35797	.09861	.04987	-.00929	.00217	.00043	1.09749	.81584	1.36192

## LA46 A/B TABULATED SOURCE DATA

PAGE 17

## UWFT-1092 (LA-46) ORBITER (B1WNSDCE1F1)

(RPGC11)

## PARAMETRIC DATA

BETA = .000  
BCFLAP = -11.700  
ELEVTR = .000  
SPDRK = 99.000

RUN NO. 40/0

MACH	ALPHA	CN	CA	CLN	CY	CYN	CBL	Q	CD	L/D	BETA
2.500	-1.146	-0.06013	-13168	.006976	.00045	.00046	.00046	-.00546	-.49233	-.06481	
2.500	-.133	-0.05523	-13080	.01023	.00478	.00056	.00056	-.03492	-.26603	-.06165	
2.500	.867	-0.05569	-12827	.01154	.00497	.00061	.00061	-.00217	-.06576	-.06217	
2.500	1.868	.02819	-12837	.01282	.00021	.00123	.00123	.00162	.19425	-.06112	
2.500	2.921	.05988	-12419	.01411	.00356	.00123	.00123	.00340	.42220	-.06362	
2.500	5.071	-13869	-12984	.01946	.00329	.00179	.00179	.00211	.12763	-.06177	
2.500	9.129	.26669	-11653	.01999	.00192	.00115	.00115	.00226	.24473	-.05528	
2.500	13.302	.42695	-11011	.02507	.00382	.00145	.00145	.00163	.15735	-.05592	
2.500	16.423	.55352	-10554	.02990	.00151	.00140	.00140	.00224	.20539	-.05966	
2.500	21.658	.76213	-9929	.03618	.00310	.00168	.00168	.00465	.67205	-.05535	
2.500	26.920	.98561	-9919	.03615	.00378	.00172	.00172	.00556	.83799	-.05537	
2.500	32.136	1.21451	-98231	.04126	.00369	.00101	.00101	.0079	.88465	-.05593	

## UWFT-1092 (LA-46) CRBITER (B1WNSDCE1F1)

## PARAMETRIC DATA

BETA = .000  
BCFLAP = -11.700  
ELEVTR = .000  
SPDRK = 99.000

RUN NO. 43/0

MACH	ALPHA	CN	CA	CLN	CY	CYN	CBL	Q	CD	L/D	BETA
1.500	-2.092	-1.14390	-17021	.06794	-1.0702	.00862	-.00444	-.03699	1.732	-.78134	2.09933
1.500	-1.061	-0.09079	-17031	.06353	-1.0201	.00774	-.00768	-.08762	1.796	-.50955	2.09460
1.500	-.045	-0.07935	-16922	.06907	-.06614	.00748	-.00564	-.03779	1.6925	-.22330	2.09001
1.500	1.058	0.01507	-16932	.05531	-.06653	.00724	-.00517	0.01210	1.6866	.07174	2.08956
1.500	2.067	0.06611	-16936	.05017	-.06577	.00652	-.00569	.00616	.16875	.37371	2.08952
1.500	4.162	1.01073	-15986	.04473	-.06261	.00541	-.00566	.00886	.17263	.97812	2.08701
1.500	8.411	.38578	-15111	.03647	-.06569	.00477	-.00516	.00548	.25821	1.74330	2.08335
1.500	12.630	.58757	-14654	.03640	-.06417	.00337	-.00564	.54082	.27136	1.99300	2.08222
1.500	15.601	.74153	-14114	.03625	-.06045	.00261	-.00746	.67518	.33773	1.99889	2.08171
1.500	21.116	1.01207	-12577	.03188	-.07454	-.00397	-.00668	.69844	.46287	1.86561	2.08124
1.500	26.436	1.26804	-11680	.03137	-.0686	-.01261	-.00747	1.58265	.67172	1.61415	2.07884
1.500	36.604	1.36604	-11935	.03928	-.05439	-.01711	-.00672	1.16468	.75432	1.51777	2.07673
26.486	28.000										

## LA46 A/B TABULATED SOURCE DATA

PAGE 10

## UWWT-1092 (LA-46A) ORBITER (B1W5DC4E1F1)

(RMED12)

## PARAMETRIC DATA

BETA = 5.000 ELEVRA = .000  
 BCFLAP = -11.770 SFDBRK = 95.520

RUN NO. 45 / 0

MACH	ALPHA	CN	CA	CLW	CY	CYN	CBL	CL	CD	L/D	BETA
2.000	-1.442	-.08258	.14855	.02787	-.09964	.00563	-.00419	-.07891	.15759	-.32402	5.07483
2.000	-.421	-.03979	.14775	.02744	-.09575	.00561	-.00430	-.03870	.1804	-.26142	5.07220
2.000	.594	-.00592	.14631	.02614	-.09991	.00518	-.00436	-.00244	.1629	-.01669	5.07506
2.000	1.633	.04183	.14481	.02526	-.09344	.00518	-.00442	.03769	.14594	.25827	5.06937
2.000	2.674	.08129	.14353	.02481	-.09305	.00489	-.00451	.07851	.1735	.53275	5.06927
2.000	4.758	.17057	.14019	.02535	-.08823	.00449	-.00485	.15385	1.02926	.00610	5.06610
2.000	8.952	.34974	.13361	.02993	-.08618	.00292	-.00568	.16503	1.76751	.170695	5.05932
2.000	13.155	.51056	.12713	.03550	-.08129	.00256	-.00646	.47164	.247079	1.9569	5.05330
2.000	16.299	.68723	.12151	.03627	-.08113	.00104	-.00684	.5871	.29627	1.96820	5.05474
2.000	21.573	.87699	.11355	.03924	-.07327	-.00629	-.00717	.77381	.42804	1.80777	5.05320
2.000	26.870	1.1669	.10244	.04316	-.03947	-.01392	-.00620	.94883	.59608	1.59345	5.05245
2.000	32.159	1.3986	.09555	.04677	-.06947	-.02113	-.00568	1.05659	.79482	1.35844	5.05563

RUN NO. 41 / 0

MACH	ALPHA	CN	CA	CLW	CY	CYN	CBL	CL	CD	L/D	BETA
2.500	-1.135	-.08351	.13058	.00846	-.09068	.00563	-.00377	-.0891	.13161	-.45215	5.06356
2.500	-.138	-.03410	.12939	.00707	-.09149	.00618	-.00369	-.0378	.12948	-.26953	5.06959
2.500	.863	-.00645	.12761	.00864	-.09551	.00616	-.00429	-.01037	.12477	-.00634	5.06306
2.500	1.914	.03969	.12595	.00846	-.09287	.00579	-.00425	.03548	.12720	.27893	5.06106
2.500	2.633	.08305	.12470	.01063	-.09353	.00346	-.00426	.01959	.12776	.42294	5.06198
2.500	5.053	.13775	.12105	.01280	-.09022	.00317	-.00475	.12666	.13261	.95112	5.05904
2.500	9.147	.18291	.11377	.01750	-.08339	.00489	-.00568	.22123	.19730	1.66768	5.05379
2.500	13.307	.43515	.10829	.02054	-.08306	.00349	-.00561	.20554	.21054	1.99912	5.05506
2.500	16.423	.59071	.10415	.02460	-.07923	.00151	-.00667	.49879	.25661	1.93141	5.05353
2.500	21.646	.79791	.09547	.02968	-.06932	-.00412	-.00672	.66925	.36332	1.81704	5.05298
2.500	26.910	.97918	.08632	.03340	-.05768	-.0057	-.00655	.63409	.52214	1.65357	5.04736
2.500	32.116	1.20362	.06212	.03920	-.04942	-.01044	-.01721	.70946	1.37371	5.04347	

LINEARIZED SOURCE DATA

REF ID: A6A0CB811E (B1WMS9AC4E1F)

ପ୍ରମାଣିତ

PARAMETRIC DATA											
					BETA = .000	ELEVTR = -10.000	SFBRK = 55.000				
					BDFLAP = -11.700						
<b>IRMEG131</b>											
RUN NO.	56 / 0	CA	CLW	CY	CYN	CBL	CL	L/C	BETA		
MACH											
ALPHA	CN	.-21270	.16326	.11620	.10593	.00040	-.20968	.19113	-.00621		
-2.151	-16206	.18270	.10100	.00552	.00177	.00056	-.15649	.18577	-.00425		
-1.112	-.09962	.18135	.10610	.00476	.00231	.00038	-.09935	.18149	-.05475		
-.984	-.04880	.17998	.10173	.00607	.00188	.00032	-.05162	.17913	-.08931		
-.957	-.00686	.17783	.09842	.00483	.00223	.00012	.00000	.17796	-.00335		
2.017											
MACH											
ALPHA	CN	.11458	.09154	.00141	.00020	.00174	.00032	.19181	.18156		
1.950	4.131	.16464	.08456	.00141	.00216	.00205	.29960	.20147	1.42346		
1.900	8.366	.32270	.08239	.00194	.00275	.00253	.49149	.26858	1.82953		
12.612	.53818	.15260	.08689	.00156	.00257	.00236	.62061	.32990	1.88122		
1.950	15.764	.14865	.07972	.00156	.00256	.00236	.84732	.46879	1.79254		
1.500	1.3512	.95270	.08159	-.00531	.00265	.00191	-.10102	.1.03595	1.56957		
21.994	26.408	.12292	.08397	-.00649	.00232	.00197	-.10377	.1.10374	1.50466		
1.950	28.465	.1.21769	.08768	-.10413	.00176						
RUN NO.	58 / 0	CA	CLW	CY	CYN	CBL	CL	L/C	BETA		
MACH											
ALPHA	CN	.15643	.00654	.00148	.00221	-.11719	.15945	-.73493	-.05621		
-1.454	-.12120	.15485	.05577	.00210	.00113	-.07596	.15244	-.48888	-.05621		
-.444	-.07719	.15399	.05329	.00134	.00019	-.03932	.15361	-.25597	-.05621		
-.33781	-.15250	.15313	.05553	.00156	.00010	-.04447	.15268	-.52766	-.05621		
-.351	1.611	.15198	.05553	.00156	.00013	-.03203	.15220	-.19526	-.05621		
2.000	2.653	.14692	.05349	.00121	.00011	-.02616	.12540	-.15782	-.05621		
2.900	4.736	.13801	.05143	.00143	.00012	-.02110	.28289	-.18655	1.51561		
2.950	8.939	.13084	.05143	.00143	.00012	-.01712	.43145	.25683	1.82176		
2.900	13.128	.47397	.13265	.06487	.00035	-.01154	.58466	.29244	1.87550		
2.950	16.277	.69866	.12704	.06687	-.0004	.00154	.67145		-.95500		
2.900	21.548	.89226	.11794	.07455	-.00286	.00208	.72728	.41794	1.76417		
2.900	26.847	1.07159	.10394	.07636	-.00549	.00129	.90125	.57644	1.57641		
2.950	32.092	1.30617	.09301	.08641	-.00745	.00180	.1.03716	.77274	1.35897		

## LA46 A/B TABULATED SOURCE DATA

PAGE 20

## UFT-1092 (LA-46A) ORBITER (B1WSDC4E1F1)

(RPTD13)

## PARAMETRIC DATA

BETA = .000  
BCFLAP = -11.700 SECBRK = 95.000

RUN NO.	90 / 0	CN	CA	CLW	CY	CWN	CR	Q	CD	L/D	BETA
MACH											
ALPHA	-1.192	-.39801	1.3744	.02998	.00263	.00121	-.00027	.13938	-.68321	-.55630	
2.500	-1.153	-.05961	1.3550	.02975	.00139	.00096	.00010	.13565	-.43265	-.55876	
2.500	-1.032	-.02807	1.3378	.03114	.00246	.00135	-.00011	.09095	-.22536	-.35842	
2.500	1.877	.00705	1.3209	.03211	.00171	.00119	-.00011	.00272	.13225	.57572	
2.500	2.914	.04512	1.3047	.03383	.00362	.00119	.00016	.03344	.13234	.52268	
2.500	4.970	.10396	1.2704	.03574	.00310	.00260	-.00016	.02537	.13557	.68280	
2.500	9.117	.24287	1.1954	.03774	.00170	.00259	-.00017	.02857	.15651	1.41116	
2.500	13.270	.38480	1.1303	.04569	.00276	.00254	-.00016	.34850	.19834	1.73746	
2.500	16.385	.55570	1.0841	.05456	.00266	.00238	-.00028	.45458	.22656	1.64293	
2.500	21.619	.70898	0.9639	.06744	.00478	.00226	-.00013	.62165	.35328	1.75965	
2.500	26.887	.92819	0.8944	.07644	.00598	.00141	-.00043	.78740	.49953	1.57630	
2.500	32.594	1.15331	0.7952	.08567	-.00537	.00098	-.00055	.93465	.60339	1.37370	

(RPTD14)

## PARAMETRIC DATA

BETA = .000  
BCFLAP = -11.700 SECBRK = 95.000

## UFT-1092 (LA-46A) ORBITER (B1WSDC4E1F1)

(RPTD14)

## PARAMETRIC DATA

BETA = .000  
BCFLAP = -11.700 SECBRK = 95.000

RUN NO.	57 / 0	CN	CA	CLW	CY	CWN	CR	Q	CD	L/D	BETA
MACH											
ALPHA	-2.148	-.21446	1.18137	1.12260	-.10335	.01010	-.00176	.20551	.16913	1.07605	5.07623
1.500	1.500	-.11230	1.15563	1.06800	1.0679	-.01122	-.00492	-.15050	.83777	-.81659	5.07401
1.500	1.504	-.094	1.10375	1.17994	1.0199	-.00608	-.00517	-.11045	.18511	.57439	5.07360
1.500	1.506	.957	1.04041	1.17958	1.07665	-.00634	-.00550	-.05121	.17824	-.28897	5.07107
1.500	2.021	.02600	1.17511	1.09569	1.02398	-.00804	-.00581	-.01023	.17761	-.00131	5.06817
1.500	4.134	.08610	1.17526	1.08610	1.08608	-.00713	-.00564	-.01021	.16121	.57196	5.06519
1.500	6.364	.13271	1.1663	.57937	-.08829	.01154	-.00752	.29968	.21476	1.42591	
1.500	12.612	.53532	1.1576	.07810	-.07725	.01254	-.00761	.48844	.26881	1.81722	5.55619
1.500	15.767	.68642	1.14734	.07787	-.07733	.00015	-.00816	.62056	.32832	1.89010	5.06269
1.500	21.012	.95020	1.1339	.07854	-.07791	-.00449	-.00883	.64510	.48450	1.80852	5.06217
1.500	26.396	1.25085	1.11905	.06349	-.05735	-.01299	-.00765	1.02879	.60447	1.59934	5.05916
1.500	28.449	1.29915	1.1716	.06017	-.05363	-.01655	-.00689	1.06645	.72191	1.30687	5.05933

L446 A/B TABULATED SOURCE DATA  
UPW-1092 (L4-46A) ORBITER (B1W5DC4E1F1)

PAGE 21  
(PMS014)

PARAMETRIC DATA

RUN NO.	59 / 0						61 / 0					
	ALPHA	CN	CA	CLN	CY	CYN	CDL	Q	CD	L/D	BETA	
MACH												
2.000	-1.465	-1.12401	.15575	.05445	-.09654	.07710	-.00407	-.11996	.15807	-75519	5.07255	
2.000	-1.449	-.07953	.15446	.05271	-.09325	.06850	-.00427	-.07871	.15506	-50735	5.07198	
2.000	.559	-.54299	.15520	.05149	-.09257	.06617	-.00437	-.04156	.15260	-27215	5.05976	
2.000	1.605	.00562	.15153	.05145	-.08947	.05626	-.00448	.02288	.15166	.01501	5.06553	
2.000	2.653	.05043	.15832	.04977	-.08951	.05178	-.00456	.04342	.15249	.28475	5.05771	
2.000	4.740	.13749	.14703	.05492	-.08650	.05053	-.00469	.12486	.15769	.76079	5.05483	
2.000	6.935	.30632	.14571	.05383	-.08165	.04932	-.00558	.28696	.18658	1.57563	5.05168	
2.000	13.134	.47614	.13283	.05679	-.07646	.04281	-.00642	.43350	.23755	1.82489	5.05332	
2.000	16.275	.61265	.12597	.05361	-.07635	.04032	-.00677	.55279	.29262	1.86959	5.05337	
2.000	21.554	.84131	.11542	.05837	-.07037	.03758	-.00711	.74008	.41642	1.77723	5.05979	
2.000	26.840	1.06886	.10179	.07473	-.06881	.031361	-.00807	.95737	.77452	1.79803	5.05233	
2.000	32.086	1.35001	.09252	.08497	-.06958	.01968	-.00933	1.35314	.79547	1.36886	5.05476	
MACH												
2.500	-1.153	-.09426	.13646	.02742	-.09751	.05633	-.00360	-.09149	.13833	-.65141	5.05711	
2.500	-1.128	-.05550	.13435	.02797	-.08594	.05617	-.00377	-.05514	.13450	-.40996	5.05591	
2.500	.845	-.02867	.13112	.02820	-.06157	.01571	-.00375	-.05093	.13268	-.23312	5.05237	
2.500	1.879	.01376	.13772	.02925	-.06285	.01532	-.00416	.07846	.13111	.07241	5.05333	
2.500	2.916	.04343	.12557	.02245	-.06211	.01518	-.00410	.03618	.13161	.27943	5.06329	
2.500	4.987	.11326	.12561	.03241	-.08877	.00512	-.00456	.16192	.13497	.75517	5.06017	
2.500	9.115	.24169	.11676	.03394	-.08537	.00423	-.00550	.22012	.15559	1.41470	5.05759	
2.500	13.289	.38944	.11211	.04116	-.04332	.02055	-.00632	.35331	.19880	1.77989	5.05772	
2.500	16.394	.59962	.10722	.05125	-.08040	.01087	-.00646	.47493	.24653	1.85913	5.05821	
2.500	21.524	.70986	.09759	.05558	-.07205	.00582	-.00619	.62313	.35199	1.77729	5.05446	
2.500	26.874	.92280	.08781	.05827	-.05756	.01099	-.00530	.79345	.49545	1.58129	5.04779	
2.500	32.981	1.16296	.08770	.04626	-.05441	-.01496	-.00529	.93162	.70377	1.32944	5.04798	

## LA46 A/B TABULATED SOURCE DATA

PAGE 22

UP-IT-1092 (LA-46A) ORBITER (B1WSDCE1F1)

(RNGC151)

## PARAMETRIC DATA

BETA = .999  
BDFLAP = -11.793 SECARK = 55.000

RUN NO. 36/ 0

MACH	ALPHA	CN	CA	CLM	CY	CYN	CBL	Q <sub>L</sub>	L/D	BETA
1.5900	-2.191	.27974	.19811	.14614	.000222	.000156	.00014	.27196	.20367	-.05620
1.5900	-1.180	.22516	.19709	.14298	-.000339	.00120	.00010	.22100	.20169	-.01792
1.5900	-1.143	.16699	.19621	.13750	-.00011	.00120	.00010	.16630	.19663	-.01829
1.5900	-.915	.11203	.19543	.13335	-.00143	.00142	.000202	.11151	.19362	-.01721
1.5900	1.970	.05680	.19423	.12943	-.00005	.00120	.00034	.06345	.19217	-.00638
1.5900	4.084	.05586	.19057	.12358	-.00105	.00116	.000201	.04215	.19456	-.55716
1.5900	8.319	.26895	.17372	.11600	-.00259	.00190	.00037	.24999	.21081	1.14317
1.5900	12.561	.47687	.16394	.11656	-.00391	.00247	.00017	.42980	.26372	1.62976
1.5900	15.716	.62720	.15578	.11575	-.00506	.00229	.00024	.56156	.31985	1.75572
1.5900	21.933	.88536	.14367	.11730	-.00444	.00197	.00038	.77456	.45168	1.71483
1.5900	26.358	1.15228	.12826	.11857	-.00812	.00234	.00035	.97534	.62652	1.55758
1.5900	28.422	1.25587	.12515	.12360	-.01563	.00236	.00049	.10498	.70771	1.47657

MACH	ALPHA	CN	CA	CLM	CY	CYN	CBL	Q <sub>L</sub>	L/D	BETA
2.0000	-1.489	.15431	.16690	.07764	.00479	.00006	-.00001	-.14992	.17086	-.05060
2.0000	-.461	.11271	.16538	.07663	.00319	.00019	-.00008	-.11132	.16632	-.06515
2.0000	.543	.07123	.16435	.07623	.00343	.00010	-.00035	-.07278	.16367	-.06384
2.0000	1.576	.02743	.16280	.07595	.01295	.00032	-.00026	-.05189	.16198	-.06220
2.0000	2.639	.01746	.16083	.07589	.00217	.00025	-.00012	.01036	.16146	-.05943
2.0000	4.726	.10463	.15666	.07716	.00195	.00022	-.00016	.39137	.16475	-.55158
2.0000	6.914	.27532	.14501	.08191	-.00766	.00107	-.00011	.24953	.16592	1.34211
2.0000	13.117	.44532	.13642	.08944	-.00174	.00112	.00035	.49274	.23392	1.72168
2.0000	16.266	.58064	.12842	.09226	-.00312	.00123	.00017	.52142	.28592	1.82259
2.0000	21.534	.80682	.11948	.10137	-.00425	.00155	.00016	.70665	.49729	1.73499
2.0000	26.021	1.03530	.10540	.10764	-.00559	.00167	.00041	.87637	.56120	1.56161
2.0000	32.053	1.26339	.09526	.11953	-.00661	.00161	.00013	.75122	1.35810	-.02248



BIBLIOGRAPHY 21

BETA = 5.000 BETA = -11.200 EQUITY = -20.000

MACH	ALPHA	CN	CA
2.0000	-1.492	-1.15658	-16553
2.0000	-0.482	-1.11394	-16398
2.0000	.536	-0.07531	.16218
2.0000	1.376	-0.02814	.16349
2.0000	2.631	.01659	-15877
2.0000	4.716	.10335	.15922
2.0000	6.911	.27676	.14497
2.0000	13.115	.44912	.13576
2.0000	16.256	.58570	.12793
2.0000	21.524	.80295	.11676
2.0000	26.822	1.03470	.10429
2.0000	32.120	1.25500	.09270

6 / 83

	CA	CLM	CV	CYN	CBL	CL	CC	L/C	BETA
868	-1.4462	.54431	-.98717	.00728	-.05282	-.11568	.14703	-.76578	5.57385
643	.14325	.03665	-.19570	.00713	-.00318	-.09597	.14355	-.66535	5.57711
572	.14020	.04444	-.08716	.02688	-.01335	-.14777	.13959	-.34223	5.57419
574	.13886	.04415	-.08563	.05644	-.02343	-.02555	.13615	-.17768	5.57322
231	.13682	.04474	-.08602	.02639	-.01359	.01540	.13727	.03934	5.57357
327	.13142	.04691	-.08455	.03566	-.01401	.07159	.13813	.51829	5.57339
222	.12197	.05281	-.07945	.00519	-.00464	.21514	.15612	1.35599	5.565917
397	.11252	.05578	-.07954	.03422	-.01564	.34398	.19676	1.74824	5.57347
592	.10720	.06201	-.07071	.00195	-.00552	.44650	.22302	1.83729	5.56484
663	.09671	.07105	-.06391	.00333	-.00369	.61962	.34650	1.77238	5.56443
86	.08644	.09119	-.05249	-.051972	-.01523	.78323	.49384	1.58599	5.56764
551	.07918	.09653	-.04576	-.01332	-.00530	.91918	.66969	1.37254	5.55943

L446 A/B TABULATED SOURCE DATA  
INPUT-1092 (LA-6A) ORBITER (B11WSDC41E1F1)

PAGE 23

(RNG017)

PARAMETRIC DATA

BETA = .000 ELEVTR = .000  
BCFLAP = -11.703 SPBRK = .000

RUN NO. 46/ 0						
MACH	ALPHA	CN	CA	CLW	CY	CYN
1.500	-2.084	-.14626	.17527	.07476	.00063	.00136
1.500	-1.565	-.09226	.17431	.06899	.00222	.00149
1.500	-.529	-.03569	.17330	.06563	.00286	.00123
1.500	1.317	.01996	.17197	.05802	.00290	.00128
1.500	2.132	.07758	.16994	.05272	.00285	.00112
1.500	4.186	.18366	.16222	.04114	.00339	.00230
1.500	8.410	.39434	.15584	.03529	.00345	.00230
1.500	12.645	.65321	.15071	.03022	-.00108	.00276
1.500	15.807	.75518	.14568	.02949	-.00173	.00234
1.500	21.197	1.01345	.13874	.02314	-.01702	.00269
1.500	26.447	1.29112	.13063	.01614	-.00728	.00186
1.500	28.557	1.39665	.12900	.012221	-.00835	.00238

RUN NO. 48/ 0						
MACH	ALPHA	CN	CA	CLW	CY	CYN
2.000	-1.439	-.08693	.19406	.02686	.00447	.00261
2.000	-.424	-.24198	.15320	.02997	.00471	.00387
2.000	-.595	-.08255	.15257	.02308	.00490	.00393
2.000	1.628	.04665	.15140	.0286	.00360	.00120
2.000	2.671	.08936	.14895	.02187	.00458	.00153
2.000	4.768	.17781	.14647	.01255	.00272	.00161
2.000	8.954	.34466	.14542	.02593	.00218	.00175
2.000	13.151	.51352	.13308	.03222	-.00360	.00121
2.000	16.294	.64749	.12642	.03308	-.00209	.00143
2.000	21.575	.87825	.12549	.03156	-.00283	.00132
2.000	26.866	1.12117	.11927	.02878	-.00448	.00156
2.000	32.116	1.36342	.10327	.02931	-.00401	.00119

RUN NO. 48/ 0						
MACH	ALPHA	CN	CA	CLW	CY	CYN
2.500	-1.439	-.08693	.19406	.02686	.00447	.00261
2.500	-.424	-.24198	.15320	.02997	.00471	.00385
2.500	-.595	-.08255	.15257	.02308	.00490	.00393
2.500	1.628	.04665	.15140	.0286	.00360	.00120
2.500	2.671	.08936	.14895	.02187	.00458	.00153
2.500	4.768	.17781	.14647	.01255	.00272	.00161
2.500	8.954	.34466	.14542	.02593	.00218	.00175
2.500	13.151	.51352	.13308	.03222	-.00360	.00121
2.500	16.294	.64749	.12642	.03308	-.00209	.00143
2.500	21.575	.87825	.12549	.03156	-.00283	.00132
2.500	26.866	1.12117	.11927	.02878	-.00448	.00156
2.500	32.116	1.36342	.10327	.02931	-.00401	.00119

TABLE AFTER SOURCE DATA

A-161) SORRY IT ISN'T (INMSCA1E1F1)

1002/2017

Ergonomics Data

```

BETA = 11.500 ELEVATE = 55.000
EPS 10 = 11.500 SEASIDE = 55.000

```

DATA JOURNAL

ELTRA = 5.000  
-11.750 SEASER = 33.000  
-0.00

卷之二

## L446 A/B TABULATED SOURCE DATA

UHMT-1092 (LA-46A) ORBITER (B1W3D041EF1)

PAGE 27

(MPCDF1)

## PARAMETRIC DATA

	RUN NO.	49/ 0	CN	CA	CLM	CR	CYN	CB	Q	L/C	BETA
MACH	ALPHA	-0.0872	.15333	.02511	-.09877	.07684	-.00965	-.08161	.15955	-.32626	3.35210
2.020	-1.451	-0.0887	.15251	.02410	-.09244	.07695	-.00925	-.03972	.15282	-.25993	3.35368
2.020	-4.433	-0.0887	.15136	.02349	-.09269	.07686	-.00927	.01116	.11138	.05774	3.35779
2.020	.563	.02270	.15091	.02591	-.09192	.07599	-.00940	.04065	.16124	.26880	3.36729
2.020	1.630	.04494	.15022	.01984	-.09121	.07583	-.00955	.08248	.15241	.34114	3.36753
2.020	2.676	.08853	.14847	.01984	-.08769	.07471	-.00851	.16328	.15996	1.522376	5.35418
2.020	4.769	-1.7692	.14583	.01913	-.08285	.07276	-.00736	.32775	.19187	1.37168	5.35233
2.020	8.959	.34672	.13959	.02202	-.07753	.07049	-.00664	.47525	.26219	1.33835	5.35982
2.020	13.155	.51858	.13659	.02856	-.07416	.06913	-.00593	.58653	.36253	1.35328	5.35984
2.020	16.295	.65117	.12848	.02878	-.07146	.06725	-.00513	.77725	.42301	1.73939	5.35753
2.020	21.564	.86173	.11656	.02741	-.06444	.06469	-.00475	.77725	.62116	1.37983	5.35723
2.020	26.866	1.12578	.10727	.02436	-.05729	.06125	-.00425	.80787	.68167	1.35846	5.35446
2.020	32.112	1.35576	.10059	.02712	-.04542	.05996	-.00362	1.06482	.80167	1.35846	5.35446
<hr/>											
	RUN NO.	51/ 0	CN	CA	CLM	CR	CYN	CB	Q	L/C	BETA
MACH	ALPHA	-0.06494	.13497	.00574	-.06861	.07454	-.00569	-.02224	.11323	-1.45885	3.35510
2.500	-1.141	-0.03061	.13355	.00513	-.05934	.07495	-.00563	-.01391	.11332	-1.32233	3.35465
2.500	-1.129	-0.03061	.13243	.00572	-.05931	.07533	-.00554	.05254	.11315	.11332	3.35251
2.500	.873	.02456	.13243	.00510	-.05927	.07533	-.00593	.05252	.11321	.26632	5.35216
2.500	1.958	.03959	.13036	.00810	-.05927	.07533	-.00435	.05229	.11320	.48457	5.35295
2.500	2.936	.07100	.12934	.00855	-.05927	.07533	-.00463	.12964	.11313	.92557	5.35173
2.500	5.934	.13842	.12554	.01123	-.08967	.07533	-.00593	.12546	.11313	1.58959	5.35204
2.500	9.133	.27554	.11717	.01191	-.09166	.07635	-.00650	.36926	.1.88186	1.88186	5.35766
2.500	13.299	.42631	.11141	.01652	-.08714	.07199	-.00756	.36926	.20542	1.91426	5.35807
2.500	16.410	.54242	.10713	.02205	-.08135	.07047	-.00705	.46536	.25627	1.91426	5.35551
2.500	21.632	.74078	.09610	.02351	-.07180	.06534	-.00616	.65236	.36522	1.70541	5.35330
2.500	26.882	.96438	.09118	.02255	-.05912	.01126	-.00556	.81695	.51737	1.36156	5.35773
2.500	32.064	1.17845	.08702	.01218	-.01558	.00506	-.00524	.93224	.69958	1.36156	5.35773

## LA46 A/B TABULATED SOURCE DATA

PAGE 28

UPN/T-1032 11-4610081TER (B1W5C41E1F1)

(REFC19)

## PARAMETRIC DATA

BETA = -11.750  
BETAAP = -11.750  
ELEVTR = -15.000  
SP28TR = 55.000

RUN NO.	52 / 0	MACH	ALPHA	CN	CA	CLN	CY	CLY	CDL	CL	CD	LC	BETA
1.500	-2.143	-21696	.1695	.00172	.00198	.00072	.00089	.00092	.00041	.000341	.00032	.00032	
1.500	-1.110	-15955	.16942	.00133	.00145	.00165	.00087	.00095	.00047	.000372	.000353	.000353	
1.500	-0.095	-10439	.16918	.00161	.00176	.00194	.00069	.00091	.00041	.000335	.000324	.000324	
1.500	.959	-0.04993	.16163	.00353	.00367	.00360	.00297	.00297	.00177	.00177	.00177	.00177	
1.500	2.020	.00569	.17961	.00876	.00271	.00182	.00055	.00055	.00174	.00196	.00196	.00196	
1.500	4.128	.11467	.17932	.00349	.00340	.00161	.00034	.00034	.00177	.00282	.00282	.00282	
1.500	6.367	.32978	.16534	.00359	.00397	.00184	.00051	.00051	.00218	.00176	.00176	.00176	
1.500	12.587	.52829	.15624	.00141	.00214	.00214	.00155	.00155	.00155	.00155	.00155	.00155	
1.500	15.764	.68794	.14965	.00341	.00145	.00216	.00082	.00082	.00141	.00152	.00152	.00152	
1.500	21.058	.94717	.13570	.00223	.00593	.00193	.00135	.00135	.00135	.00135	.00135	.00135	
1.500	26.476	1.22520	.12681	.00252	.00190	.00190	.00197	.00197	.00197	.00197	.00197	.00197	
1.500	28.463	1.31569	.12692	.00194	.001593	.00125	.00126	.00126	.00126	.00126	.00126	.00126	
RUN NO.	54 / 0	MACH	ALPHA	CN	CA	CLN	CY	CLY	CDL	CL	CD	LC	BETA
2.000	-1.11737	.15701	.00970	.00121	.00137	.00104	.00131	.00131	.00097	.00097	.00097	.00097	
2.000	-0.496	-0.07747	.15593	.00325	.00397	.00357	.00214	.00214	.00233	.00233	.00233	.00233	
2.000	.556	-.03341	.15432	.00271	.00255	.00110	.00035	.00035	.00454	.00454	.00454	.00454	
2.000	1.610	.00935	.15314	.00121	.00136	.00106	.00036	.00036	.00534	.00534	.00534	.00534	
2.000	2.693	.05335	.15151	.00019	.00128	.00091	.00022	.00022	.00523	.00523	.00523	.00523	
2.000	4.740	.13673	.14792	.00932	.00421	.00253	.00253	.00253	.00434	.00434	.00434	.00434	
2.000	6.927	.30484	.14110	.00358	.00151	.00151	.00035	.00035	.00295	.00295	.00295	.00295	
2.000	13.135	.47074	.13135	.00209	.00102	.00118	.00036	.00036	.00265	.00265	.00265	.00265	
2.000	16.266	.60511	.12543	.00157	.00135	.00137	.00037	.00037	.00376	.00376	.00376	.00376	
2.000	21.526	.83151	.11663	.00180	.00151	.00113	.00095	.00095	.00392	.00392	.00392	.00392	
2.000	26.636	1.26937	.12642	.00266	.00250	.00144	.00142	.00142	.002616	.002616	.002616	.002616	
2.000	32.076	1.30799	.09585	.00368	.00233	.00138	.00152	.00152	.003737	.003737	.003737	.003737	

LARGE AND DISTRIBUTED SOURCE DATA

Hart-Weinberg Equilibrium (Continued)

122

2  
PAGE

CARBONATE 21

RUN NO.	59 / 0	CA	CA
ALPHA	CN	CN	CN
-1.473	-1.12929	-1.15640	-1.15640
- .449	- .57683	- .15119	- .15119
.564	- .55612	- .15373	- .15373
1.612	- .59356	- .15216	- .15216
2.651	- .84975	- .15288	- .15288
2.577	4.733	- .13358	- .14651
2.525	0.125	- .35336	- .14964
15.125	15.125	- .47169	- .13149
16.250	16.250	.60554	.12476
21.542	21.542	.03624	.11572
22.550	22.550	.03624	.11572
22.070	22.070	1.06697	1.06697
32.266	32.266	1.25944	1.25944

END  
DATE

96

APR. 23, 1985